# Standard Test Method for Evaluation of Engine Oils in Diesel Four-Stroke Cycle Supercharged 1M-PC Single Cylinder Oil Test Engine ${ }^{1}$ 


#### Abstract

This standard is issued under the fixed designation D 6618; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.


## INTRODUCTION

This test method can be used by any properly equipped laboratory, without outside assistance. However, the ASTM Test Monitoring Center (TMC) ${ }^{2}$ provides reference oils and an assessment of the test results obtained on those oils by the laboratory. By this means, the laboratory will know whether their use of the test method gives results statistically similar to those obtained by other laboratories. Furthermore, various agencies require that a laboratory utilize the TMC services in seeking qualification of oils against specifications. For example, the U.S. Army imposes such a requirement, in connection with several Army engine lubricating oil specifications.

Accordingly, this test method is written for use by laboratories that utilize the TMC services. Laboratories that choose not to use those services may simply ignore those portions of the test method that refer to the TMC.

This test method may be modified by means of Information Letters issued by the TMC. In addition, the TMC may issue supplementary memoranda related to the test method.

## 1. Scope

1.1 This test method covers a four-stroke cycle diesel engine test procedure for evaluating engine oils for certain high-temperature performance characteristics, particularly ring sticking, ring and cylinder wear, and accumulation of piston deposits. Such oils include both single viscosity SAE grade and multiviscosity SAE grade oils used in diesel engines. It is commonly known as the $1 \mathrm{M}-\mathrm{PC}$ test (PC for Pre-Chamber) and is used in several API oil categories, notably the CF and CF-2 and the military category described in MIL-PRF-2104 (see Note 1).

Note 1-Companion test methods used to evaluate other engine oil performance characteristics for API oil categories CF and CF-2 are discussed in SAE J304. The companion tests used by the military can be found in MIL-PRF-2104.
1.2 The values stated in either SI units or other units are to be regarded separately as the standard. The values stated in each system may not be exact equivalents; therefore, each system shall be used independently of the other, without combining values in any way.
1.3 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the

[^0]responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.
1.4 This test method is arranged as follows:
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## 2. Referenced Documents

2.1 ASTM Standards:

D 86 Test Method for Distillation of Petroleum Products at Atmospheric Pressure ${ }^{3}$
D 93 Test Methods for Flash Point by Pensky-Martens Closed Cup Tester ${ }^{3}$
D 97 Test Method for Pour Point of Petroleum Products ${ }^{3}$
D 130 Test Method for Detection of Copper Corrosion from Petroleum Products by the Copper Strip Tarnish Test ${ }^{3}$
D 445 Test Method for Kinematic Viscosity for Transparent and Opaque Liquids (the Calculation of Dynamic Viscosity) ${ }^{3}$
D 482 Test Method for Ash from Petroleum Products ${ }^{3}$

[^1]D 524 Test Method for Ramsbottom Carbon Residue of Petroleum Products ${ }^{3}$
D 613 Test Method for Cetane Number of Diesel Fuel Oil ${ }^{4}$
D 664 Test Method for Acid Number of Petroleum Products by Potentiometric Titration ${ }^{3}$
D 1319 Test Method for Hydrocarbon Types in Liquid Petroleum Products by Fluorescent Indicator Adsorption ${ }^{3}$
D 1796 Test Method for Water and Sediment in Fuel Oils by the Centrifuge Method (Laboratory Procedure) ${ }^{3}$
D 2422 Classification of Industrial Fluid Lubricants by Viscosity System ${ }^{3}$
D 2425 Test Method for Hydrocarbon Types in Middle Distillates by Mass Spectrometry ${ }^{3}$
D 2500 Test Method for Cloud Point of Petroleum Products ${ }^{3}$
D 2622 Test Method for Sulfur in Petroleum Products by Wavelength Dispersive X-Ray Fluorescence Spectrometry ${ }^{5}$
D 4052 Test Method for Density and Relative Density of Liquids by Digital Density Meter ${ }^{5}$
D 4294 Test Method for Sulfur in Petroleum and Petroleum Products by Energy-Dispersive X-Ray Fluorescence Spectroscopy ${ }^{5}$
D 4485 Specification for Performance of Engine Oils ${ }^{5}$
D 4863 Test Method for Determination of Lubricity of Two-Stroke-Cycle Gasoline Engine Lubricants ${ }^{5}$
D 5302 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Deposit Formation and Wear in a Spark-Ignition Internal Combustion Engine Fueled with Gasoline and Operated Under Low-Temperature, LightDuty Conditions ${ }^{6}$
D 5844 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Rusting (Sequence IID) ${ }^{6}$
D 5862 Test Method for Evaluation of Engine Oils in the Two-Stroke Cycle Turbo-Supercharged 6V92TA Diesel Engine ${ }^{6}$
D 6202 Test Method for Automotive Engine Oils on the Fuel Economy of Passenger Cars and Light-Duty Trucks in the Sequence VIA Spark Ignition Engine ${ }^{6}$
E 344 Terminology Relating to Thermometry and Hydrometry ${ }^{7}$
2.2 SAE Standard: ${ }^{8}$

SAE J304 Engine Oil Tests
2.3 Military Standard: ${ }^{9}$

MIL-PRF-2104 Lubricating Oil, Internal Combustion Engine, Combat/Tactical Service

## 3. Terminology

3.1 Definitions:
3.1.1 calibrate, $v$-to determine the indication or output of a measuring device with respect to that of a standard. E 344

[^2]3.1.2 candidate oil, $n$-an oil that is intended to have the performance characteristics necessary to satisfy a specification and is tested against that specification.

D 5844
3.1.3 clogging, $n$-the restriction of a flow path due to the accumulation of material along the flow path boundaries.

D 5844
3.1.4 engine oil, $n$-a liquid that reduces friction or wear, or both, between the moving parts within an engine; removes heat, particularly from the underside of pistons; and serves as a combustion gas sealant for the piston rings.

D 5862
3.1.4.1 Discussion-It may contain additives to enhance certain properties. Inhibition of engine rusting, deposit formation, valve train wear, oil oxidation, and foaming are examples.
3.1.5 non-reference oil, $n$-any oil other than a reference oil: such as a research formulation, commercial oil, or candidate oil.

D 5844
3.1.6 purchaser, $n$-of an ASTM test, a person or organization that pays for the conduct of an ASTM test method on a specified product.

D 6202
3.1.6.1 Discussion-The preferred term is purchaser. Deprecated terms that have been used are client, requester, sponsor, and customer.
3.1.7 reference oil, $n$-an oil of known performance characteristics, used as a basis for comparison

D 5844
3.1.7.1 Discussion-Reference oils are used to calibrate testing facilities, to compare the performance of other oils, or to evaluate other materials (such as seals) that interact with oils.
3.1.8 scuffing, $n$-in lubrication, damage caused by instantaneous localized welding between surfaces in relative motion that does not result in immobilization of the parts. D 4863
3.1.9 wear, $n$-the loss of material from, or relocation of material on, a surface.

D 5302
3.1.9.1 Discussion-Wear generally occurs between two surfaces moving relative to each other and is the result of mechanical or chemical action or by a combination of mechanical and chemical actions.
3.2 Definitions of Terms Specific to This Standard:
3.2.1 calibration test, $n$-an engine test conducted on a reference oil under carefully prescribed conditions whose result is used to determine the suitability of the engine stand/laboratory to conduct such tests on non-reference oils.
3.2.1.1 Discussion-In this test method, it can also refer to tests conducted on parts to ensure their suitability for use in reference or non-reference tests.
3.2.2 test, $n$-any test time accumulated in accordance with this test method.

## 4. Summary of Test Method

4.1 Prior to each test run, the power section of the engine (excluding piston assembly) is completely disassembled, solvent-cleaned, measured, and rebuilt in strict accordance with furnished specifications. A new piston, piston ring assembly, and cylinder liner are installed each test. The engine crankcase is solvent-cleaned, and worn or defective parts are replaced. The test stand is equipped with appropriate accessories for controlling speed, fuel rate, and various engine operating conditions. A suitable system for supercharging the engine with humidified and heated air shall also be provided.
4.2 Test operation involves the control of the supercharged, single-cylinder diesel test engine for a total of 120 h at a fixed speed and fuel rate, using the test oil as a lubricant. A 1 h engine break-in precedes each test. At the conclusion of the test, the piston, rings, and cylinder liner are examined. Note the degree of cylinder liner and piston ring wear, the amount and nature of piston deposits present, and whether any rings are stuck.

## 5. Significance and Use

5.1 The test method is designed to relate to high-speed, supercharged diesel engine operation and, in particular, to the deposit control characteristics and antiwear properties of diesel crankcase lubricating oils.
5.2 The test method is useful for the evaluation of diesel engine oil quality and crankcase oil specification acceptance. This test method, along with others, defines the minimum performance level of the API categories CF and CF-2 (detailed information about passing limits for these categories is included in Specification D 4485). It is also used in MIL-PRF2104.
5.3 The results are significant only when all details of the procedure are followed. The basic engine used in this test method has a precombustion chamber (as compared to direct injection) and is most useful in predicting performance of engines similarly equipped. This factor should be considered when extrapolating test results. It has been found useful in predicting results with high sulfur fuels (that is, greater than 0.5 wt \%) and with certain preemission controlled engines. It has also been found useful when correlated with deposit control in two-stroke cycle diesel engines.

## 6. Apparatus

6.1 Test Engine—A single-cylinder Caterpillar diesel oil test engine having a 2.2 L (134.1 in. ${ }^{3}$ ) displacement is required. Bore and stroke are 13.0 cm ( 5.125 in .) and 16.5 cm ( 6.5 in. ) respectively. The engine arrangement is shown in Fig. A1.1. The supply of test engines and parts is discussed in 6.22 . The engine is equipped with the accessories or equipment listed in 6.2 through 6.24 .
6.2 Air Pressure-Use a supercharging blower or other device arranged to control air pressure.
6.3 Air Intake System-Use the 1Y38 surge chamber and the air heater mechanism (see Annex A1) or its equivalent.
6.4 Humidity—Use a system to control humidity to the specified test conditions.
6.5 Cooling System—Use a closed, pressurized, circulating cooling system having an engine-driven centrifugal water pump.
6.6 Speed/Load Controls-Use a dynamometer or suitable loading device to control engine speed and measure load.
6.7 Starting-Use a suitable starting arrangement capable of $420 \mathrm{~N} \cdot \mathrm{~m}(310 \mathrm{lbf} \cdot \mathrm{ft})$ breakaway and $373 \mathrm{~N} \cdot \mathrm{~m}(275 \mathrm{lbf} \cdot \mathrm{ft})$ sustained torque at approximately $200 \mathrm{r} / \mathrm{min}$.
6.8 Exhaust System—Use an exhaust system using piping and an exhaust barrel as specified in Annex A1. A restriction valve down stream of the barrel maintains the exhaust gases at a given back pressure as specified in the test conditions.
6.9 Data Acquisition-Configure all stands to acquire data
automatically for speed, fuel flow, intake air pressure, intake air temperature, coolant temperature, oil-to-bearing temperature, and oil-to-jet pressure (as a minimum) with closed loop control on speed, intake air temperature, coolant temperature, and oil-to-bearing temperature (as a minimum).
6.10 Cylinder Head and Cylinder Assemblies-Only cylinder head and cylinder assemblies that have previously passed a calibration test are acceptable for non-reference testing.
6.11 Piston Cooling Nozzle:
6.11.1 Oil Jet Pressure Measurement-The following is required to allow for measurement of the piston cooling nozzle pressure:
6.11.1.1 Replace the 3B9407 fitting with a $1 / 4 \mathrm{in}$. tee fitting, and reconnect the 1 Y 6 oil line.
6.11.1.2 Modify the 1 Y 8199 oil pan to provide access for the pressure pickup.
6.11.1.3 Use oil pressure gage 8 M 2743 , or equivalent.
6.11.1.4 Only piston cooling jets that have been flowchecked by the specified industry standard are approved for use. See footnote 11 for supplier. Fig. A1.2 shows the suggested modification of the 1 Y8199 oil pan and necessary hardware for the cooling nozzle pressure pickup. All test engines with serial numbers greater than 2511252 will be provided with the pressure pickup modification.
6.11.2 Piston Cooling Jet Supplier-To improve precision, Perkin Elmer Automotive Research and Southwest Research Institute (SWRI) have agreed to provide flow-checked 1M-PC P-tubes to the industry. Perkin Elmer Automotive Research will flow and serialize the units and determine if they are within specification and will maintain records, while SWRI will coordinate the redistribution. Send P-tubes to be inspected to Perkin Elmer Automotive Research. ${ }^{10}$
6.11.2.1 The P-tubes will be flowed, using EF-411 oil at $37.8 \pm 0.6^{\circ} \mathrm{C}\left(100 \pm 1^{\circ} \mathrm{F}\right)$ and $165.5 \pm 0.5 \mathrm{kPa}(24 \pm 0.5 \mathrm{psi})$ as measured at the location shown in Fig. A1.2. The acceptable flow range is 1.89 to $2.27 \mathrm{~L} / \mathrm{min}(0.50$ to $0.60 \mathrm{gal} / \mathrm{min})$.
6.11.2.2 To maintain impartiality in selecting P-tubes, only acceptable assemblies will be forwarded to SWRI as unmarked units. These units will be randomly selected for redistribution. In cases in which the only units available are from a single order, only those units will be returned. Assemblies that fall outside of the specifications will not be returned. Instead, Perkin Elmer Automotive Research will generate a nonconformance report with an additional copy to be sent to the laboratory that supplied the P-tube. The failed units will be returned to Caterpillar for credit. Perkin Elmer Automotive Research will indicate on the nonconformance report that the appropriate credit be issued to the originating laboratory. Additional piston cooling assemblies will need to be supplied by the requesting laboratory and submitted to Perkin Elmer Automotive Research.
6.11.2.3 Perkin Elmer Automotive Research will enclose a statement with each unit inspected, disclaiming any liability for subsequent performance of the part. No attempt will be made to ensure that the tubing is properly configured or that any

[^3]other physical property makes it suitable for use. Units damaged during shipment will not be tested, unless specifically requested. Include a packing list and separate purchase orders to Perkin Elmer Automotive Research and SWRI ${ }^{11}$ with each shipment. Please specify a name and address where the parts are to be returned.
6.12 Engine Oil Level Gage—Lower the bayonet gage housing 5 cm ( 2.0 in .) to provide for more accurate oil level readings. Parts required for this modification are shown in Fig. A1.3.
6.13 Crankcase Pressure Control Valve—Install a pressure control valve (1Y479) at the crankcase breather outlet to stabilize crankcase pressure. Installation is shown in Fig A1.4.
6.14 Oil Cooler Inlet Temperature-Record the temperature of the oil cooler inlet by installing a thermocouple in the pipe-tapped hole provided on the rear side of the oil-cooler cover adjacent to the oil inlet port. Care should be taken to provide sufficient thermocouple insertion depth to provide a mid-stream oil temperature.
6.15 Engine Oil System—Use the last chance screen 1Y3549. Modify the oil pump as shown in Fig. A1.10. Add the external oil pump bypass line for safety and convenience factors to adjust oil pressure on engine break-in and warm-up.
6.16 Cooling System—Replace the 7.6 cm (3 in.) standard cooling tower with the 12.7 cm ( 5 in .) pressurized cooling tower as shown in Fig. A1.6. Modify the cooling system to accommodate the pressurized cooling tower, bypass flow control and flow meter as shown in Fig. A1.7 and Fig A1.8. Use a Barco Venturi Meter \#BR 12705-16-31. ${ }^{12,13}$ Use brass or stainless steel pipe that has chamfered ends $\left(45^{\circ}\right)$ into and out of the venturi meter [ 15.2 cm ( 6 in .) minimum into and 5.1 cm (2 in.) minimum out]. Orient the high pressure tap (the first seen by the flow) horizontally.
6.17 Fuel System-Use a standardized engine fuel system to ensure that fuel-line pressure transients are held to acceptable values and to minimize cranking times. Use a Micro Motion ${ }^{13,14}$ flow meter having a range no greater than $0-90.7 \mathrm{~kg} / \mathrm{h}$ $(0-200 \mathrm{lb} / \mathrm{h})$ to measure fuel flow rate.
6.17.1 The line lengths, line sizes, and fuel system components are shown in Fig. A1.5. Use this system without modification, with the possible exception that the fuel shut-off solenoid ${ }^{13,15}$ is eliminated if the line length from the enginemounted filter to the injector pump is standardized at $107 \pm 1$ $\mathrm{cm}(42.25 \pm 0.5 \mathrm{in}$.). Also, an external fuel pump may be used in place of the engine-mounted fuel pump. Control the fuel rate with either manual or automated fuel rack manipulation.
6.18 Intake Air System—Install a dry element oil and particle filter between the air supply source and each engine to

[^4]be run. Use an air filter capable of $10 \mu \mathrm{~m}$ (or smaller) filtration. (Oil bath filters are not acceptable in this location.) Make air filter replacements as required to minimize pressure losses and with sufficient frequency to maintain the air heater barrel as free as possible form oil and dust particles. The 1Y38 surge chamber and air heater assembly required is shown in Annex A1.
6.18.1 Suitable equipment is required to maintain the specified moisture content, temperature, and pressure of the inlet air to the cylinder head. The accuracy of the humidification system is to be within $\pm 0.648 \mathrm{~g}$ ( $\pm 10$ grains) of the humiditymeasuring, chilled-mirror dew point hydrometer (see 9.6.2).
6.19 Exhaust System—Uniformity in exhaust system pressure patterns within a laboratory and from laboratory-tolaboratory is required to minimize a major test variable. The dimensions and distance of the exhaust piping from the exhaust elbow to the barrel, as well as the volume of the exhaust barrel, are specified in Figs. A1.30 to A1.34. Note the exhaust barrel may be insulated or water cooled. The downstream distance of the restriction valve from the exhaust barrel is not specified.
6.19.1 Set the exhaust pressure at specified conditions as given in Table 1 by varying the restriction valve. Measure the pressure in the exhaust barrel as shown in Fig. A1.31. The location of the 1 Y 467 or equivalent exhaust thermocouple is shown in Fig. A1.30.
6.20 Blowby Meter, a displacement type gas meter or equivalent fitted with an oil separator and surge chamber. A fitting on the crankcase breather (see Fig. A1.4) permits attachment of the meter to the engine by using appropriate lengths of hose or pipe, or both, suitable to the laboratory's needs.
6.21 Thermocouples-Specified thermocouples (or equivalents) are required for obtaining temperatures at the following locations: air-to-engine (1Y468), exhaust temperature (1Y467), and water inlet, water outlet, oil-to-bearings (1Y466).
6.21.1 Install thermocouples 1 Y 468 , 1 Y 467 , and 1 Y 466 only at the temperature-sensing locations provided with the 1Y73 engine arrangement. Locate the immersion depth for water inlet, water outlet, and oil-to-bearing temperature sensors so that the tip of the sensor is midstream of the fluid measured. Immersion depth for the air and exhaust temperature sensors are measured as follows (variation from these dimensions is not permitted):
6.21.1.1 Air temperature sensor depth: $27 \pm 2 \mathrm{~mm}(11 / 16 \pm$ 1/16 in.)
6.21.1.2 Exhaust temperature sensor depth: $65 \pm 2 \mathrm{~mm}$ ( $29 / 16 \pm 1 / 16$ in.)
6.22 Parts:
6.22.1 Procurement of Parts-Information concerning procurement of Caterpillar test engines and replacement parts and approval of equivalent parts substitutions allowed in this test method is obtained by contacting Caterpillar Inc. ${ }^{13,16}$ Other parts and their sources referred to throughout the procedure are found in the footnotes. Use all Caterpillar parts on a first-in-first-out basis.
6.22.2 All parts for the 1 Y 73 engine and the 1 Y 73 Conversion Kit that are nonconforming by reason of faulty manufacture should be discussed with the Engine System Technology Department (ESTD) at Caterpillar Inc. ${ }^{13,16}$
6.22.2.1 The test labs should contact ESTD when they believe a part is nonconforming:
6.22.2.2 ESTD will determine if they want the part returned, or provide warranty without viewing the part.
6.22.2.3 If ESTD determines that the part is nonconforming without viewing the part, the test labs will be asked to return the part to their Caterpillar dealer. ESTD will contact the dealer with the information that the part is being returned and provide warranty for it.
6.22.2.4 If ESTD wants to view the part, they will issue a Return Goods Authorization Number (RGA) to the test lab and send the part and the form to Caterpillar Inc. ${ }^{13,17}$
6.22.2.5 If ESTD determines that the part is nonconforming, they will contact the dealer for the test lab and have the dealer provide warranty.
6.22.2.6 A sample of the RGA Claim Form is shown in Fig. 1. It should include return goods authorization number, part name, hours on the part, part number, quantity, purchase order number, date purchased, test lab that purchased the part, contact person's name, phone, fax, and address, dealer's name that sold the part, and measurements or photographs, or both, to document the nonconformance.

[^5]TABLE 1 1M-PC Operating Conditions ${ }^{A, B}$

| Speed, r/min | $1800 \pm 10$ |
| :---: | :---: |
| Fuel flow, kg/h (lb/h) | $8.13 \pm 0.07(17.92 \pm 0.15)$ |
| Temperature, water from cylinder head, ${ }^{\circ} \mathrm{C}\left({ }^{\circ} \mathrm{F}\right)$ | $87.8 \pm 2.8(190 \pm 5)$ |
| Flow rate, engine coolant, L/min (gal/min) | $57.9 \pm 3.8(15.3 \pm 1.0)$ |
| Temperature, oil to bearings, ${ }^{\circ} \mathrm{C}\left({ }^{\circ} \mathrm{F}\right)$ | $96.1 \pm 2.8(205 \pm 5)$ |
| Temperature, inlet air to engine, ${ }^{\circ} \mathrm{C}\left({ }^{\circ} \mathrm{F}\right)$ | $123.9 \pm 2.8(255 \pm 5)$ |
| Temperature, exhaust, ${ }^{\circ} \mathrm{C}\left({ }^{\circ} \mathrm{F}\right)$ | $573 \pm 28(1063 \pm 50)$ |
| Pressure, fuel to injection pump, kPa (psi) | $137.9 \pm 13.8(20 \pm 2)$ |
| Pressure, exhaust, kPa (in. Hg Abs.) | $106.7 \pm 1.7(31.5 \pm 0.05)$ |
| Pressure, oil at jet cooling nozzle, kPa (psi) | $165.5 \pm 13.8(24 \pm 2)$ |
| Pressure, oil to bearings maximum, kPa (psi) | 220.6 (32) |
| Pressure, air to engine, kPa (in. Hg Abs .) | $179.0 \pm 1.0(53 \pm 0.3)$ |
| Vacuum, crankcase, kPa (in. $\mathrm{H}_{2} \mathrm{O}$ ) | $0.25 \pm 0.12(1.0 \pm 0.5)$ |
| Humidity, air to engine, g/kg of dry air (grains/lb) | $17.8 \pm 1.7(125 \pm 12)$ |
| Flow rate, engine air, approximate $\mathrm{m}^{3} / \mathrm{min}\left(\mathrm{ft}^{3} / \mathrm{min}\right)$ at $15.6^{\circ} \mathrm{C}\left(60^{\circ} \mathrm{F}\right)$, 101.3 kPa Abs. ( 14.7 psi Abs.) | 0.2 (94) |

RETURN GOODS AUTHORIZATION CLAIM FORM

## RETURN GOODS AUTHORIZATION CLAIM FORM

Return Goods Authorization Number: $\qquad$ .

Claim Date: $\qquad$
Contact: Caterpillar Inc
Engine System Tech Dev.
P.O. Box 610

Mossville, Il 61552
Phone: 309-578-2131
Fax: 309-578-6457
Attn: R.A. Riviere

Part Number / Quantity: $\qquad$
Part Name / Hrs On Part: $\qquad$
Date Part Purchased: $\qquad$
Engine Serial Number: $\qquad$ .

Test Lab
Name: $\qquad$
Address: $\qquad$
Contact Person's Name: $\qquad$ .

Phone Number: $\qquad$
Fax Number: $\qquad$ .

Name of Dealer That Sold Part: $\qquad$ .

INCLUDE DOCUMENTATION AND PHOTOS OF NONCONFORMING PART
FIG. 1 Return Goods Authorization Claim Form
6.23 Instrumentation, capable of meeting (or exceeding) the calibration tolerances, measuring resolutions, and maximum system time constants shown in Tables 2-4.
6.24 Crankcase Paint-Inspect crankcases regularly to ensure proper paint coating. Coat crankcases as necessary, using

TABLE 2 Calibration Tolerances

| Parameter | Tolerance |
| :---: | :---: |
| Speed, r/min | 2 |
| Load | NA due to differences within industry. TMC to verify each lab during visits. |
| Fuel flow | Absolute error $\leq 0.125$ \% |
| Humidity | NA. Already specified. Checked during running conditions as outlined in the test procedure (see form attached) |
| Temperatures | ${ }^{\circ} \mathrm{C} \quad{ }^{\circ} \mathrm{F}$ |
| Coolant out | 0.25 0.5 |
| Coolant in | 0.25 0.5 |
| Oil to bearing | 0.5 |
| Intake air | 0.5 |
| Exhaust | 1.0 2.0 |
| Pressures |  |
| Oil to bearing, psig | $0.7 \mathrm{kPa} \quad 0.1$ |
| Oil to jet, psig | $0.7 \mathrm{kPa} \quad 0.1$ |
| Inlet air, in Hg | $0.3 \mathrm{kPa} \quad 0.1$ |
| Exhaust, in Hg | $0.3 \mathrm{kPa} \quad 0.1$ |
| Fuel at filter housing., psig | $0.7 \mathrm{kPa} \quad 0.1$ |
| Crankcase vacuum, in $\mathrm{H}_{2} \mathrm{O}$ | 0.02 kPa |

either of two approved coatings. ${ }^{13,18}$

## 7. Reagents and Materials

7.1 Fuel-The test fuel is specified: Fuels \& Chemicals, LLC 0.4 \% Sulfur Diesel Test Fuel. ${ }^{13,19}$ All fuel shall meet the fuel specifications as shown in Annex A4 and shall be referenced through the ASTM TMC. Approximately 1137 L ( 300 gal ) are required for each test. Include the fuel analysis for the last batch used for the test in the final report (Fig. A2.19). The fuel supplier provides the analysis. If more than one batch is used, note this is in the comments section (Fig. A2.10) with the appropriate percentages of run time.
7.2 Test Oil—Approximately 30 to 34 L ( 8 to 9 gal ) of test oil are required for each test.
7.3 Engine Coolant, a mixture of 118 mL (4 fluid oz) Part Number 3P2044 coolant additive (Pencool $2000^{13,20}$ ) per 4 L (1 gal) of mineral-free water. Mineral-free water is defined as having a mineral content no higher than 34.2 ppm (2 grains/ gal) total dissolved solids. A fresh coolant mixture is used for each new test.

### 7.4 Cleaning Materials:

7.4.1 Solvent-Use aliphatic naphtha Stoddard solvent in the engine flush procedure outlined in 9.10. (WarningFlammable. Eye irritant. Wear goggles or face shield (as for gasoline).)
7.4.2 Dispersant Engine Cleaner-Use Dispersant Engine Cleaner ${ }^{13,21}$ (order by this name) in solution with the aliphatic naphtha in the engine flush procedure.

[^6]7.4.3 General Cleaning Agents-Use sodium bi-sulfate $\left(\mathrm{Na}_{2} \mathrm{SO}_{4}\right)$ and tri-sodium phosphate $\left(\mathrm{Na}_{3} \mathrm{PO}_{4}\right)$ in solution with water in the cooling system flush procedure. (Warning-Eye and throat irritants; repeated exposure can cause dermatitis. Wear protective gloves, face mask, or chemical type goggles.)

## 8. Safety

8.1 The operating of engine tests can expose personnel and facilities to a number of safety hazards. It is recommended that only personnel who are thoroughly trained and experienced in engine testing should undertake the design, installation and operation of engine test stands. Each laboratory conducting engine tests should have its test installation inspected and approved by its safety department. Provide personnel working on the engines with the proper tools, be alert to common sense safety practices, and avoid contact with moving or hot engine parts. Guards should be installed around all external moving or hot parts. When engines are operating at high speeds, heavy duty guards are required and personnel should be cautioned against working alongside the engine and coupling shaft. Provide barrier protection for personnel. All fuel, oil lines, and electrical wiring should be properly routed, guarded, and kept in good order. Scraped knuckles, minor burns, and cuts are common if proper safety precautions are not taken. Safety masks or glasses should always be worn by personnel working on the engines, and no loose or flowing clothing should be worn near running engines.
8.2 Keep the external parts on the engine and the floor area around the engines clean and free of oil and fuel spills. In addition, keep working areas free of all tripping hazards. In case of injury, no matter how slight, first aid attention should be applied at once and the incident reported. Personnel should be alert for leaking fuel or exhaust gas. Leaking fuel represents a fire hazard, and exhaust gas fumes are noxious. Containers of oil or fuel cannot be permitted to accumulate in the testing area.
8.3 Equip the test installation with a fuel shut-off valve designed to automatically cut off the fuel supply to the engine when the engine is not running. A remote station for cutting off fuel from the test stand is recommended. Provide suitable interlocks so that engine is automatically shut down when any of the following events occur: engine or dynamometer loses field current, engine overspeeds, exhaust system fails, room ventilation fails, or the fire protection system is activated. Consider an excessive vibration pickup interlock if equipment is operated unattended. Provide fixed fire protection equipment, and make dry chemical fire extinguishers available at the test stands. (Warning-Many ASTM tests use chemicals to flush engines between tests. Some of these chemicals require that personnel wear face masks, dust breathers, and gloves because exothermic reactions are possible. Provide emergency showers and face rinse facilities when handling materials.)

## 9. Preparation of Apparatus

### 9.1 Supplementary Service Information:

9.1.1 Caterpillar Service Manual-Engine service information not found in this test method may be obtained by referring to the Caterpillar Single Cylinder Oil Test Engine Service

TABLE 3 Operational Specifications, Measurement Resolution, and Reporting Resolution

|  | SI Specification |  |  |  | US Customary System (USCS) Specification |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Parameter | Units | Spec | Minimum Measurement Regulation | Round Values to the Nearest | Units | Spec | Minimum Measurement Resolution | Round Values to the Nearest |
| Speed | $\mathrm{r} / \mathrm{min}$ | $1800 \pm 10$ | 1 | Whole number | r/min | $1800 \pm 10$ | 1 | Whole number |
| Power | kW | 31.3 |  |  | bhp | 42 |  |  |
| BMEP | kPa | 951 |  |  | psig | 138 |  |  |
| Fuel rate | $\mathrm{kJ} / \mathrm{min}$ | $6172 \pm 53$ |  |  | Btu/min | $5850 \pm 50$ |  |  |
| Fuel flow ${ }^{\text {A }}$ | $\mathrm{kg} / \mathrm{h}$ | $8.13 \pm 0.07$ | 0.01 | Hundredth | $\mathrm{lb} / \mathrm{h}$ | $17.92 \pm 0.15$ | 0.01 | Hundredth |
| BSFC | kg/kWh | 0.260 |  |  | lb/bhp.h | 0.427 |  |  |
| Humidity | $\mathrm{g} / \mathrm{kg}$ | $17.8 \pm 1.7$ | 0.1 | Tenth | grains/lb | $125 \pm 12$ | 1 | Whole number |
| Oil weight | g | N/A | 1 | Whole number | lb | N/A | 0.01 | Hundredth |
| Temperatures |  |  |  |  |  |  |  |  |
| Coolant out | ${ }^{\circ} \mathrm{C}$ | $87.8 \pm 2.8$ | 0.1 | Tenth | ${ }^{\circ} \mathrm{F}$ | $190 \pm 5$ | 0.1 | Tenth |
| Coolant in | ${ }^{\circ} \mathrm{C}$ | 82.8 | 0.1 | Tenth | ${ }^{\circ} \mathrm{F}$ | 181 | 0.1 | Tenth |
| Coolant $\Delta$ | ${ }^{\circ} \mathrm{C}$ | $5 \pm 1.0$ | 0.1 | Tenth | ${ }^{\circ} \mathrm{F}$ | $9 \pm 2$ | 0.1 | Tenth |
| Oil to bearing | ${ }^{\circ} \mathrm{C}$ | $96.1 \pm 2.8$ | 0.1 | Tenth | ${ }^{\circ} \mathrm{F}$ | $205 \pm 5$ | 0.1 | Tenth |
| Inlet air | ${ }^{\circ} \mathrm{C}$ | $123.9 \pm 2.8$ | 0.1 | Tenth | ${ }^{\circ} \mathrm{F}$ | $255 \pm 5$ | 0.1 | Tenth |
| Exhaust | ${ }^{\circ} \mathrm{C}$ | $573 \pm 28$ | 1 | Whole number | ${ }^{\circ} \mathrm{F}$ | $1063 \pm 50$ | 1 | Whole number |
| Pressures |  |  |  |  |  |  |  |  |
| Oil to bearing | kPa | 220.6 Max |  |  | psig | 32 max |  |  |
| Oil to jet | kPa | $165.5 \pm 13.8$ | 0.1 | Tenth | psig | $24 \pm 2$ | 0.1 | Tenth |
| Inlet air (ABS) | kPa | $179 \pm 1$ | 0.1 | Tenth | in. Hg | $53.0 \pm 0.3$ | 0.1 | Tenth |
| Exhaust (ABS) | kPa | $106.7 \pm 1.7$ | 0.1 | Tenth | in. Hg | $31.5 \pm 0.5$ | 0.1 | Tenth |
| Fuel at filter housing. | kPa | $137.9 \pm 13.8$ | 0.1 | Tenth | psig | $20 \pm 2$ | 0.1 | Tenth |
| Crankcase vac | kPa | $0.25 \pm 0.12$ | 0.01 | Hundredth | in. $\mathrm{H}_{2} \mathrm{O}$ | $1 \pm 0.5$ | 0.1 | Tenth |
| Flows Coolant flow | L/min | $57.9 \pm 3.8$ | 0.1 | Tenth | $\mathrm{gal} / \mathrm{min}$ | $15.3 \pm 1.0$ | 0.1 | Tenth |

${ }^{A}$ Fuel flow spec is based on the high heating value of 19.590 Btu/lb at an A.P.I. gravity of 35 . Fuel spec is 33 to 35 A.P.I. gravity.

TABLE 4 Maximum Allowable System Time Constants

| Measurements |  |
| :--- | :---: |
| Speed | 3.0 s |
| Fuel Flow | 73.0 s |
| Temperatures |  |
| Coolant Out | 3.0 s |
| Coolant In | 3.0 s |
| Oil to Bearings | 3.0 s |
| Intake air | 3.0 s |
| Exhaust | 3.0 s |
| Pressures | 3.0 s |
| Oil to Bearings | 3.0 s |
| Oil to Jet | 3.0 s |
| Intake Air | 3.0 s |
| Exhaust | 3.0 s |
| Fuel at Filter | 3.0 s |
| Crankcase Vac. |  |

Manual (Form No. SENR2074) and parts manual SEBP1299. ${ }^{13,16}$
9.1.2 Pretest Maintenance Check List and Continuing Engine Inspection-A recommended list of items that are checked or replaced at the intervals specified is shown in Table 5.

### 9.2 General Engine Inspection:

9.2.1 Perform a complete engine inspection every 10000 test hours. This inspection is done to ensure that wearing surfaces, such as main bearings and journals, rod bearings and journals, camshaft bearings, and so forth, are within manufacturer's specifications. This inspection will terminate the current test stand calibration (if any). Recalibration is required any time the crank is removed for any purpose other than bearing replacement.
9.2.2 Maintain a complete record of all engine maintenance and measurements. Retain a description of inspection methods along with the maintenance records for review when requested.
9.3 Intake Air System—Prior to each stand calibration test, inspect the intake air barrel for rust and debris. This may be done through either of the pipe flanges, using a borescope or some other optical means. Remove any foreign material.
9.4 Cooling System:
9.4.1 Whenever visual inspection indicates the need, remove all mineral deposits and oil from the cooling system. Make the initial coolant charge at the start of the test with distilled or de-ionized water and a rust inhibitor (Penncol 2000) (see 7.3). The cooling system shall remain full during all shutdowns that do not require the cooling system to be drained.
9.4.2 Make any make-up coolant additions throughout the test with the same treated water solution. Monitor the cooling system visually at the glass or plastic tube in the 1Y504 water outlet line assembly. At any indication of vapor formation, the coolant will have a clouded appearance. Should this occur during a test, shutdown the engine and check for air leakage on the suction side of the water pump or combustion gas leakage in the cylinder head. No air is permitted in the system.
9.5 Engine Cooling System Cleaning-Clean the cooling system when visual inspection shows the presence of oil or grease, mineral deposits, or rust. Heads may be cleaned when either on or off the engine. Use the following procedure:
9.5.1 Operate the engine long enough to reach oil and water operating temperatures; drain the cooling system.
9.5.2 Fill the cooling system with a solution of $450 \mathrm{~g}(1 \mathrm{lb})$ commercial sodium bisulfate $\left(\mathrm{Na}_{2} \mathrm{SO}_{4}\right)$ to $19 \mathrm{~L}(5 \mathrm{gal})$ of water; then run the engine at operating temperature for $1 / 2 \mathrm{~h}$.
9.5.3 Drain and flush the engine with fresh water, and drain the water from the system.
9.5.4 Fill the cooling system with a solution of $450 \mathrm{~g}(1 \mathrm{lb})$ of tri-sodium phosphate $\left(\mathrm{Na}_{3} \mathrm{PO}_{4}\right)$ to $38 \mathrm{~L}(10 \mathrm{gal})$ of water;

TABLE 5 Pretest Maintenance Check List ${ }^{A}$ and Continuing Engine ${ }^{B}$ Inspection

| Item to be checked | Remarks |
| :---: | :---: |
| Fuel injection pump adjusting screw (2F8337) | Inspect before each test. Replace as necessary. |
| Fuel injection pump | Check pump plunger sector gear for tooth wear-general condition of pump (visual); replace pump as necessary. |
| Fuel injection valve | Install new before each test. Inspect fuel injection line orifice (both ends) for correct diameter, 1.57 mm ( 0.062 in.) minimum. |
| Fuel injection timing | $3.81 \pm 0.127 \mathrm{~mm}\left(0.150 \pm 0.005 \mathrm{in}\right.$.) lift, BPC at $8^{\circ} \mathrm{BTC}$. |
| Injection pump inlet seal (2M4453) | Install new before each test. |
| Filter-fuel system | Install when fuel pressure cannot be held within test limits. |
| Cylinder head | New (calibration test only) or reconditioned head for each test. Measure and record valve head and stem projection. Measure prechamber orifice diameter (7.59-7.64 mm [0.299-0.301 in.]). |
| Cylinder head gasket (1Y7960) | Install new before each test. |
| Piston cooling jet | Inspect for plugging and proper positioning before each test; use aiming guide. Verify piston-tocooling jet clearance. |
| Water pump and fuel transfer pump belts | Inspect and adjust as necessary. (Measure deflection at point midway between pulleys - water and fuel.) |
|  | Belt deflection Force |
|  | 19.05 mm |
|  | (0.75 in.) (25 lb) |
| Fuel pressure | $138 \mathrm{kPa}(20 \mathrm{psi})$ |
| Water flow | $58.0 \mathrm{~L} / \mathrm{min}(15.3 \mathrm{gal} / \mathrm{min}$ ) |
| Crankcase stud seal (1Y2310) | Inspect and replace as required. Install with taper down. |
| Valve tappets | Zero lash $+1 / 2$ turn hydraulic lash adjusters. ${ }^{\text {C }}$ |
| Piston pin | Clearance in rod pin bushing-0.051 mm (0.002 in.) maximum |
| Fuel pump rack and rack control rod, gov. button, lever, and sliding sleeve | Check rack for tooth wear-rack control rod for worn ball and socket joints and loose nuts and washers. Gov. button and lever for wear and free movement, sliding sleeve for free movement, bearing condition, and gov. wt. contact and wear. |
| Valve rotators | Inspect for proper operation at start of test and end of test. |
| Leaks | Repair immediately upon detection, particularly fuel, oil, air, exhaust, and coolant. |

[^7]operate the engine for 5 min to ensure complete mixing of the $\mathrm{Na}_{3} \mathrm{PO}_{4}$ solution with any material left from the previous flush.
9.5.5 Drain the engine, flush with clear water, and drain after flushing.
9.5.6 Disassemble the engine, and prepare for the next test.

Note 2-If the purpose of the system cleaning is to descale only, 9.5.4 and 9.5 .5 can be omitted.
9.6 Instrumentation Calibration Requirements:

### 9.6.1 General Requirements:

9.6.1.1 Calibrate all facility read-out instrumentation used for the test immediately prior to commencing a test stand calibration. Instrumentation calibrations prior to subsequent stand calibration tests (that is, those that follow a failed or invalid first attempt) are at the discretion of the test laboratory. Make these calibrations part of the laboratory record (refer to Tables 2-4 for specifications).
9.6.1.2 Calibrate on a yearly basis all temperature, pressure, flow, and speed measurement standards with instruments traceable to a national bureau of standards (for example, the National Bureau of Standards and Technology or its successor agency for labs operating in the United States). Maintain records of all calibrations for a minimum of two years.
9.6.2 Specific Humidity Requirements:
9.6.2.1 Calibrate the primary laboratory humidity measurement system during the first 24 h of each individual stand calibration test using a chilled-mirror dew point hygrometer with an accuracy of at least $\pm 0.55^{\circ} \mathrm{C}$ at $24^{\circ} \mathrm{C}\left( \pm 1^{\circ} \mathrm{F}\right.$ at $\left.75^{\circ} \mathrm{F}\right)$ dew point. The calibration consists of a series of paired comparison measurements between the primary system and the chilled-mirror dew point hygrometer. The comparison period
lasts from 20 min to 2 h with measurements taken at 1 to 6 min intervals, for a total of 20 paired measurements. The measurement interval should be appropriate for the time constant of the humidity measuring instruments.
9.6.2.2 The location of the hygrometer tap is shown in Fig. A1.28. The sample line may require insulation to prevent dropping below dew point temperature and shall not be hygroscopic. The flow rate shall be verified to be within the equipment manufacturer's specification.
9.6.2.3 All measurements taken with the dew point hygrometer are at atmospheric pressure and corrected to standard conditions ( 101.12 kPa [29.92 in. Hg ]) using the perfect gas law or Tables X1.1 to X1.9 in Appendix X1. Compute the difference between each pair of measurements and use to form a mean and standard deviation. The absolute value of the mean difference shall not exceed 0.648 g ( 10 grains), and the standard deviation shall be less than or equal to 0.324 g ( 5 grains). Both of these requirements shall be met for the primary humidity measurement system to be considered calibrated. If either of these requirements cannot be met, the laboratory should investigate the cause, make repairs, and recalibrate. Maintain the calibration data for two years.
9.6.2.4 Recommended Practice-Install drain taps at the low points of the combustion air system and keep open during shut-down and warm-up.

### 9.6.3 Specific Coolant Flow Requirements:

9.6.3.1 As a calibration standard, each test lab is required to maintain at least one Barco venturi flow meter configured as shown in Fig. A1.8 and described in 6.16. On a yearly basis, calibrate this Barco (with its inlet and outlet piping) with an
instrument traceable to a national bureau of standards (for example, the National Bureau of Standards and Technology or its successor agency for labs operating in the United States). The inlet and outlet piping shall remain with this Barco assembly.
9.6.3.2 During the break-in prior to each calibration test, place this calibrated Barco assembly in the standard mounting position. Adjust the coolant flow bypass valve until the readout equipment being used registers the differential pressure that corresponds to $57.9 \mathrm{~L} / \mathrm{min}(15.3 \mathrm{gal} / \mathrm{min})$ for this calibrated Barco assembly.
9.6.3.3 After break-in, replace the calibrated Barco assembly with the stand's running Barco assembly. Do not re-adjust the coolant flow bypass valve. Maintain whatever differential pressure is registered with the stand Barco at this point throughout the duration of the test. Test all non-reference oils with this stand Barco assembly run at this differential pressure. If desired, adjust any readout equipment to make this differential pressure correspond to $57.9 \mathrm{~L} / \mathrm{min}(15.3 \mathrm{gal} / \mathrm{min})$.
9.7 Engine Crankcase Cleaning-Flush the engine prior to each new test. The objective is to remove all deposits from all surfaces of all engine cavities prior to each test. In some instances, extra cleaning may be required. A finger-wiping check may be made on less accessible engine surfaces from time-to-time to determine if the engine is clean.
9.8 Additional Oil Filter-Install a full-flow paper element oil filter in the flushing pump unit to remove engine wear particles during engine flush. Such particles have been known to cause piston scuffing during subsequent testing. ${ }^{13,22}$
9.9 Flushing Procedure Components-Conduct the engine flushing procedure with the components shown in Fig. A1.12 through A1.19 (the design for mobilizing the flushing pump arrangement, Fig. A1.13, is optional). Figure A1.17 (Views A and B) illustrates the use of the flushing components.
9.10 Flushing Procedures-Use the following flushing procedure:
9.10.1 Rotate the crankshaft until the top end of the connecting rod is below the cylinder block bore in the top of the crankcase. Install the poly(methyl methacrylate) (PMMA) or clear plastic cover (Fig. A1.12 on the top surface of the crankcase, as shown in Fig. A1.17 (View A).
9.10.2 For First Stage Flushing with Stoddard Solvent ${ }^{13,} 23$ :
9.10.2.1 Install a clean 1Y5700 element in both the engine and flushing pump oil filter housings.
9.10.2.2 Connect the flushing pump (Fig. A1.13) outlet hose to the engine oil cooler drain location.
9.10.2.3 Remove breather assembly 1Y2592 (top portion of side cover assembly) and clean separately by soaking in aliphatic naphtha. Air-dry.
9.10.2.4 Insert the 1 Y5 rocker shaft oil line in the center opening of the clear plastic cover (see Fig. A1.12).
9.10.2.5 Place the flushing pump inlet line in a clean supply tank (sample location illustrated in Fig. A1.13) containing 7.6

[^8]L (2 gal) of aliphatic naphtha. Open the crankcase drain, start the flushing pump, and run this flush material through the engine into a drain pan one time. Do not recirculate.
9.10.2.6 Close the crankcase drain and connect the flushing pump inlet line to the crankcase drain.
9.10.3 For Second Stage Flushing and Recirculating with Cleaning Mixture—Mix 1.9 L ( $1 / 2 \mathrm{gal}$ ) of dispersant engine cleaner (see Footnote 19) with 5.7 L ( $11 / 2 \mathrm{gal}$ ) of aliphatic naphtha to obtain $7.6 \mathrm{~L}(2 \mathrm{gal})$ of flushing solution. Add this mixture to the crankcase.
9.10.3.1 Connect the flushing pump outlet line to the engine oil cooler drain location. Open the crankcase drain valve, start the flushing pump, and circulate the flushing solution through the engine for approximately 15 min . Turn off the pump. (Do not drain the flushing solution from the crankcase.)
9.10.3.2 Close the oil cooler drain valve, disconnect the flushing pump outlet hose from the oil cooler drain location, and connect to the crankcase sprayer (Fig. A1.14).
9.10.3.3 Remove the 1 Y5 oil line from the cover hole, insert the crankcase sprayer through the opening in the PMMA cover. Start the flushing pump, and spray the interior of the crankcase by slowly moving the sprayer around and into all accessible areas of the crankcase (see Fig. A1.17, View A) for approximately 10 min . Turn off the pump. (Do not drain the flushing solution from the crankcase).
9.10.3.4 Remove the $1 / 2 \mathrm{in}$. pipe plug from the modified 1Y1990 governor housing cover (see Fig. A1.15). Insert the crankcase sprayer (Fig. A1.14) through the opening in the governor housing cover, start the pump, and spray the interior of the governor housing for approximately 10 min . Turn off the pump. (Do not drain the flushing solution from the crankcase.)
9.10.3.5 Remove the oil filler spout assembly from the front of the crankcase, and install the front cover sprayer (see Fig. A1.16) as shown in Fig. A1.17.
9.10.3.6 Connect the flushing pump outlet to a $64 \mathrm{~mm} \times 13$ $\mathrm{cm}(1 / 2 \mathrm{in} . \times 5 \mathrm{in}$.) pipe on the front cover sprayer (see Fig. A1.16). Start the flushing pump, and spray the interior of the front cover for approximately 10 min . Drain the crankcase, governor, oil filter, and oil cooler; and discard the flushing solution.
9.10.4 Using aliphatic naphtha-Repeat 9.10.2.4 through 9.10.2.6 until the aliphatic naphtha discharge is clean. (Three to four flushes with aliphatic naphtha are usually sufficient to remove all traces of the flushing solution from the engine.) Drain the aliphatic naphtha from the crankcase, governor housing, oil filter, and oil cooler.
9.10.5 Test Oil Flushing-When engine is to be used immediately:
9.10.5.1 Prepare for the flush with the test oil by blocking off the 1 Y 5 oil line to the rocker arm shaft and installing the 6.4 $\mathrm{mm}(1 / 4 \mathrm{in}$.) fitting (see Fig. A1.18) on the open end of the line. Close all drain openings.
9.10.5.2 Using the flushing pump, add 4.7 L (5 qt) of test oil to the engine crankcase through the engine oil cooler.
9.10.5.3 Connect the flushing pump outlet to the engine oil cooler drain location. Start the flushing pump, and force any aliphatic naphtha in the system out the crankcase drain. After the aliphatic naphtha has been forced out of the system,
connect the inlet line of the flushing pump to the crankcase drain. Install the dummy piston (reference service manual SENR2074 ${ }^{13,16}$ ) and the assembled cylinder liner and block assembly or the alignment fixture specified in Fig. A1.19. Re-install the oil filler spout and pipe plug in the modified governor housing cover (see Fig. A1.15).
9.10.5.4 Open the crankcase drain and start the flushing pump. Set and maintain the oil pressure at $207 \mathrm{kPa}(30 \mathrm{psi})$. With the starter or dynamometer, turn the engine over for 1 min. Turn off the pump, and drain all oil from the engine crankcase, governor housing, oil filter, and oil cooler. Discard the oil drained.
9.10.5.5 Charge the engine again with 4.7 L (5 qt) of test oil, and repeat the procedure described in 9.10.2. During this flush, check the alignment of the piston cooling nozzle and adjust, if necessary. Before any such adjustment, make sure that the oil-stream condition has stabilized, that is, a steady stream of oil impinges the piston indicating that the oil pressure has attained a constant value. After draining the oil, install a clean element in the engine oil filter housing. Reinstall crankcase breather assembly 1Y2592.
9.10.6 Test Oil Flushing-When the test oil is not available and the engine test start will be delayed: follow the steps up to 9.10 .5 .2 . However, in 9.10 .5 .2 , use buildup oil ${ }^{13,24}$ in place of test oil. When a test oil is scheduled for the engine, perform the following steps:
9.10.6.1 Connect the flushing pump outlet to the engine oil cooler drain location. Using the flushing pump, add 4.7 L (5 qt) of test oil to the engine crankcase through the engine oil cooler. Start the flushing pump, and force the build-up oil out the crankcase drain. After the build-up oil has been forced out of the system, connect the inlet line of the flushing pump to the crankcase drain. Set and maintain oil pressure at 207 kPa (30 $\mathrm{psi})$. By hand, turn the engine five revolutions, and continue to run the pump for 4 min . Turn off the pump, and drain all oil from the engine crankcase, governor housing, oil filter, and oil cooler. Discard the oil drained.
9.10.6.2 Repeat the procedure described in 9.10.6.1. After draining the oil, install a clean element in the engine oil filter housing and prepare the engine for break-in.
9.10.7 An instruction sheet for technician use during the engine cleaning is shown in Fig. 2.
9.11 Piston Cleaning Preparation-Clean new pistons using the following procedure before the installation of rings and final installation into the engine:
9.11.1 Spray with aliphatic naphtha or mineral spirits, and dry with compressed air. (Warning-High concentration of vapors should be avoided. Use vented hood, face shield, gloves (same precautions as for gasoline).)
9.11.2 Using a lint-free cloth, wipe clean the entire piston with pentane, paying special attention to ring groove and land areas. Allow the piston to air dry.
9.11.3 Wipe the piston with Mobil EF-411 ${ }^{13,24}$ before final installation into the engine.

[^9]9.12 Cylinder Head:
9.12.1 Valve Guide Bushings-Remove and replace the 1 Y 448 and 1Y449 valve guide bushings with 1Y457 valve guide bushings (inlet) and 1Y469 valve guide bushing (exhaust). The new guides have the I.D. (inside diameter) threaded and require either reaming (see 9.12.1.2) or honing (see 9.12.1.3) after installation in the cylinder head. The required procedure is as follows:
9.12.1.1 Install the 1 Y 469 and 1Y457 bushings into the bores in the cylinder head.
9.12.1.2 Ream the I.D. of both bushings in successive steps with the following reamers as required to obtain the clearances listed in 9.12.1.4: $12.52 \mathrm{~mm}(0.4930 \mathrm{in}$.), $12.55 \mathrm{~mm}(0.4940$ in.), 12.57 mm ( 0.4950 in .), $12.59 \mathrm{~mm}(0.4955 \mathrm{in}$.), 12.60 mm ( 0.4960 in .), and 12.61 mm ( 0.4965 in .).
9.12.1.3 Hone valve guide I.D. by using mandrel mounted honing stones. ${ }^{13,25}$ A continuous flow of honing oils is required. Turn the mandrel at slow speed ( 300 to $400 \mathrm{r} / \mathrm{min}$ ) until the final size, as listed in 9.12.1.4 is obtained. In general, honed guides produce more uniform stem-to-guide clearances, resulting in longer service life of valves and guides.
9.12.1.4 The reamed stem-to-guide clearance shall be 0.013 to $0.051 \mathrm{~mm}(0.0005$ to 0.0020 in .). The honed stem-to-guide clearance shall be 0.025 to 0.051 mm ( 0.0010 to 0.0020 in .). All measurements shall be made using a direct reading dial bore gage in the guide and micrometer on the valve stem. Valve stem drag shall not exceed 26 N ( 6 lbs ).
(1) Usual final size for intake guide: 12.59 or 12.60 mm ( 0.4955 or 0.4960 in .).
(2) Usual final size for exhaust guide: 12.57 or 12.59 mm (0.4950 or 0.4955 in .).
9.12.1.5 Thoroughly clean the reamed valve guide bushing with aliphatic naphtha or hot water, detergent, and stiff brush.
9.12.1.6 Grind the valve seats and faces in accordance with the dimensions for the 1 Y 73 engine as specified in the Caterpillar, Inc. Service Manual for Single Cylinder Oil Test Engine for Diesel Lubricants, Form No. SENR2074. ${ }^{13,16}$
9.12.1.7 Thoroughly clean the entire cylinder head and valves after grinding. Prelube the valve stems and guides with Mobil EF-411. ${ }^{13,24}$
9.12.1.8 Insert a rubber O-ring ( $\mathrm{p} / \mathrm{n} 8 \mathrm{~F} 9206$ ) into the 3H5867 valve spring retainer for all 1M-PC tests. Inspect this O-ring for hardness or cracking during cylinder head reconditioning and replace as necessary.
9.12.2 Precombustion Chamber Inspection and Maintenance-Maintain the orifice diameter of the precombustion chamber, Part Number 6 H 1528 , at $7.620 \pm 0.025 \mathrm{~mm}$ ( $3.300 \pm 0.001$ in.). Inspect and measure the orifice prior to installation of the cylinder head on the engine at the start of the

[^10]ASIM D 6618


1M-PC test method. Any measurement that is out of the 7.620 $\pm 0.025 \mathrm{~mm}(0.300 \pm 0.001 \mathrm{in}$.) diameter limit or shows any indication of ovality requires the replacement of the precombustion chamber.
9.13 Fuel Nozzle—Inspect the nozzle tip for carbon build-up and deformed surfaces, and replace questionable nozzles. Check the valve opening pressure before each test. Refer to the service manual for additional information.
9.14 Measurement-Measure the piston, rings, cylinder liner, and fuel timing before the start and at the completion of the test. Use a new piston, ring set, and cylinder liner for each new test. Measure and report compression ratio at the start of the test.
9.14.1 Initial Cylinder Liner Measurements-Assemble the cylinder head, block, and liner with specified stud nut torque. Measure the 1Y3590 liner in both transverse and longitudinal directions relative to the crankshaft to ensure that the out-ofround and taper conditions are within specified tolerances. Take measurements from underneath at 25 mm ( 1 in .) intervals for 23 cm ( 9 in .), starting 25 mm ( 1 in .) from the top of the liner. Determine the out-of-round condition for each $25 \mathrm{~mm}(1$ in.) interval: It shall not exceed $0.038 \mathrm{~mm}(0.0015 \mathrm{in}$.). The taper measurement compares the diameters from 25 mm ( 1 in .) to 23 cm ( 9 in .) for both transverse and longitudinal positions; the maximum difference shall not exceed $0.051 \mathrm{~mm}(0.0020$ in.). Measure liner surface finish. Record all measurements in Form 9, Fig. A2.12 (in Annex A2).
9.14.2 Post Test Wear Measurements for Liner Step Wear-At the end of the test, determine the liner wear step in both transverse and longitudinal directions by using a surface profile measurement. Remove deposits on the liner above the piston ring travel. Take transverse and longitudinal measurements at the wear step location approximately 20 to 25 mm ( 0.75 to 1 in .) from the top of the liner at four locations. Record the measurements as liner wear on Form 9, Fig. A2.11.
9.14.3 Ring End Gap-Determine wear on the rings by measuring the gap width before and after the test with the ring confined in a 13.02 cm ( 5.125 in .) inside diameter ring gage. Remove all deposits from the end of the rings after the deposit inspection and before the final ring gap measurements. Record the difference between these two measurements as ring gap increase or wear in Form 8, Fig. A2.11.

### 9.14.4 Ring Side Clearance:

9.14.4.1 Before and after the test, measure the piston ring side clearance of all rings. Make the after-test measurements before the rings are removed from the piston and with the accumulated deposits in place. Record all measurements in Form 8, Fig. A2.11. Measure side clearances as follows:
(1) Insert thickness (feeler) gage underneath the piston ring.
(2) Slide gage around the piston while holding ring in gently at the point of measurement to determine the minimum and maximum clearance to the nearest 0.013 mm ( 0.0005 in .)
(3) Use of gage requires firm but smooth horizontal pull. If gage movement is not firm or requires undue stress to move it, adjust the thickness up or down as required.
(4) Repeat 9.14.4.1 (1), (2), and (3), being careful not to force ring or gage against any deposit build up.
9.14.4.2 Calculate ring side clearance loss from:

$$
\begin{equation*}
\text { Max }_{\text {before }}-\operatorname{Max}_{\text {after }} \text { or } \operatorname{Min}_{\text {before }}-\operatorname{Min}_{\text {after }} \tag{1}
\end{equation*}
$$

which ever is larger.
9.14.4.3 Side clearance (new parts) is:
(1) Top ring, 0.185 mm maximum ( 0.0073 in .) to 0.114 mm minimum ( 0.0045 in .)
(2) Two intermediate rings, 0.122 mm maximum ( 0.0048 in.) to 0.076 mm minimum ( 0.0030 in .)
(3) Oil ring, 0.076 mm maximum ( 0.0030 in .) to 0.038 mm minimum ( 0.0015 in .)
9.14.5 Compression Ratio:
9.14.5.1 Determine the compression ratio before starting the test. Essential to measuring compression ratio is piston-to-head clearance. Determine this dimension by using 2.41 to 2.67 mm ( $0.095-0.105 \mathrm{in}$.) diameter lead shot. These lead pieces are held on the top of the piston with light grease. The location pattern for the lead shot is shown in Fig. A1.20. With the piston approximately halfway up on the stroke the cylinder head is installed and torqued to the standard torque specifications. Turn the engine over top center by hand, remove the head and block assembly, and measure the thickness of the lead shot to obtain the piston-to-head clearance. The average piston-to-head clearance shall measure $1.30 \pm 0.127 \mathrm{~mm}(0.051 \pm 0.005 \mathrm{in}$.).
9.14.5.2 Use multiple block gaskets (1Y3698) to adjust clearance. If the piston-to-head measurement exceeds the tolerance specification, check the crankshaft main and rod journals, connecting rod and main bearings, piston pin, and bushing for excessive wear. If these dimensions are not all within specifications, consult Caterpillar before any standard 1M-PC test is started.
9.14.6 Piston Ring Gap Location-Install the piston in the engine in accordance with standardized ring gap location. Use the 1Y3589 piston and 1Y3588 ring set. See Fig. A1.22 for ring gap locations.

## 10. Procedure

10.1 Engine Break-in—Weigh in $4.8 \pm 0.11 \mathrm{~kg}(10.6 \pm .25$ $\mathrm{lb})$ of oil. For non-reference tests, take a $240 \mathrm{~mL}(8 \mathrm{oz})$ sample of the oil for use in the $40^{\circ} \mathrm{C}$ initial viscosity measurement reported on Form 2, Fig. A2.3. Perform break-in per Table 6. When the cooldown is complete and the engine is still hot,

TABLE 6 Break-in Conditions

|  | Step $^{A}$ |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | $5^{B}$ |
| Speed, r/min | 1000 | 1000 | 1600 | 1800 | $1800 \pm 10$ |
|  |  | 7.5 | 17.1 | 24.6 | 31.3 |
| Load, kW (bhp) | Idle | $(10)$ | $(23)$ | $(33)$ | $(42)$ |
| Fuel rate | 1.36 | 2.27 | 4.72 | 6.88 | $8.13 \pm 0.07$ |
| kg/h (lb/h) | $(3.0)$ | $(5.0)$ | $(10.42)$ | $(15.16)$ | $(17.92 \pm 0.15)$ |
| Bearing oil temp. |  |  |  | 82.0 | $96.1 \pm 2.8$ |
| ${ }^{\circ} \mathrm{C}\left({ }^{\circ} \mathrm{F}\right)$ |  | $(180)$ | $(205 \pm 5)$ |  |  |
| Jet pressure | 158.6 | 158.6 | 158.6 | 165.5 | 165.5 |
| $\mathrm{kPa}($ psi), min. | $(23)$ | $(23)$ | $(23)$ | $(24)$ | $(24)$ |
| Water oil temp. |  |  | 71.0 | 71.0 | $87.8 \pm 2.8$ |
| ${ }^{\circ} \mathrm{C}\left({ }^{\circ} \mathrm{F}\right)$ |  | $(160)$ | $(160)$ | $(190 \pm 5)$ |  |
| Air inlet temp. |  |  |  | 76.7 | $123.9 \pm 2.8$ |
| C ( ${ }^{\circ} \mathrm{F}$ ) |  |  |  | $(170)$ | $(255 \pm 5)$ |
| Air inlet pressure | 118.0 | 118.0 | 135.0 | 135.0 | $179 \pm 1$ |
| kPa (in. Hg Absolute) | $(35.0)$ | $(35.0)$ | $(40.0)$ | $(40.0)$ | $(53 \pm 0.3)$ |
| Time, minutes | 5 | 5 | 10 | 20 | 20 |

[^11]drain the crankcase, governor housing, oil cooler, and lubricating oil filter housing for 30 min . Use the drain cocks provided.
10.2 Pre-Test Preparations:
10.2.1 Weigh $4.8 \pm 0.11 \mathrm{~kg}(10.6 \pm 0.25 \mathrm{lb})$ of oil into the engine.
10.2.2 Perform warm-up as described in 10.3.
10.3 Warm-up Procedure:
10.3.1 Perform Steps 1, 2, and 3 of Table 7 for all starts except break-in.
10.3.2 When finished with warm-up, turn on inlet air heating elements and bring stand to test conditions (see Table $1)$.
10.4 Operating Conditions-During this test, target all controlled parameters to the specified mean. Run the engine continuously for 120 h at the conditions shown in Table 1.
10.5 Periodic Measurements:
10.5.1 Except engine air flow rate, record the parameters listed in Table 1 hourly as snapshots. Record values as found before adjustments are made to correct to the specification mean. These recorded values show the engine conditions actually present at each hour of the test. (They are not averages computed from data logged during the test hour.) Make corrections to each hourly humidity reading for nonstandard barometric conditions, using additive correction factors derived from the perfect gas law equation (see 9.6.2).
10.5.2 Also record and report the following data:
10.5.2.1 Crankcase blowby, $\mathrm{m}^{3} / \mathrm{h}\left(\mathrm{ft}^{3} / \mathrm{h}\right)$, once each $12-\mathrm{h}$ period. (A minimal increase in crankcase pressure is allowed for a time period no greater than 4 min when switching from a normal operating system to the blowby measuring system.)
10.5.2.2 Engine load (should be approx. 31.3 kW or 42 bhp).
10.5.2.3 The weight of all oil added and drained and the engine hours at that time.
10.5.2.4 Document missing or bad test data on the test outlier sheet (see Form 7, Fig. A2.10). If a test has greater than four consecutive hours without data acquisition on any controlled parameter, the test will be considered operationally invalid. Note any alternate method of data acquisition in the comment section (Fig. A2.10).
10.6 Engine Oil Level-With the bayonet oil level gage housing lowered, use the following procedure for measuring the crankcase oil level:
10.6.1 Withdraw the bayonet gage and wipe free of oil.
10.6.2 Insert the bayonet gage with the numerals facing the operator.

| TABLE 7 Warm Up |  |  |  |
| :--- | :---: | :---: | :---: |
|  | 1 | 2 | 3 |
| Speed, r/min | 1000 | 1000 | 1600 |
| Load, kW (bhp) |  | 7.5 | 17.1 |
| Fuel rate | 1.36 | $(10)$ | $(23)$ |
| $\mathrm{kg} / \mathrm{h}$ (lb/h) | $(3.0)$ | 2.27 | 4.72 |
| Jet pressure | 158.6 | $(5.0)$ | $(10.42)$ |
| $\mathrm{kPa}(\mathrm{psi})$, min | $(23)$ | 158.6 | 158.6 |
| Water out temp. |  | $(23)$ | $(23)$ |
| $\mathrm{C}^{\circ}\left({ }^{\circ} \mathrm{F}\right)$ |  | 71.0 |  |
| Air inlet pressure | 118.0 | 118.0 | $(160)$ |
| kPa (in. Hg absolute) | $(35.0)$ | $(35.0)$ | 135.0 |
| Time, min | 5 | 10 | $(40.0)$ |

10.6.3 Count off 5 s .
10.6.4 Withdraw the bayonet gage and read the oil level.
10.7 Oil Addition Procedure-Use the following steps when making oil additions:
10.7.1 At the end of the run-in, drain all the engine oil for 30 min and weigh in $4.8 \pm 0.11 \mathrm{~kg}(10.6 \pm 0.25 \mathrm{lb})$ of fresh oil.
10.7.2 During the first hour of the test, when the oil temperature reaches $96 \pm 2.8^{\circ} \mathrm{C}\left(205 \pm 5^{\circ} \mathrm{F}\right)$, record the crankcase level as the Full Mark.
10.7.3 Calculate the following levels:
10.7.3.1 Drain Level is two units below the Full Mark.
10.7.3.2 Low Level is two and one-half units below the Full Mark.
10.7.3.3 Emergency Add Level is three units below the Full Mark.
10.7.4 At the end of each 12 -h period, check the crankcase oil level and perform the following:
10.7.4.1 If the oil level is above the Full Mark, drain to a level of Drain Level and weigh in $0.8 \pm 0.22 \mathrm{~kg}(1.76 \pm 0.05$ $\mathrm{lb})$ of fresh oil.
10.7.4.2 If the oil level is between the Full Mark and the Drain Level, drain oil from the engine until the oil level is at the Drain Level. Add $0.8 \pm 0.22 \mathrm{~kg}(1.76 \pm 0.05 \mathrm{lb})$ of fresh oil.
10.7.4.3 If the oil level is between Drain Level and Low Level, add $0.8 \pm 0.22 \mathrm{~kg}(1.76 \pm 0.05 \mathrm{lb})$ of fresh oil.
10.7.4.4 If the oil level is below the Low Level, add enough oil to the engine to bring it up to the Full Mark.
10.7.5 If the oil level falls below the Emergency Add Level at any time during the test, add $0.8 \pm 0.22 \mathrm{~kg}(1.76 \pm 0.05 \mathrm{lb})$ of fresh oil.
10.8 Cool-Down Procedure-Except for emergency (uncontrolled) stops, use the following procedure prior to all engine shutdowns including the break-in: Stop counting test time at the start of Stage 3 in Table 8. Turn off all heater elements and let air temperature cool normally.
10.9 Shutdowns:
10.9.1 Report the test hours and length of time down for all occurrences. If the cool-down procedure is not used, identify the shutdown as an emergency shutdown. In the event of an emergency shutdown, maintain a 2 h off-test condition for engine cooling before restarting. Maximum total allowable downtime for the duration of the test is 125 h . Minimize the total downtime of the test. To protect deposits, rotate the engine to top dead center of the compression stroke during shutdowns.
10.9.2 An excessive number of emergency or regularly

| TABLE 8 Cool Down |  |  |  |
| :--- | :---: | :---: | :---: |
|  | 3 | 2 | 1 |
| Speed, r/min | 1600 | 1000 | 1000 |
|  | 17.1 | 7.5 |  |
| Load, kW (bhp) | $(23)$ | $(10)$ | Idle |
| Fuel rate | 4.72 | 2.27 | 1.36 |
| kg/h (lb/h) | $(10.42)$ | $(5.0)$ | $(3.0)$ |
| Jet pressure | 158.6 | 158.6 | 158.6 |
| kPa (psi), min. | $(23)$ | $(23)$ | $(23)$ |
| Water out temp. | 71.0 |  |  |
| ${ }^{\circ} \mathrm{C}\left({ }^{\circ} \mathrm{F}\right)$ | $(160)$ |  |  |
| Air inlet pressure | 135.0 | 118.0 | 118.0 |
| kPa (in. Hg Absolute) | $(40.0)$ | $(35.0)$ | $(35.0)$ |
| Time, min | 5 | 5 | 5 |

scheduled shutdowns that reasonably could have been prevented will influence test acceptability. Pre-arrange schedules for tests with planned shutdowns (for reasons other than those normally permitted) with the TMC.
10.10 Fuel System—Bleed the fuel lines free of air prior to each test or if fuel is drained from the engine fuel system for any reason.
10.11 Brake Specific Oil Consumption (BSOC) Calculation-Calculate the BSOC for the test as follows:

$$
\begin{equation*}
\frac{(\Sigma \text { of adds })-(\Sigma \text { of drains })}{(120 \times \text { average engine power })} \tag{2}
\end{equation*}
$$

BSOC greater than $1.216 \mathrm{~g} / \mathrm{kW}-\mathrm{h}(0.002 \mathrm{lb} / \mathrm{bhp}-\mathrm{h})$ will invalidate the test. Plot each 12-h oil consumption point on Form 13, Fig. A2.16.

## 11. Inspection

11.1 Preparation-Use a clean, soft, dry cloth (for example, cotton outing flannel) free from any solvents or polishes, and wipe the test piston free of oil film.
11.2 Inspection-Inspect the piston and liner, and photograph the piston at the end of the test. Make a complete written description of the inspection. Remove all rings from the piston before it is photographed. Determine and record cylinder liner and piston ring wear. Inspect the piston, rings, and liner in accordance with the report forms shown in CRC Manual \#18 (1991), ${ }^{13,26}$ with the following exceptions:
11.2.1 Use a Sylvania 8-in. circular bulb, 20 W , cool white, Part \# FC8T9-CW-RS ${ }^{13,27}$ in the rating lamp.
11.2.2 Conduct routine maintenance, such as bulb replacement, fixture cleaning, and booth repainting, on a regular basis.
11.2.3 Have a probe available for use in identifying questionable carbon-like deposits.
11.2.4 Use the recommended 20 -segment template to obtain maximum precision. Each segment, which represents a $5 \%$ area, should not be broken down into areas smaller than $1 \%$.
11.2.5 Evaluate only three levels of carbon in the piston grooves. They are defined as follows:
11.2.5.1 Heavy Carbon - Carbon that will take up the whole space between the back of the ring and the back of the groove and the lesser levels of carbon that exhibit polished areas due to an excessive amount of carbon on the back of the ring with relative ring movement.
11.2.5.2 Medium Carbon-Carbon that will take up to between approximately one-quarter to just less than the whole space between the back of the ring and the back of the groove.
11.2.5.3 Light Carbon-Carbon that will take up to approximately one-quarter of the space between the back of the ring and the back of the groove.
11.2.6 Evaluate only two levels of carbon on the ring lands. They are defined as follows:
11.2.6.1 Heavy Carbon-Carbon that shows signs of rubbing or polishing, or both.
11.2.6.2 Light Carbon-Any other carbon deposit.

[^12]11.2.7 For standardization of the interpretation of clean, keep a new piston in the rating booth for comparison. Replace this piston daily with another new piston, if possible.
11.3 Rater Training-Each lab shall send, on a calendar year basis, a minimum of one heavy duty diesel piston rater to either the Task Force meeting held every spring or expanded Heavy Duty Piston Rating Workshop held every fall. Each rater shall rate a minimum of six diesel pistons. If this schedule is not suitable to a particular rater or test lab, then alternative arrangements shall be made as soon as possible to have the rater calibrated.
11.4 Referee Ratings-To quickly detect and correct any shifts in rater severity, all operationally valid calibration tests shall be refereed. Obtain referee ratings only from another calibrated test lab. Wrap all pistons being shipped for referee ratings in paper, place in plastic with the CRC approved desiccant, ${ }^{13,28}$ and then seal before placing in any other shipping container.

## 12. Calibration of Test Method

12.1 Requirements-To maintain test consistency and severity levels, engine test stand calibrations are required at regular intervals.
12.2 Reference Oils-The reference oils used to calibrate 1M-PC test stands have been formulated or selected to represent specific chemical types and performance levels. They are available from the ASTM TMC. The TMC will assign reference oils for calibration tests. These oils are supplied under code numbers (blind reference oils).

### 12.3 Test Numbering:

12.3.1 Number each 1M-PC test to identify the test stand number and the test run number. Number all runs sequentially. Append repeat calibration runs with a letter (also sequential). Maintain the letter suffix sequencing for each test type calibration until the calibration has been accepted. Any test start, regardless of type, increments the run number. Test start is defined in 12.4.
12.3.2 An example of test numbering:

|  |  | 1M-PC Test |  | Text $X$ |
| :---: | :---: | :---: | :---: | :---: |
| 1st Test | 1 | Ref. Fail |  |  |
| 2nd Test | 2A | Ref. Fail |  |  |
| 3rd Test | 3B | Ref. Fail |  |  |
| 4th Test |  |  | 4 | Ref. Fail |
| 5th Test |  |  | 5A | Ref. Pass |
| 6th Test | 6C | Ref. Pass |  |  |
| 7th Test | 7 | Candidate |  |  |
| 8th Test |  |  | 8 | Candidate |

12.4 Definition of Test—A test (or test start) is defined, for purposes of this test method, as any engine test time accumulated in accordance with this test method.
12.5 New Laboratories and New Test Stands:
12.5.1 New Test Stands-A new stand is defined as a test engine and support hardware that has never been previously calibrated under this test method.
12.5.2 New Laboratory-A new laboratory shall have two calibration test passes on approved reference oils to be considered valid.

[^13]12.5.3 Special Circumstances-A laboratory not running a 1M-PC test for twelve months from the start of the last test is considered a new laboratory. Under special circumstances (that is, extended downtime due to industry-wide parts shortage or fuel outages) the TMC may extend the lapsed time requirement. Annotate non-reference tests conducted during an extended time allowance on the comment form (Fig A2.10).
12.6 Frequency of Calibration Tests:
12.6.1 A calibration test on a reference oil assigned by the TMC is required after no more than 14 test starts or after six months from the start date of the last acceptable calibration test (whichever comes first). The $1 \mathrm{M}-\mathrm{PC}$ calibration run is not counted as one of the 14 test starts; however, all other test starts are counted. The TMC is permitted to move up or extend reference tests to enhance reference test program design and test severity monitoring. If a reference test calibration period is extended beyond the normal duration, any non-reference tests shall include a notation of this fact in the comments section (Fig. A2.10). Additionally, written confirmation from the TMC shall be attached to the report.
12.6.2 Any non-reference testing is to be completed prior to the expiration of the present calibration. In cases in which a non-reference test does not complete when expected due to unscheduled shutdowns, the calibration will continue to the end of the test.
12.7 Specified Test Parameters-The specified test parameters for determination of test acceptance are:
12.7.1 Top groove fill, percent area.
12.7.2 Weighted total deposits, demerits.
12.8 Acceptance of Calibration Tests-Refer to the TMC's Lubricant Test Monitoring System (LTMS) for calibration test targets and acceptance criteria.
12.9 Failing Reference Oil Calibration Tests:
12.9.1 Failure of a calibration test to meet test acceptance bands can indicate a testing stand problem, testing laboratory problem, or industry-wide problem, or it can be a false alarm. When this occurs, the laboratory, in conjunction with the TMC, must attempt to determine the problem source.
12.9.2 In the determination of the problem, TMC will decide, with input as needed from industry expertise (testing laboratories, test developer, ASTM Technical Guidance Committee, Surveillance Panel, and so forth), if the reason for any unacceptable blind reference oil test is isolated to one particular stand or related to other stands. If it is decided that the problem is isolated to an individual stand, calibrated testing on other stands can continue throughout the laboratory. Alternatively, if it is decided that more than one stand may be involved, the involved stands will not be considered calibrated until the problem is identified and corrected and an acceptable reference oil test is completed in one of the involved stands.
12.10 Non-Standard Tests-If non-standard tests are conducted on the referenced test stand, the stand may, at the discretion of the TMC, be required to be recalibrated prior to running standard tests.
12.11 Severity Adjustments and Control Charting:
12.11.1 Severity Adjustments-This test method incorporates the use of a surveillance panel accepted method of calculating a severity adjustment (SA) for non-reference test
results. A control chart technique, described in 12.11.2, has been selected for the purpose of identifying when a bias becomes significant. When a significant bias is identified, an SA is applied to non-reference test results. The SA remains in effect until subsequent calibration test results indicate that the bias is no longer significant. SAs are calculated and applied on a laboratory basis.
12.11.2 Control Chart Technique for SAs-Apply an exponentially weighted moving average (EWMA) technique to standardized calibration test results. Standardize values using $\Delta / s$ (result - target) / standard deviation). The targets and standard deviations are published by the TMC. Include all operationally valid calibration tests in a laboratory control chart. Chart tests in order of completion. Record completion of tests by end of test (EOT) date and time. Report EOT as hour and minute in accordance with the $24-\mathrm{h}$ clock ( $1 \mathrm{a} . \mathrm{m} .=1: 00$, 1 p.m $=13: 00$ ). Reporting test completion time enables the TMC to properly order tests that are completed on the same day for industry plotting purposes. Report calibration tests to the TMC in order of test completion. A minimum of two tests is required to initialize a control chart. Calculate EWMA values, using the following equation:
\[

$$
\begin{equation*}
Z_{i}=\lambda Y_{i}+(1-\lambda) Z_{i-1} \tag{3}
\end{equation*}
$$

\]

where:
$Z_{O}=0$,
$Y_{i}=$ standardized test result,
$Z_{i}=$ EWMA of the standardized test result at test order $i$, and
$\lambda=$ the appropriate $\lambda$ from the LTMS document.
If the absolute value of EWMA, rounded to three places after the decimal, exceeds the alarm limit established in the LTMS document, then apply an SA to subsequent non-reference results.
12.11.3 Calculation of SA-Compute and apply EWMA and SA values as shown in the following example. Please note that test targets are presented for example only.
12.11.3.1 TGF Severity Adjustment:

Applicable Test Targets: Mean $=40.8$; Standard Deviation $=15.9 ;$ TGF $=55 \mathrm{Z}_{1}=$ 0.897

Standard Test Result: $\mathrm{Y}_{2}=($ TGF - Mean $) /$ STD $=0.893$
Alarm Limit: 0.653

$$
\begin{equation*}
\text { EWMA: } Z_{2}=0.2 Y_{2}+0.8 Z_{1}=0.896 \tag{4}
\end{equation*}
$$

Since $0.896>0.653$, an SA shall be applied: $\mathrm{SA}=-1 *$ EWMA * STD (in the above example, $S A=-14$ ). For TGF, the SA is rounded to a whole percent; for WTD, it is rounded to one decimal place. Enter this number on Form 1, Fig. A2.2, in the appropriate Lab Severity Adjustment box and add it to the non-reference test result. An SA will remain in effect until the next calibration test. At that time, calculate a new EWMA and SA.
12.12 Test Reporting:
12.12.1 Report Forms-All report forms making up the 1M-PC final report are given in Annex A2. Additionally, the control chart summary page sent to the lab from the TMC shall be attached to each calibration test report. An example of this and other forms are shown in Fig. X2.1 of Appendix X2 and Fig. X3.1 of Appendix X3.
12.12.2 Deviation Percent and Offset Percent CalculationOffset percent measures how close any given test parameter is run to the target mean. Deviation percent indicates excursions made by any given parameter outside the minimum or maximum limit. Record these values on Form 3 (see Fig. A2.4), and calculate them as follows:
12.12.2.1 Round recorded values, if necessary, in accordance with the specifications listed on the U.S. Customary System (USCS) and SI specifications given in Table 3.
12.12.2.2 Use the test specifications and tolerances listed in Table 3 for the percent calculations.
12.12.2.3 Calculate the percent out and percent off, using the same units as the recorded data. For example, if the test is operated in USCS units, calculate the percentages using USCS units. Do not convert the units before figuring the percentages.
12.12.2.4 The logging frequency used for calculating the percentages will be at the discretion of the laboratory, but shall be at least hourly.
12.12.2.5 Include an explanation for any data used in the calculation of the percentages that are edited. List the data before they are edited, the new value, and the explanation for the change in comments or outlier section of the test report (Fig A2.10).
12.12.2.6 Include these percent calculations within each test report on Form 3, Fig. A2.4.
12.12.2.7 Carry each percent out calculation to three significant digits (see Table 9).
12.12.2.8 Round the calculated average used in the percent off calculation to the measurement resolution shown in Table 2. See example in Table 9.
12.12.2.9 Round the percent out summation and percent off results to the minimum measurement resolution listed in Table 2 (see example in Table 9).

## TABLE 9 Example $^{A}$ of Percent Out and Percent Off Calculations

Note 1 -Percent out Summation $=8.33$ (Round to 0.01 ).
Average of the rounded values $=128.6$ (round to 0.1$)$.
Percent offset $=15.5$ (round to 0.1 ).

| Test Hours | Raw Value <br> $\mathrm{g} / \mathrm{kg}$ | Rounded Value <br> $\mathrm{g} / \mathrm{kg}$ | \% Out for Each <br> Value Rounded to <br> 0.001 |
| :---: | :---: | :---: | :---: |
| 1 | 18.65 | 18.7 |  |
| 2 | 18.65 | 18.7 |  |
| 3 | 18.55 | 18.6 |  |
| 4 | 17.96 | 18.0 |  |
| 5 | 18.28 | 18.3 |  |
| 6 | 17.96 | 18.0 |  |
| 7 | 18.00 | 18.0 |  |
| 8 | 17.73 | 17.7 |  |
| 9 | 17.59 | 17.6 | 0.053 |
| 10 | 16.90 | 16.9 | 0.437 |
| 11 | 15.99 | 16.0 |  |
| 12 | 15.21 | 15.2 | 0.067 |
| 13 | 18.28 | 18.3 | 0.221 |
| 14 | 18.95 | 19.0 | 0.081 |
| 15 | 19.27 | 19.3 | 0.067 |
| 16 | 19.64 | 19.6 | 0.221 |
| 17 | 19.95 | 20.0 |  |
| 18 | 19.67 | 19.7 |  |
| 19 | 19.64 | 19.6 |  |
| 20 | 19.95 | 20.0 |  |
| 21 | 18.06 | 18.1 |  |

[^14]Note 3-Use ASTM rounding rules when carrying out 12.12.2.7 through 12.12.2.9.
12.12.2.10 An example of the calculation for percent out for test hour eleven, using the formula shown in 12.12.2.11, is as follows:

$$
\begin{equation*}
\% \text { Out }=\frac{\frac{112-113}{12} \times \frac{60}{60} \times 100}{120}=0.069 \tag{5}
\end{equation*}
$$

12.12.2.11 Use the following formula to calculate the percent out:

$$
\begin{equation*}
\% \text { Out }=\frac{\frac{|A-B|}{C} \times \frac{D}{60} \times 100}{120} \tag{6}
\end{equation*}
$$

where:
$A=$ recorded test measurement of parameter that is beyond test limits prior to any corrective action,
$B=$ upper test spec if the measured parameter is out on the high side, and the lower test spec if it is out on the low side,
$C=$ specification tolerance of the measured parameter,
$D=$ length of deviation in minutes (It cannot be less than the logging frequency.),
$60=$ conversion factor for $\mathrm{min} / \mathrm{h}$, and
$100=$ conversion factor for percentage units.
Calculate the percent out for each measured parameter, based on its logging frequency. Sum the individual percent out's to arrive at the final percent out for judging test validity (see Table 10).
12.12.2.12 Use the following formula to calculate the percent off:

$$
\begin{equation*}
\% \text { Off }=\frac{\mid \bar{X}-\text { SPEC } \mid \times 100}{\text { SPEC RANGE }} \tag{7}
\end{equation*}
$$

where:
$\bar{X}$
$=$ average of all readings of the parameter for the entire test duration, and
SPEC RANGE $=$ the upper spec minus the lower spec, or two times the spec tolerance.
12.12.3 Electronic Data Communication and Data Dictionary-Use the data dictionary given in Annex A3 (see Fig. A3.1) for any electronic transmission of data to the TMC. The data dictionary lists all variable names given to all fields as well as the important information about those fields.
12.13 Reporting Reference Results-Transmit the calibration test results by facsimile to the ASTM TMC immediately after completion of test analysis, using the Cover Sheet and Forms 1, 2, 3, and 7 (see Figs. A2.1, A2.2, A2.3, A2.4, and A2.10 respectively). The lab shall send this fax within seven days of EOT for the test to be considered valid. Lab rating will be considered the primary rating; referee ratings are secondary. Report referee results to the TMC on Form 5A, Fig. A2.8, within ten working days of the test completion. The TMC will review all calibration test results to determine test acceptability. If the test is judged acceptable, the reference oil code along with the industry average for the reference oil, will be disclosed by the TMC. In the event the reference oil test is not acceptable, an explanation of the problem relating to the failure is to be provided by the test laboratory. If the problem is not

TABLE 10 Allowable Limits for Percent Out and Percent Off

| Controlled Parameter ${ }^{A}$ | Allowable \% Out | Allowable \% Off |
| :--- | :---: | :---: |
| Speed | 5 | 20 |
| Fuel flow | 10 | 25 |
| Humidity | 10 | 25 |
| Coolant flow | 5 | 25 |
| Temperatures |  |  |
| Coolant out | 5 | 20 |
| Oil to bearing | 5 | 20 |
| Intake air | 5 | 20 |
| Pressures |  |  |
| Oil jet | 5 | 25 |
| Intake air | 10 | 25 |
| Exhaust | 10 | 25 |
| Fuel at filter housing | 5 | 20 |
| Crankcase vacuum | 10 | 20 |

${ }^{A}$ The parameters in this table shall be used to judge test validity based on operational control. Any parameter for a given test with a percent out or percent off that is greater than the specifications listed shall be considered to be operated in an invalid manner.
obvious, all test-related equipment shall be rechecked. If no explanation of the problem is presented, it will be assumed that the problem is laboratory-related and another reference oil will be assigned. One copy of the standard final test report with photographs for each $1 \mathrm{M}-\mathrm{PC}$ reference oil test shall be forwarded within 30 days of test completion (or the test will not be considered valid) to Caterpillar Inc. ${ }^{13,29}$ and ASTM TMC. ${ }^{2}$
12.14 Analysis of Reference Oils-Do not submit reference oils to physical or chemical analyses for identification purposes. Identifying the oils by analyses could undermine the confidentiality required to operate an effective blind reference oil system. Therefore, reference oils are supplied with the explicit understanding that they will not be subjected to analyses other than those specified within this test method unless specifically authorized by the ASTM TMC. In such cases in which analyses are authorized, supply written confirmation of the circumstances involved, the data obtained, and the name of the person authorizing the analysis to the ASTM TMC.

## 13. Precision and Bias

13.1 Precision - To aid the potential user of this test method to assess the variability that can be expected between test results when the test method is used in one or more calibrated laboratories, the following precision information, as shown in Table 11 has been developed. Test precision is established on

[^15]TABLE 11 1M-PC Reference Oil Precision Statistics ${ }^{A}$
Note 1—Reported units.

|  | Intermediate Precision |  | Reproducibility |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\mathrm{S}_{\mathrm{i} . \mathrm{p} .}$ | i.p. | $\mathrm{S}_{\mathrm{R}}$ | R |
| Top groove fill, \% | 17.0 | 47.6 | 17.8 | 49.8 |
| Weighted total demerits | 43.3 | 121.2 | 45.0 | 126.0 |

${ }^{\text {A }}$ These statistics are based on ASTM Test Monitoring Reference Oils 873 and 873-1. $\mathrm{S}_{\text {i.p. }}$ is the intermediate precision standard deviation, and $\mathrm{S}_{\mathrm{R}}$ is the reproducibility standard deviation.
the basis of reference oil test results (for operationally valid tests) monitored by the ASTM TMC. The test precision is reviewed semi-annually by the 1M-PC Surveillance Panel and is available on request from TMC.
13.1.1 Intermediate Precision (i.p.) (formerly called repeatability)—The difference between two results obtained by the same laboratory under constant operating conditions on the same oil. In the normal and correct conduct of this test method, results would exceed this value only one time in twenty.
13.1.2 Reproducibility-The difference between two single and independent results obtained by different operators working in different laboratories on the same oil. In the normal and correct conduct of this test method, results would exceed this value only one time in twenty.
13.2 Bias-Bias is determined by applying an accepted statistical technique to reference oil test results, and when a significant bias is determined, an SA is permitted for nonreference oil test results (see 12.11; also refer to ASTM TMC Memorandum 94-200)

## 14. Keywords

14.1 diesel engines; heavy-duty performance; 1M-PC; ring belt deposits; single cylinder test

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## ANNEXES

## (Mandatory Information)

## A1. SCHEMATICS

A1.1 See Table A1.1 for the bill of material for surge chamber and air heater assembly.

A1.2 See Figs. A1.1-A1.35 for schematic drawings and information relating to the engine used in this test method.

TABLE A1.1 Bill of Material - Surge Chamber and Air Heater Assembly
Nоте 1-All dimensions are in inches unless otherwise specified.

| Item No. | Name | Caterpiller <br> Tractor Co. Part No. | Description | No. Req'd | Ref Fig. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1-1 | Surge chamber \& heater Assembly |  |  | 1 | Fig. A1. 23 |
| 1-2 | Bolt | L1648 | $3 / 8-24$ thd 2.50 long $^{\text {A }}$ | 1 |  |
| 1-4 | Thermostatic switch |  |  | 2 |  |
| 1-5 | Lockwasher | 3B4506 | Std. for 0.375 dia bolt | 20 |  |
| 1-6 | Bolt | 2A4996 | $3 / 8-24$ thd 1.375 long $^{\text {B }}$ | 20 |  |
| 1-7 | Pressure relief valve |  |  | 1 |  |
| 1-8 | Gasket |  | 0.0312 thick ${ }^{\text {c }}$ | 1 |  |
| 1-9 | Mounting plate |  | $20 \times 12 \times 0.0625$ thick SAE steel | 1 |  |
| 1-10 | Spacer | 8B7430 | 0.750 OD 0.359 ID 0.531 thick SAE steel | 4 |  |
| 1-11 | Bolt | L1590 | $1 / 4-28$ thd 1.125 long | 4 |  |
| 1-12 | Lockwasher | 3B4504 | Std. for 0.250 dia bolt | 4 |  |
| 1-13 | Nut | 1B4201 | $1 / 4-28$ thd | 4 |  |
| 1-14 | Electrical junction box |  | $12 \times 18 \times 4$ std pull box w/hinged cover $^{D}$ | 1 |  |
| 1-15 | Strip heater |  |  | 24 |  |
| 1-16 | Gasket |  | 0.0312 thick $^{\text {c }}$ | 1 |  |
| 2-1 | Assembly |  |  | 1 | Fig. A1. 24 |
| 2-2 | Top ring |  |  | 1 |  |
| 2-3 | Bottom plate |  |  | 1 |  |
| 2-4 | Strap-surge chamber |  |  | 2 |  |
| 2-5 | Hook |  |  | 2 |  |
| 2-6 | Pad |  |  | 1 |  |
| 3-1 | Assembly |  |  | 1 | Fig. A1. 25 |
| 3-2 | Top cover |  |  | 1 |  |
| 3-3 | Inner bracket |  |  | 1 |  |
| 3-4 | Outer bracket |  |  | 1 |  |
| 4-1 | Terminal assembly |  |  | 5 | Fig. A1. 26 |
| 4-2 | Nut |  | 7/16-14 thd SAE 73 brass | 29 |  |
| 4-3 | Washer |  | Std. for 0.437 dia. bolt | 10 |  |
| 4-4 | Insulator |  | 1.250 OD 0.453 ID . 187 thick Synthane | 5 |  |
| 4-5 | Stud |  | 7/16-14 thd 3 long brass | 5 |  |
| 4-6 | Collar |  |  | 5 |  |
| 4-7 | Insulator assembly |  |  | 48 |  |
| 4-8 | Washer |  | . 750 OD . 265 ID 0.125 thick Mica | 48 |  |
| 4-9 | Insulator |  | . 500 OD . 265 ID 0.0625 thick Synthane | 48 |  |
| 4-10 | Insulator |  | $1.687 \times 1 \times 0.0625$ w/0.265 hold Mica | 48 |  |
| 4-11 | Bolt |  | $1 / 4-20$ thd 1 long | 48 |  |
| 4-12 | Washer |  | Std. for 0.250 dia bolt | 48 |  |
| 4-13 | Nut |  | Std. for $1 / 420$ thd | 48 |  |
| 4-14 | Electric cable cover |  |  | 1 |  |
| 4-15 | Terminal connector |  |  | As |  |
|  |  |  |  | Req'd |  |
| 4-16 | Lower bracket assembly |  |  | 1 |  |

[^16]

FIG. A1.1 1 Y73 Engine Arrangement


FIG. A1.2 Suggested Piston Cooling Nozzle Pressure Pick-up


Note 1-1—Material-mild steel.
2-Two required per engine.
3-Replace mounting bolts 8B5144 with two 6F7024 bolts.
FIG. A1.3 Bayonet Oil Gage Lowering Spacer

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FIG. A1.4 Crankcase Pressure Control Valve Installation


Note $1-3 / 8$ in. I.D. Aeroquip hose type 2556-6.
FIG. A1.5 Standardized Engine Fuel System

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FIG. A1.6 Pressurized 5-in. Cooling Tower


Note 1—Legend:

1. $1 / 4 \mathrm{in}$. NPT-TO-No. 4 AN (male connector)
2. No. 4 Hose
3. Pressure gage 0-15 PSIG
4. Pressure regulator (self bleeding)
5. Radiator cap 15-16 PSIG
6. Radiator filler neck
7. Overflow tube (optional)
8. Overflow tank (optional)

Note 2—If the system builds to greater than regulator setting, then condensate will back-flow through regulator.
FIG. A1.7 Cooling System Modification


FIG. A1.8 Recommended Cooling System


Note 1-Legend:

1. Line to fuel cam.
2. Line to rockerarm.
3. Line to accessory shaft.
4. Rear cam bearing
5. Line to piston cooling jet
6. Line, jet pressure pickup.
7. Manifold
8. Oil filter.
9. Oil pan.
10. Bypass line.
11. Oil pump.
12. Oil pump supply line.
13. Oil cooler assembly.

FIG. A1.9 Oil Flow Schematic

$\begin{array}{ll}\text { NSTALL: } \quad 1-2 H 3751 \text { BOLT }\left(1-1 / 8-12 \times 2-1 / 22^{\prime}\right) \\ & 1-583265 \text { GASKET }\end{array}$
Note 1—If desired, bolt thread may be sealed with 7M7456 bearing mount.
FIG. A1.10 Oil Pump Relief Valve Plug


FIG. A1.11 Remote Mount Oil Pump Relief Valve


Note 1-Use 1 Y3698 gasket as pattern for bolt hole locations. FIG. A1.12 Clear Plastic Cover


Note 1-Portable cart, optional.
FIG. A1.13 Typical Flushing Pump Arrangement


FIG. A1.14 Crankcase/Governor Housing Sprayer


FIG. A1.15 Governor Housing Cover Modification


FIG. A1.16 Front Cover Sprayer

(B)

FIG. A1.17 Flushing Components Location


FIG. A1.18 Rocker Oil Line Blocking-off Fitting


FIG. A1.19 Jet Alignment Fixture


Note 1—Lead shot are oriented with axis of piston as viewed from the top. FIG. A1.20 Placement Location of Lead Shot


FIG. A1.21 Compression Ratio Versus Piston to Head Clearance

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FIG. A1.23 Surge Chamber and Air Heater Assembly (1-1)


FIG. A1.24 Air Barrel Construction


FIG. A1.24 Air Barrel Construction (continued)

FIG. A1.24 Air Barrel Construction (continued)


FIG. A1.25 Wiring Diagram for 1Y38 Surge Chamber and Air Heater Assembly

A1.26 Air Transfer Pipe
A1.26.1 The IY73 Engine Arrangement or the IY7500 Engine Arrangement modified with the IY7999 High Speed Change-Over Group requires an air transfer pipe as illustrated in Figs. A1.26-A1.29. It consists of two sections of 2-in. black iron pipe (or equivalent). The 1Y73 Flange, part of the section attached to the engine, is available as a standard part.

A1.26.2 A slight bend may be made in one of the sections as long as the inner surface is not rippled and the inside circularity is not distorted. If a more pronounced bend is required, a $45^{\circ}$ or $90^{\circ}$ standard welding pipe fitting, illustrated in Fig. A1.27, is recommended. The centerline pipe distance of the temperature and pressure bosses from the flange face, shown in Figs. A1.28 and A1.29, should be maintained regardless of pipe curvature in this area.

A1.26.3 To isolate the surge chamber from engine vibration the two sections are connected with a length of rubber hose as shown in Fig. A1.27. Any other suitable isolation device may be employed that has an inside diameter of $6.35 \pm 1.3 \mathrm{~cm}$ ( $2.5 \pm 0.5 \mathrm{in}$.) and does not alter the total pipe length of $76 \pm 1.3 \mathrm{~cm}$ (31.25 $\pm 0.5 \mathrm{in}$.).

A1.26.4 The IY7500 Engine Arrangement modified with the IY7630 Supercharger Change-Over Group uses an air transfer pipe identical to the one just described except for the flange on the section attached to the engine. The IY217 Flange shown in Fig. A1.29, available as a standard part, is used in constructing this section.


FIG. A1.26 Alternate Air Transfer Pipe Arrangements


FIG. A1.28 Air Transfer Pipe

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FIG. A1.28 Air Transfer Pipe (continued)



SAE 1020 STEEL
FIG. A1.29 Surge Chamber Outlet Pipe Assembly

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COUPLING installation
FIG. A1.30 Exhaust Thermocouple Location


ONE
FIG. A1.31 Exhaust Barrel Diagram


FIG. A1.32 Exhaust Piping


FIG. A1.33 Exhaust Barrel Flange


FIG. A1.34 Exhaust Bellows

This assembly is essentially a pressure vessel with internal electric heating elements. The general dimensions of the surge chamber are:

Volume $209 \mathrm{~L}\left(7.37 \mathrm{ft}^{3}\right)$
Inside Diameter........................................................................ 53 cm (21 in)
Inside Height............................................................................... 93 cm (36.75 in)
If individual requirements or local building codes necessitate changes in the design, the following modifications are permissible:

1. Volume may vary from seven to eight cubic feet.
2. Inside diameter may vary from $48-58 \mathrm{~cm}$ (19 to 23 in$)$.
3. Inside height will be a function of the volume and inside diameter selected.
4. Inlet and outlet fittings may be located anywhere except directly opposite each other.
5. The type and arrangement of heating controls may be determined by local conditions.
6. The chamber may be located in any of a number of positions relative to the engine as long as:
(a) The length of the air transfer pipe is $76 \pm 1.3 \mathrm{~cm}$ ( $31.25 \pm 0.5 \mathrm{in}$ ) from the face of the surge chamber mounting pad to the inlet port face of the cylinder head.
(b) The air transfer pipe contains only one bend.
(c) The one bend shall not exceed 90 degrees.
7. A stand may be constructed to raise the chamber to the proper height depending upon the engine arrangement and mounting.

FIG. A1.35 1Y38 Surge Chamber and Air Heater Assembly

## A2. REPORT FORMS

A2.1 For Report Forms 1 through 17, see Figs. A2.1-A2.20.

CATERPILLAR 1M-PC
FINAL REPORT COVER SHEET

VERSION 19980922

CONDUCTED FOR
TSTSPON1
TSTSPON2

| LABVALID | $V=$ VALID |
| :--- | :--- |
|  | I = INVALID |
|  | N = RESULTS CAN NOT BE INTERPRETED AS REPRESENTATIVE <br>  <br>  <br>  <br>  <br> OF OIL PERFORMANCE (NON-REFERENCE OIL) AND SHALL NOT <br> BE USED IN DETERMINING AN AVERAGE TEST RESULT USING <br> MULTIPLE TEST CRITERIA |


| Test Number |  |  |  |
| :--- | :--- | :--- | :---: |
| Test Stand: STAND | Engine Run \#: | ENRUN |  |
| EOT Time: EOTTME | EOT Date: DTCOMP |  |  |
| Oil Code ${ }^{\text {A }: ~ C M I R / O I L C O D E ~}$ |  |  |  |
| Formulation/Stand Code: FORM | ALTCODE2 | ALTCODE3 |  |
| Alternate Codes: ALTCODE1 |  |  |  |

In my opinion this test OPVALID Procedure and the appropriate amendments throus included in the report describe the anomalies associated with this test.
${ }^{\text {A }}$ CMIR or Non-Reference Oil Code


FIG. A2.1 Final Report Cover Sheet

| LAB: $\angle A B$ | EOT DATE: | DTCOMP | END TIME: EOTTIME |
| :--- | :--- | :--- | :--- | :--- |
| STAND: STAND | RUN NUMBER: | ENRUN |  |
| FORMULATION/STAND CODE: | FORM |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |  |
| START DATE: DTSTRT | TOTAL TEST LENGTH: TESTLEN | TMC OIL TYPE: IND |  |
| LABORATORY INTERNAL OIL CODE: | LABOCODE |  |  |


|  | CORRECTION EFFECTIVE DATE | WTD | $\begin{gathered} \text { TGF } \\ \% \end{gathered}$ | BSOC <br> g/k W-h |
| :---: | :---: | :---: | :---: | :---: |
| UNADJUSTED LAB RATING |  | WTD | TGF | BSOC |
| INDUSTRY CORRECTION (IF ANY) | DATECF | WTDCF | TGFCF | BSOCCF |
| SUBTOTAL |  | WTDCOR | TGFCOR | BSOCCOR |
| LAB SEVERITY ADJUSTMENT (IF ANY) ${ }^{\text {A }}$ | DATESA | WTDSA | TGFSA | BSOCSA |
| TOTAL |  | WTDFNL | TGFFNL | BSOCFNL |


|  | EFFECTIVE DATE | WTD | $\begin{gathered} \text { TGF } \\ \% \end{gathered}$ | $\begin{aligned} & \text { BSOC } \\ & \mathrm{g} / \mathrm{kW} \text {-h } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| TEST TARGET MEAN ${ }^{\text {B }}$ | EFFDATE | WTDM | TGFM | BSOCM |
| TEST TARGET STD ${ }^{\text {B }}$ | EFFDATE | WTDS | TGFS | BSOCS |
|  | REFEREE LAB | WTD | $\begin{gathered} \text { TGF } \\ \% \end{gathered}$ |  |
| REFEREE RATINGS | RRLAB | RRWTD | RRTGF |  |


|  | TOP | INT. 1 | INT. 2 | OIL | PISTON | LINER |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RING LOSS OF SIDE CLEARANCE (mm) | LSCTOP | LSCINT1 | LSCINT2 | LSCOIL |  |  |
| RING END GAP INCREASE (mm) | RINGGTI | RINGGIII | RINGGI2I | RINGGOI |  |  |
| IS THE RING STUCK? | STUCKTOP | STUCKIN1 | STUCKIN2 | STUCKOIL |  |  |
| SCUFFED AREA \% | SCUFFTOP | SCUFFINT | SCUFFIN2 | SCUFFOIL | SCUFFPIS | SCUFFLIN |
| AVERAGE WEAR STEP (mm) | \%. | \%. | ஊॉ.\%』 |  |  | AWEARST |

[^17]FIG. A2.2 Form 1-Test Report Summary

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[^18](1) AND (2) NUMBER ON PARTS BOX YELLOW LABEL

FIG. A2.3 Form 2-Operational Summary

| LAB: $\angle A B$ | EOT DATE: DTCOMP | END TIME: EOTTIME |
| :--- | :--- | :--- | :--- |
| STAND: STAND | RUN NUMBER: ENRUN |  |
| FORMULATION/STAND CODE: FORM |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |


| CONTROMLD PABAMETER | ALUOWABLE $\%$ OUT | $\begin{aligned} & \text { THIS IESH } \\ & \text { \% OMH. } \end{aligned}$ | $\begin{aligned} & \text { AMOWABLE } \\ & \% \% \text { ork\%\%. } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| SPEED | 5 | RPMOUT | 20 | RPMOFF |
| FUEL FLOW | 10 | FFLOOUT | 25 | FFLOOFF |
| HUMIDITY | 10 | HUMOUT | 25 | HUMOFF |
| COOLANT FLOW | 5 | COLFOUT | 25 | COLFOFF |
| TEMPERATIURES |  |  |  |  |
| COOLANT OUT | 5 | COTOUT | 20 | COTOFF |
| OIL TO BEARING | 5 | OBRGOUT | 20 | OBRGOFF |
| INTAKE AIR | 5 | AIRTOUT | 20 | AIRTOFF |
| PRESSURES |  |  |  |  |
| OIL JET | 5 | OJETOUT | 25 | OJETOFF |
| INTAKE AIR | 10 | AIRPOUT | 25 | AIRPOFF |
| EXHAUST | 10 | EXPOUT | 25 | EXPOFF |
| FUEL AT FILTER HOUSING | 5 | FFILOUT | 20 | FFILOFF |
| CRANKCASE VACUUM | 10 | CCVOUT | 20 | CCVOFF |

FIG. A2.4 Form 3-Operational Summary - Offset and Deviation


FIG. A2.5 Form 4-Piston Rating Summary

| LAB: $\quad$ LAB | EOT DATE: DTCOMP | END TIME: EOTTIME |
| :--- | :--- | :--- | :--- |
| STAND: STAND | RUN NUMBER: ENRUN |  |
| FORMULATION/STAND CODE: FORM |  |  |
| OILCODE/CMIR: $\quad$ CMIR/OILCODE |  |  |

Note 1—Refer to Fig. X2.1 of Appendix X2 for an example of a Piston Rating Worksheet. FIG. A2.6 Form 4A—Piston Rating Worksheet

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FIG. A2.7 Form 5-Piston Rating Breakdown

## TEST IDENTIFICATION



## TOTAL PISTON RATINGS SUMMARY



FIG. A2.8 Form 5A—Referee Rating


FIG. A2.9 Form 6-CF-2 Rating



FIG. A2.10 Form 7—Unscheduled Downtime and Maintenance Summary

| LAB: $L A B$ | EOT DATE: DTCOMP | END TIME: EOTTIME |
| :--- | :--- | :--- |
| STAND: STAND | RUN NUMBER: ENRUN |  |
| FORMULATION/STAND CODE: FORM |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |


| RING GAPS(mm) | TOP | INTERMEDIATE |  | OIL |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 1 | 2 |  |
| SPECIFICATIONS | $\begin{aligned} & 0.508-0.660 \mathrm{~mm} \\ & (0.020-0.026 \mathrm{in} .) \end{aligned}$ | $\begin{aligned} & 0.508-0.660 \mathrm{~mm} \\ & (0.020-0.026 \mathrm{in} .) \end{aligned}$ | $\begin{aligned} & 0.508-0.660 \mathrm{~mm} \\ & (0.020-0.026 \mathrm{in} .) \end{aligned}$ | $\begin{aligned} & 0.381-0.762 \mathrm{~mm} \\ & (0.015-0.030 \mathrm{in} .) \end{aligned}$ |
| PRE-TEST | RINGGTE | RINGG/1E | RINGGI2E | RINGGOE |
| POST-TEST | RINGGTO | RINGG/10 | RINGGI2O | RINGGOO |
| INCREASE | RINGGTI | RINGG/1/ | RINGG/2/ | RINGGOI |


| RING SIDE CLEARANCE ${ }^{\text {A }}$ |  | MINIMUM | MAXIMUM | SPECIFICATION |
| :---: | :---: | :---: | :---: | :---: |
| TOP | PRE-TEST | ISIDETPE | XSIDETPE | $\begin{gathered} 0.114-0.185 \mathrm{~mm} \\ \left(0.0045-0.0073^{\prime \prime}\right) \end{gathered}$ |
|  | POST-TEST | ISIDETPO | XSIDETPO |  |
|  | LSC | LSCTOP |  |  |
| INT. 1 | PRE-TEST | ISIDE1PE | XSIDE1PE | $\begin{gathered} 0.076-0.122 \mathrm{~mm} \\ \left(0.0030-0.0048^{\prime \prime}\right) \end{gathered}$ |
|  | POST-TEST | ISIDETPO | XSIDE1PO |  |
|  | LSC | LSCINT1 |  |  |
| INT. 2 | PRE-TEST | ISIDE2PE | XSIDE2PE | $\begin{gathered} 0.076-0.122 \mathrm{~mm} \\ \left(0.0030-0.0048^{\prime \prime}\right) \end{gathered}$ |
|  | POST-TEST | ISIDE2PO | XSIDE2PO |  |
|  | LSC | LSCINT2 |  |  |
| OIL | PRE-TEST | ISIDEOPE | XSIDEOPE | $\begin{gathered} 0.038-0.076 \mathrm{~mm} \\ (0.0015-0.0030 ") \end{gathered}$ |
|  | POST-TEST | ISIDEOPO | XSIDEOPO |  |
|  | LSC | LSCOIL |  |  |

A Notes:

1. WRITE "STUCK" IN PLACE OF DIMENSION WHERE APPLICABLE.
2. LSC: LOSS OF SIDE CLEARANCE.
3. REPORT METRIC UNITS.

FIG. A2.11 Form 8-Ring Measurements

| LAB: $\angle A B$ | EOT DATE: DTCOMP | END TIME: EOTTIME |
| :--- | :--- | :--- |
| STAND: STAND | RUN NUMBER: ENRUN |  |
| FORMULATION/STAND CODE: FORM |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |


| LINER BORE MEASUREMENT (mm) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| BEFORE TEST - DIAMETER (DIAL BORE GAGE) |  |  |  |  |
| BORE HEIGHT |  | LONGITUDINAL | TRANSVERSE | OUT OF ROUND |
| 22.86 cm | (9 in.) | BBLONG1 | BBTRAN1 | BBOOR1 |
| 20.32 | (8 in.) | BBLONG2 | BBTRAN2 | BBOOR2 |
| 17.78 | (7 in.) | BBLONG3 | BBTRAN3 | BBOOR3 |
| 15.24 | (6 in.) | BBLONG4 | BBTRAN4 | BBOOR4 |
| 12.70 | (5 in.) | BBLONG5 | BBTRAN5 | BBOOR5 |
| 10.16 | (4 in.) | BBLONG6 | BBTRANG | BBOOR6 |
| 7.62 | (3 in.) | BBLONG7 | BBTRAN7 | BBOOR 7 |
| 5.08 | (2 in.) | BBLONG8 | BBTRAN8 | BBOOR8 |
| 2.54 | (1 in.) | BBLONG9 | BBTRAN9 | BBOOR9 |
| TAPER (MAX) |  | BTAPLONG | BTAPTRAN |  |
| MAX. OUT OF ROUND |  |  |  | MAXOOR |
| LINER SURFACE FINISH |  | BBLFIN | 0.4-0.8 micromet |  |


| AFTER TEST - (SURFACE PROFILE) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LONGITUDINAL |  | TRANSVERSE |  |
|  | FRONT | REAR | T | AT |
| WEAR STEP | A WEARLF | AWEARLR | AWEARTT | AWEARTAT |

FIG. A2.12 Form 9—Liner Measurements

| LAB: $\angle A B$ | EOT DATE: DTCOMP |  | END TIME: EOTTIME |  |
| :---: | :---: | :---: | :---: | :---: |
| STAND: ST |  | RUN NUMBER: ENRUN |  |  |
| FORMULATION/STAND CODE: FORM |  |  |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |  |  |


| PARAMETER <br> (1) | $\begin{gathered} \text { SENSING } \\ \text { DEVICE } \\ \text { (2) } \\ \hline \end{gathered}$ | CALIBRATION FREQUENCY (3) | RECORD DEVICE | OBSERVATION FREQUENCY <br> (5) | RECORD FREQUENCY <br> (6) | LOG FREQUENCY $(7)$ | SYSTEM RESPONSE $\qquad$ (8) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Q |  |  |  |  |  |  |  |
| ENGINE SPEED (rlmin) | RPMSENS | RPMCALF | RPMRECD | RPMOBSF | RPMRECF | bPMLOGF | RPMSYSR |
| ENGINE POWER (kW) | PWRSENS | PWRCALF | PWRRECD | PWROBSF | PWRRECF | PWRLOGF | PWRSYSR |
| FUEL FLOW ( $\mathrm{kJ} / \mathrm{min}$ ) | fFLOSENS | fflocalf | fFlorecd | FFLOOBSF | fFLORECF | fflologf | fflosysh |
| HUMIDITY ( $\mathrm{g} / \mathrm{kg}$ ) | HUMSENS | HUMCALF | HUMRECD | HUMOBSF | HUMRECF | humlogf | HUMSYSR |
|  |  |  |  |  |  |  |  |
| COOLANT OUT | COTSENS | COTCALF | COTRECD | Cotobsf | COTRECF | cotlogf | COTSYSR |
| COOLANT IN | Consens | CONCALF | CONRECD | CONOBS | CONRECF | CONLOGF | CONSYSR |
| OIL TO BRG. | obrgsens | obrgcalf | OBRGRECD | obrgobsf | obrgrecf | obrglogf | OBRGSYSR |
| OIL COOLER IN | ocolsens | OCOLCALF | OCOLRECD | OCOLOBS | OCOLRECF | OCOLlOGF | OCOLSYSR |
| INLET AIR | AIRTSENS | AIRTCALF | AIRTRECD | AIRTOBSF | AIBTRECF | Airtlogf | AIRTSYSR |
| EXHAUST | EXTSENS | EXTCALF | EXTRECD | EXTOBSF | EXTRECF | Extlogf | EXTSYSR |
| RRESS (tRES. (kRal |  |  |  |  |  |  |  |
| OIL TO BRG. | OBRPSENS | OBRPCALF | OBRPRECD | obrpobsf | OBRPRECF | obrploge | OBRPSYSR |
| OIL TO JET | ojetsens | OJETCALF | OJETRECD | OJETOBSF | ojetrecf | OJEtlogf | OJETSYSR |
| INLET AIR | AIRPSENS | AIRPCALF | AIRPRECD | AIRPOBSF | AIRPRECF | AIRPLOGF | AIRPSYSR |
| EXHAUST | EXPSENS | EXPCALF | EXPRECD | EXPOBSF | EXPRECF | EXPLOGF | EXPSYSR |
| FUEL @ FILTER HSG | fFILSENS | frllcalf | FFLLRECD | fFILOBSF | fFIL RECF | fFILLOGF | fFILSYSR |
| CRANKCASF VAC | ccusens | clucalf | CCVRECD | CCVOBSF | CCVRECF | ccilogr | CCVSYSR |
| Hows. IImink |  |  |  |  |  |  |  |
| BLOWBY | BLBYSENS | BLBYCALF | BLBYRECD | BLBYOBSF | BLBYRECF | blbylogf | BLBYSYSR |
| COOLANT FLOW | CFL WSENS | CFLWCALF | CFLWRECD | CFLWOBSF | CFLWRECF | CFLWLogf | CFLWSYSR |

[^19] LEGEND:

FIG. A2.14 Form 11-Operational Summary

\[

$$
\begin{array}{r}
\text { HOURS } \\
\text { FIG. A2.16 Form 13-Oil Consumption Plot }
\end{array}
$$
\]

| LAB: | LAB | EOT DATE: DTCOMP | END TIME: EOTTIME |
| :--- | :--- | :--- | :--- |
| STAND: $\quad$ STAND | RUN NUMBER: ENRUN |  |  |
| FORMULATION/STAND CODE: FORM |  |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |  |

Note 1-Refer to Fig. X2.1 of Appendix X2 for example of photo layout. FIG. A2.17 Form 14-Piston and Ring Photographs

| LAB: | LAB | EOT DATE: DTCOMP | END TIME: | EOTTIME |
| :--- | :--- | :--- | :--- | :--- |
| STAND: | STAND | RUN NUMBER: | ENRUN |  |
| FORMULATION/STAND CODE: FORM |  |  |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |  |  |


| USAGE DATES |  | WTD |  | TGF |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| START | TIME | Lab Zi | S.A. | Lab Zi | S.A. |
| DTSTR001 | DTTMR001 | WDZIR001 | WDSAR001 | TGZIR001 | TGSAR001 |
|  |  |  |  |  |  |
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FIG. A2.18 Form 15—Severity Adjustment History

| LAB: | LAB | EOT DATE: DTCOMP | END TIME: EOTTIME |
| :--- | :--- | :--- | :--- |
| STAND: $\quad$ STAND | RUN NUMBER: ENRUN |  |  |
| FORMULATION/STAND CODE: FORM |  |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |  |

Note 1—Refer to Fig. A4.1 for example of an appropriate fuel batch analysis page.
FIG. A2.19 Form 16-Fuel Batch Analysis

| LAB: | LAB | EOT DATE: DTCOMP | END TIME: EOTTIME |
| :--- | :--- | :--- | :--- |
| STAND: STAND | RUN NUMBER: ENRUN |  |  |
| FORMULATION/STAND CODE: FORM |  |  |  |
| OILCODE/CMIR: CMIR/OILCODE |  |  |  |

Note 1—Refer to Fig. X2.3 to Appendix X2 for example Control Chart Analysis page.
FIG. A2.20 Form 17-TMC Control Chart Analysis

## A3. DATA DICTIONARY

A3.1 For Data Dictionary, See Fig. A3.1.

A3.2 For specifications and field groupings for fields in the Data Dictionary that are repeating fields, see Fig. A3.2.

| Sequence | Test |  | Data Dictionary |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Field | Field | Decimal | Data |  |  |
|  | Form | Area | Name | Length | Size | Type | Units/Format | Description |
| 10 | 0 | 1 MPC | VERSION | 8 | 0 | c | YYYYMMDD | 1MPC VERSION 19980922 |
| 20 | 0 | 1 MPC | TSTSPON1 | 40 | 0 | c |  | CONDUCTED FOR, FIRST LINE |
| 30 | 0 | 1 MPC | TSTSPON2 | 40 | 0 | c |  | CONDUCTED FOR, SECOND LINE |
| 40 | 0 | 1MPC | LABVALID | 1 | 0 | C | $V, I$ OR N | TEST LAB VALIDATION (V, I OR N ) |
| 50 | 0 | 1MPC | STAND | 5 | 0 | C |  | STAND |
| 60 | 0 | 1MPC | ENRUN | 4 | 0 | C |  | ENGINE RUN |
| 70 | 0 | 1MPC | EOTTIME | 5 | 0 | C | HH:MM | END OF TEST TIME (HH:MM) |
| 80 | 0 | 1 MPC | DTCOMP | 8 | 0 | C | YYYYMMDD | COMPLETED DATE (YYYYMMDD) |
| 90 | 0 | 1MPC | OILCODE | 38 | 0 | C |  | OIL CODE |
| 100 | 0 | 1MPC | CMIR | 6 | 0 | C |  | CMIR |
| 110 | 0 | 1MPC | FORM | 38 | 0 | C |  | FORMULATION/STAND CODE |
| 120 | 0 | 1MPC | ALTCODE1 | 10 | 0 | C |  | ALTERNATE OIL CODE 1 |
| 130 | 0 | 1MPC | ALTCOOE2 | 10 | 0 | C |  | ALTERNATE OIL CODE 2 |
| 140 | 0 | 1 MPC | ALTCOOE3 | 10 | 0 | C |  | ALTERNATE OIL CODE 3 |
| 150 | 0 | 1MPC | OPVALID | 8 | 0 | C |  | OPERATIONAL VALIDITY -- HAS/HAS NOT |
| 160 | 0 | 1MPC | SUBLAB | 40 | 0 | C |  | SUBMITTED BY: TESTING LABORATORY |
| 170 | 0 | 1 MPC | SUBSIGIM | 70 | 0 | C |  | SUBMITTED BY: SIGNATURE IMAGE |
| 180 | 0 | 1MPC | SUBNAME | 40 | 0 | C |  | SUBMITTED BY: SIGNATURE TYPED NAME |
| 190 | 0 | 1MPC | SUBTITLE | 40 | 0 | C |  | SUBMITTED BY: TITLE |
| 200 | 1 | 1MPC | LAB | 2 | 0 | C |  | LAB CODE |
| 210 | 1 | 1MPC | DTSTRT | 8 | 0 | C | YYYYMMDD | STARTING DATE (YYYYMMDD) |
| 220 | 1 | 1MPC | TESTLEN | 3 | 0 | Z | HHH | TOTAL TEST LENGTH (HHH) |
| 230 | 1 | 1 MPC | IND | 6 | 0 | C |  | TMC OIL CODE |
| 240 | 1 | 1 MPC | LABOCODE | 12 | 0 | C |  | LABORATORY INTERNAL OIL CODE |
| 250 | 1 | 1 MPC | WTD | 6 | 1 | $N$ | DEMERITS | TOTAL WEIGHTED DEMERITS UNADJUSTED LAB RATING (DEMERITS) |
| 260 | 1 | 1MPC | TGF | 3 | 0 | $N$ | \% | TOP GROOVE FILLING UNAJUSTED LAB RATING (\%) |
| 270 | 1 | 1MPC | BSOC | 5 | 3 | $N$ | g/kW-h | UNADJUSTED LAB RATING BSOC ( $\mathrm{g} / \mathrm{kW}$-h) |
| 280 | 1 | 1MPC | DATECF | 8 | 0 | C | YYYYMMDD | INDUSTRY CORRECTION DATE (YYYYMMDD) |
| 290 | 1 | 1MPC | HTDCF | 6 | 1 | $N$ | DEMERITS | INDUSTRY CORRECTION TOTAL WEIGHTED DEMERITS (DEMERITS) |
| 300 | 1 | 1MPC | TGFCF | 3 | 0 | $N$ | \% | INDUSTRY CORRECTION TOP GROOVE FILLING (\%) |
| 310 | 1 | 1 MPC | BSOCCF | 5 | 3 | $N$ | g/kW-h | INDUSTRY CORRECTION BSOC ( $\mathrm{g} / \mathrm{kW}$-h) |
| 320 | 1 | 1MPC | WTDCOR | 6 | 1 | $N$ | DEMERITS | CORRECTED WEIGHTED DEMERITS (DEMERITS) |
| 330 | 1 | 1MPC | TGFCOR | 3 | 0 | $N$ | \% | CORRECTED TOP GROOVE FILLING (\%) |
| 340 | 1 | 1 MPC | BSOCCOR | 5 | 3 | $N$ | g/kW-h | CORRECTED BSOC ( $\mathrm{g} / \mathrm{kW}-\mathrm{h}$ ) |
| 350 | 1 | 1MPC | datesa | 8 | 0 | C | YYYYMMDD | LAB SEVERITY ADJUSTMENT DATE (YYYYMMDD) |
| 360 | 1 | 1MPC | WTDSA | 6 | 1 | $N$ | DEMERITS | LAB SEVERITY ADJUSTMENT TOTAL WEIGHTED DEMERITS (DEMERITS) |
| 370 | 1 | 1MPC | TGFSA | 3 | 0 | $N$ | \% | LAB SEVERITY ADJUSTMENT TOP GROOVE FILLING (\%) |
| 380 | 1 | 1MPC | BSOCSA | 5 | 3 | $N$ | 9/kW-h | LAB SEVERITY ADJUSTMENT BSOC ( $\mathrm{g} / \mathrm{kW}-\mathrm{h}$ ) |
| 390 | 1 | 1MPC | WTDFNL | 6 | 1 | N | DEMERITS | FINAL WEIGHTED TOTAL DEMERITS (DEMERITS) |
| 400 | 1 | 1 MPC | TGFFNL | 3 | 0 | $N$ | \% | FINAL TOP GROOVE FILLING (\%) |
| 410 | 1 | 1MPC | BSOCFNL | 5 | 3 | N | g/kW-h | FINAL BSOC ( $\mathrm{g} / \mathrm{kW}$-h) |
| 420 | 1 | 1 MPC | EFFDATE | 8 | 0 | C | YYYYMMDD | TEST TARGET EFFECTIVE DATE (YYYYMMDD) |
| 430 | 1 | 1 MPC | WTDM | 6 | 1 | $N$ | DEMERITS | TEST TARGET MEAN HEIGHTED TOTAL DEMERITS (DEMERITS) |
| 440 | 1 | 1MPC | TGFM | 5 | 1 | $N$ | \% | test target mean top groove filling (\%) |
| 450 | 1 | 1MPC | BSOCM | 5 | 3 | N | g/kW-h | test target mean bsoc (g/kw-h) |
| 460 | 1 | 1MPC | WTDS | 6 | 1 | N | DEMERITS | test target sto weighted total demerits (demerits) |
| 470 | 1 | 1MPC | TGFS | 5 | 1 | $N$ | \% | TEST TARGET STD TOP GROOVE FILLING (\%) |
| 480 | 1 | 1MPC | RRLAB | 2 | 0 | C |  | REFEREE LAB CODE |
| 490 | 1 | IMPC | BSOCS | 5 | 3 | $N$ | g/kW-h | TEST TARGET STD BSOC ( $\mathrm{g} / \mathrm{kW}$-h) |
| 500 | 1 | 1MPC | RRWTD | 6 | 1 | $N$ | DEMERITS | REFEREE RATING WEIGHTED total demerits (DEMERITS) |
| 510 | 1 | 1MPC | RRTGF | 3 | 0 | $N$ | \% | REFEREE RATING TOP GROOVE FILLING (\%) |
| 520 | 1 | 1MPC | LSCTOP | 5 | 3 | $N$ | mm | TOP RING SIDE CLEARANCE LSC--0.114-0.185MM (mm) |
| 530 | 1 | 1 MPC | LSCINT1 | 5 | 3 | N | mm | INT. 1 RING SIDE CLEARANCE LSC--0.114-0.185MM (mm) |
|  |  |  |  |  |  |  | FIG. A3.1 Data | ctionary |


|  |  | ASM D 6618 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22-sep-1998 |  |  |  |  |  |  | Report: ASTM Data Dictionary |  |  |
|  |  | Test | Field | Field | Decimal | Data |  |  |  |
| Sequenc | Form | Area | Name | Length | Size | Type | Units/Format | Description |  |
| 540 | 1 | 1 MPC | LSCINT2 | 5 | 3 | $N$ | mm | Int. 2 RING SIDE CLEARANCE LSC--0 | 114-0.185MM (mm) |
| 550 | 1 | 1 MPC | LSCOIL | 5 | 3 | N | mm | OIL RING SIDE CLEARANCE LSC-0.114 | -0.185Mm (mm) |
| 560 | 1 | 1MPC | RINGGTI | 5 | 3 | $N$ | m | top ring end gap increase (mm) |  |
| 570 | 1 | 1 MPC | RINGGIII | 5 | 3 | $N$ | mm | intermediate 1 Ring end gap increas | SE (mm) |
| 580 | 1 | 1 MPC | RINGGI2I | 5 | 3 | $N$ | mm | INTERMEDIATE 2 RING END GAP InCREA | SE (mm) |
| 590 | 1 | 1 MPC | Ringgoi | 5 | 3 | N | mm | OIL RING END GAP INCREASE (mm) |  |
| 600 | 1 | 1 MPC | STUCKTOP | 3 | 0 | c |  | IS The top ring stuck? yes or nol! |  |
| 610 | 1 | 1 MPC | Stuckin1 | 3 | 0 | c |  | IS the int. 1 RING Stuck? yes OR NO |  |
| 620 | 1 | 1 MPC | stuckin2 | 3 | 0 | c |  | IS the int. 2 RING STUCK? yes OR No |  |
| 630 | 1 | 1 PPC | stuckoil | 3 | 0 | c |  | IS THE OIL RING STUCK? YES OR NO!! |  |
| 640 | 1 | 1 MPC | SCUFFTOP | 3 | 0 | $N$ | \% | SCUFFED AREA TOP (\%) |  |
| 650 | 1 | 1 MPC | SCUFFIN1 | 3 | 0 | $N$ | \% | SCUFFED AREA INT. 1 (\%) |  |
| 660 | 1 | 1 MPC | scuffin2 | 3 | 0 | $N$ | \% | SCuFfed area int. 2 (\%) |  |
| 670 | 1 | 1 MPC | SCUFFOIL | 3 | 0 | $N$ | \% | SCUFFED AREA OIL (\%) |  |
| 680 | 1 | 1 MPC | SCuFfPIS | 3 | 0 | N | \% | SCuFfed area piston (\%) |  |
| 690 | 1 | 1 MPC | SCUFFLIN | 3 | 0 | $N$ | \% | SCUFFED AREA LINER (\%) |  |
| 700 | 1 | 1 MPC | awearst | 5 | 3 | $N$ | mm | average wear step liner (mm) |  |
| 710 | 2 | 1 MPC | IRPM | 6 | 1 | $N$ | $\mathrm{r} / \mathrm{min}$ | min engine SPEed (r/min) |  |
| 720 | 2 | 1MPC | XRPM | 6 | 1 | $N$ | r/min | max engine SPEEd ( $r$ /min) |  |
| 730 | 2 | 1 MPC | ARPM | 6 | 1 | $N$ | r/min | AVG ENGINE SPEED ( $\mathrm{r} / \mathrm{min}$ ) |  |
| 740 | 2 | 1 MPC | I PUR | 5 | 1 | $N$ | kW | MIN ENGINE POWER (kW) |  |
| 750 | 2 | 1 MPC | XPWR | 5 | 1 | $N$ | kw | max engine poler (kW) |  |
| 760 | 2 | 1 MPC | APWR | 5 | 1 | $N$ | kW | AVg engine power (kW) |  |
| 770 | 2 | 1 MPC | IfFLO | 6 | 2 | N | kg/h | MIN FUEL FLOW (kg/h) |  |
| 780 | 2 | 1 MPC | XFFLO | 6 | 2 | N | kg/h | MAX FUEL FLOW (kg/h) |  |
| 790 | 2 | 1 MPC | Afflo | 6 | 2 | $N$ | kg/h | AVG FUEL FLOW (kg/h) |  |
| 800 | 2 | 1 MPC | I Humid | 4 | 1 | $N$ | g/kg | MIN HUMIDITY ( $\mathrm{g} / \mathrm{kg}$ ) |  |
| 810 | 2 | 1 MPC | XHUMID | 4 | 1 | $N$ | 9/kg | MAX HUMIDITY ( $\mathrm{g} / \mathrm{kg}$ ) |  |
| 820 | 2 | 1 MPC | AHUMID | 4 | 1 | $N$ | 9/kg | AVG RUMIDITY ( $\mathrm{g} / \mathrm{kg}$ ) |  |
| 830 | 2 | 1 MPC | ICOLOUT | 4 | 1 | $N$ | $1 / 2 \mathrm{C}$ | min coolant out ( $\%$ C ) |  |
| 840 | 2 | 1 MPC | xCOLOUT | 4 | 1 | $N$ | 1/2c | max Coolant out ( $1 / \mathrm{C}$ ) |  |
| 850 | 2 | 1 MPC | ACOLOUT | 4 | 1 | $N$ | 1/2C | avg coolant out ( $1 / \mathrm{C}$ C ) |  |
| 860 | 2 | 1MPC | ICOLIN | 4 | 1 | $N$ | $1 / 20$ | min Coolant in ( $1 / 2 \mathrm{C}$ ) |  |
| 870 | 2 | 1 MPC | xCOLIN | 4 | 1 | $N$ | $1 / 2 \mathrm{c}$ | max coolant in ( $1 / 2 \mathrm{C}$ ) |  |
| 880 | 2 | 1MPC | ACOLIN | 4 | 1 | $N$ | $1 / 20$ | avg coolant in ( $1 / 2 \mathrm{C}$ ) |  |
| 890 | 2 | 1 MPC | ICOLDT | 4 | 1 | N | $1 / 20$ | MIN COOLANT DELTA (1/2C) |  |
| 900 | 2 | 1 MPC | XCOLDT | 4 | 1 | $N$ | $1 / 2 C$ | max coolant delta (1/2C ) |  |
| 910 | 2 | 1 MPC | ACOLDT | 4 | 1 | $N$ | $1 / 2 c$ | avg coolant delta (1/2C) |  |
| 920 | 2 | 1MPC | IOBRGTMP | 5 | 1 | N | $1 / 2 \mathrm{C}$ | min oil to bearing temperature (1/2C | ) |
| 930 | 2 | 1MPC | XOBRGTMP | 5 | 1 | $N$ | 1/2C | max OIL to bearing temperature (\%/2 | ) |
| 940 | 2 | 1MPC | AOBRGTMP | 5 | 1 | N | $1 / 20$ | avg oil to bearing temperature ( $1 / 2 \mathrm{C}$ | ) |
| 950 | 2 | 1 MPC | IOCOOLIN | 5 | 1 | N | $1 / 2$ | min oil cooler in temperature ( $1 / 2 \mathrm{C}$ | ) |
| 960 | 2 | 1 MPC | xocoolin | 5 | 1 | $N$ | $1 / 2 \mathrm{C}$ | max Oil cooler in temperature ( $1 / 2 \mathrm{C}$ | ) |
| 970 | 2 | 1 MPC | aocoolin | 5 | 1 | $N$ | 1/2c | avg oil cooler in temperature ( $1 / 2 \mathrm{C}$ | ) |
| 980 | 2 | 1 MPC | IINAIRT | 5 | 1 | $N$ | $1 / 2$ | min inlet alr temperature ( $1 / \mathrm{C}$ () |  |
| 990 | 2 | 1 MPC | XINAIRT | 5 | 1 | N | $1 / 2 \mathrm{c}$ | max inlet alr temperature ( $1 / \mathrm{C}$ ) |  |
| 1000 | 2 | 1 MPC | AInAIRT | 5 | 1 | $N$ | 1/2C | avg inlet air temperature ( $1 / 2 \mathrm{C}$ ) |  |
| 1010 | 2 | 1 MPC | IEXHTMP | 5 | 1 | $N$ | $1 / 20$ | min exhaust temperature ( $1 / 2 \mathrm{C}$ ) |  |
| 1020 | 2 | 1 MPC | ХеХНTMP | 5 | 1 | $N$ | $1 / 2 \mathrm{c}$ | max exhaust temperature ( $1 / 2 \mathrm{C}$ ) |  |
| 1030 | 2 | 1 MPC | AEXHTMP | 5 | 1 | $N$ | $1 / 2$ | avg exhaust temperature ( $1 / 2 \mathrm{C}$ ) |  |
| 1040 | 2 | 1 MPC | IOBRGPR | 5 | 1 | $N$ | kPa | min oil to bearing pressure (kPa) |  |
| 1050 | 2 | 1 MPC | XOBRGPR | 5 | 1 | $N$ | kPa | max oll to bearing pressure (kPa) |  |
| 1060 | 2 | 1 MPC | AOBRGPR | 5 | 1 | $N$ | kPa | avg oil to bearing pressure (kPa) |  |
| 1070 | 2 | 1 MPC | 10JETPR | 5 | 1 | $N$ | kPa | Min oil to jet pressure (kPa) |  |
|  |  |  |  |  |  | A3.1 | Data Dictionary | continued) |  |


|  |  |  |  |  |  |  | 和 D 6618 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22-sep-1998 |  | Test | Report: ASTM Data Dictionary |  |  |  |  |  |
|  |  | Field | Field | Decimal | Data |  |  |
| Sequence | Form |  | Area | Name | Length | Size |  | Units/Format | Description |
| 1080 | 2 | 1 MPC | XOJETPR | 5 | 1 | $N$ | kPa | max oil to jet pressure (kPa) |
| 1090 | 2 | 1MPC | AOJETPR | 5 | 1 | N | kPa | avg oil to Jet pressure (kPa) |
| 1100 | 2 | 1MPC | 1 INAIRP | 5 | 1 | $N$ | kPa | min inlet air pressure (kPa) |
| 1110 | 2 | 1 MPC | XINAIRP | 5 | 1 | $N$ | kPa | max inlet alr pressure (kPa) |
| 1120 | 2 | 1 MPC | AINAIRP | 5 | 1 | $N$ | kPa | avg inlet air pressure (kPa) |
| 1130 | 2 | 1MPC | IEBP | 5 | 1 | $N$ | kPa | MIN EXHAUST PRESSURE (kPa) |
| 1140 | 2 | 1 MPC | XEBP | 5 | 1 | $N$ | kPa | max exhaust pressure (kPa) |
| 1150 | 2 | 1MPC | AEBP | 5 | 1 | $N$ | kPa | AVG EXHAUST PRESSURE (kPa) |
| 1160 | 2 | 1MPC | IFUELPR | 5 | 1 | $N$ | kPa | Min fuel a filter housing pressure (kPa) |
| 1170 | 2 | 1 MPC | XFUELPR | 5 | 1 | $N$ | kPa | max fuel a filter housing pressure (kPa) |
| 1180 | 2 | 1 MPC | AfUELPR | 5 | 1 | N | kPa | avg fuel a filter housing pressure (kPa) |
| 1190 | 2 | 1 MPC | ICCV | 4 | 2 | $N$ | kPa | Min Crankcase vacuum pressure (kPa) |
| 1200 | 2 | 1 MPC | xccv | 4 | 2 | $N$ | kPa | max crankcase vacuum pressure (kPa) |
| 1210 | 2 | 1 MPC | ACCV | 4 | 2 | $N$ | kPa | avg crankcase vacuum pressure (kPa) |
| 1220 | 2 | 1 MPC | IBLOBY | 5 | 1 | N | L/min | min blowby (L/min) |
| 1230 | 2 | 1MPC | XBLOBY | 5 | 1 | $N$ | L/min | max blowby (L/min) |
| 1240 | 2 | 1MPC | ABLOBY | 5 | 1 | $N$ | L/min | AVG blowby (L/min) |
| 1250 | 2 | 1 MPC | ICOLFLO | 6 | 1 | $N$ | L/min | MIN COOLANT FLOW (L/min) |
| 1260 | 2 | 1 MPC | XCOLFLO | 6 | 1 | N | L/min | MAX COOLANT FLOW (L/min) |
| 1270 | 2 | 1 MPC | ACOLFLO | 6 | 1 | $N$ | L/min | AVG COOLANT FLOW (L/min) |
| 1280 | 2 | 1 MPC | PISTONCL | 5 | 3 | $N$ | mm | PISTON/HEAD CLEAR ASSEM. MEASUREMENT (mm) |
| 1290 | 2 | 1 MPC | VNEW | 7 | 2 | $N$ | cst | VISCOSITY OF NEW OIL (cSt) |
| 1300 | 2 | 1 MPC | SAEVISC | 7 | 0 | C |  | SAE VISCOSITY GRADE |
| 1310 | 2 | 1 MPC | LINERPN | 12 | 0 | c |  | LINER PART NUMBER |
| 1320 | 2 | 1 MPC | LINERSN | 12 | 0 | c |  | Liner serial number |
| 1330 | 2 | 1 MPC | LINERDC | 12 | 0 | c |  | liner date cooe |
| 1340 | 2 | 1 MPC | LINERIC | 12 | 0 | c |  | LINER INSPECTION COOE |
| 1350 | 2 | 1 MPC | RINGPN | 12 | 0 | c |  | RING SET PART NUMBER |
| 1360 | 2 | 1 MPC | RINGDC | 12 | 0 | c |  | RING SET date cooe |
| 1370 | 2 | 1 MPC | ringic | 12 | 0 | c |  | Ring set inspection code |
| 1380 | 2 | 14PC | PISTPN | 12 | 0 | c |  | PISTON PART NUMBER |
| 1390 | 2 | 1 MPC | PISTSN | 12 | 0 | c |  | PISTON SERIAL HUMBER |
| 1400 | 2 | 1MPC | PISTDC | 12 | 0 | c |  | PISTON DATE COOE |
| 1410 | 2 | 1MPC | PISTIC | 12 | 0 | c |  | PISTON INSPECTION CODE |
| 1420 | 3 | 1 MPC | RPMOUT | 5 | 1 | $N$ | \% | OFFSET \& DEV SPEED TEST \% OUT (\%) |
| 1430 | 3 | 1 MPC | RPMOFF | 5 | 1 | $N$ | \% | OFFSET \& DEV SPEED TEST \% OFF (\%) |
| 1440 | 3 | 1 MPC | FFLOOUT | 5 | 1 | $N$ | \% | OfFSET \& dev fuel flow test \% OUT (\%) |
| 1450 | 3 | 1 MPC | FFLOOFF | 5 | 1 | $N$ | \% | OfFSET \& dev fuel flow test \% OfF (\%) |
| 1460 | 3 | 1 MPC | HUMOUT | 5 | 1 | $N$ | \% | OFFSET \& DEV HUMIDITY TEST \% OUT (\%) |
| 1470 | 3 | 1 MPC | HUMOFF | 5 | 1 | $N$ | \% | OFFSET \& DEV HUMIDITY TEST \% OFF (\%) |
| 1480 | 3 | 1MPC | COLFOUT | 5 | 1 | $N$ | \% | OFFSET \& DEV COOLANT FLOW TEST \% OUT (\%) |
| 1490 | 3 | 1 MPC | COLFOFF | 5 | 1 | $N$ | \% | OfFSET \& dev coolant flow test \% off (\%) |
| 1500 | 3 | 1 MPC | cotout | 5 | 1 | N | \% | OFFSET \& DEV COOLANT OUT TEST \% OUT (\%) |
| 1510 | 3 | 1 MPC | COTOFF | 5 | 1 | $N$ | \% | OFFSET \& DEV COOLANT OUT TEST \% OFF (\%) |
| 1520 | 3 | 1 MPC | OBRGOUT | 5 | 1 | $N$ | \% | OFFSET \& DEV OIL TO BEARING TEST \% OUT (\%) |
| 1530 | 3 | 1 MPC | OBRGOFF | 5 | 1 | $N$ | \% | OfFSET \& dev oil to bearing test \% off (\%) |
| 1540 | 3 | 1 MPC | AIRTOUT | 5 | 1 | N | \% | OfFSET \& DEV Intake alr temp test \% OUT (\%) |
| 1550 | 3 | 1 MPC | AlRtoff | 5 | 1 | $N$ | \% | OFFSET \& DEV Intake alr temp test \% off (\%) |
| 1560 | 3 | 1 MPC | OJETOUT | 5 | 1 | $N$ | \% | OFFSET \& DEV OIL JET TEST \% OUT (\%) |
| 1570 | 3 | 1 mPC | OJETOFF | 5 | 1 | $N$ | \% | OFFSET \& DEV OIL JET TEST \% OFF (\%) |
| 1580 | 3 | 1 MPC | AIRPOUT | 5 | 1 |  | \% | OFFSET \& DEV InLET AIR PRESSURE TEST \% OUT (\%) |
| 1590 | 3 | 1 MPC | AIRPOFF | 5 | 1 | $N$ | \% | OFFSET \& DEV INLET AIR PRESSURE TEST \% OfF (\%) |
| 1600 | 3 | 1 MPC | EXPOUT | 5 | 1 |  | \% | OFFSET \& DEV EXHAUST PRESSURE TEST \% OUT (\%) |
| 1610 | 3 | 1mPC | EXPOFF | 5 | 1 | N | \% | OFFSET \& DEV EXHAUST PRESSURE TEST \% OFF (\%) |
|  |  |  |  |  | FIG. A3 | . 1 Da | Data Dictionary (cond | ontinued) |



[^20]22-sep-1998 Test
Sequence Form Area

Field Field Decimal Data
Name

Length Size Type Units/Format

Report: ASTM Data Dictionary

| 2160 | 4 | 1 MPC | L4LCD | 6 | 2 | $N$ | demerits | LAND \#4 LC-1.0 CARBON DEMERITS (DEMERITS) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2170 | 4 | 1 MPC | g1actot | 3 | 0 | $N$ | \% area | total groove \#1 carbon area percent (\% area) |
| 2180 | 4 | 1 MPC | G10ctot | 6 | 2 | $N$ | demerits | total groove \#1 carbon demerits (demerits) |
| 2190 | 4 | 1 MPC | GZACTOT | 3 | 0 | $N$ | \% area | total groove \#2 carbon area percent (\% area) |
| 2200 | 4 | 1 MPC | G2DCtot | 6 | 2 | $N$ | demerits | total groove \#2 carbon demerits (demerits) |
| 2210 | 4 | 1 MPC | g3actot | 3 | 0 | $N$ | \% AREA | total groove \#3 Carbon area percent (\% area) |
| 2220 | 4 | 1 MPC | G3DCTOT | 6 | 2 | $N$ | demerits | total groove \#3 Carbon demerits (demerits) |
| 2230 | 4 | 1 MPC | G4Actot | 3 | 0 | $N$ | \% Area | total groove \#4 Carbon area percent (\% area) |
| 2240 | 4 | 1 MPC | G4DCtot | 6 | 2 | $N$ | demerits | total groove \#4 Carbon demerits (demerits) |
| 2250 | 4 | 1 MPC | L2actot | 3 | 0 | $N$ | \% AREA | total land \#2 Carbon area percent (\% area) |
| 2260 | 4 | 1 MPC | Lгостот | 6 | 2 | $N$ | demerits | total land \#2 Carbon demerits (DEmerits) |
| 2270 | 4 | 1 MPC | L3ACtot | 3 | 0 | $N$ | \% area | total land \#3 carbon area percent (\% area) |
| 2280 | 4 | 1 MPC | L3DCtot | 6 | 2 | N | DEMERITS | total land \#3 carbon demerits (demerits) |
| 2290 | 4 | 1 MPC | L4ACTOT | 3 | 0 | $N$ | \% AREA | total land \#4 carbon area percent (\% area) |
| 2300 | 4 | 1 MPC | L4DCtot | 6 | 2 | $N$ | DEMERITS | TOTAL LAND \#4 CARBON DEMERITS (DEMERITS) |
| 2310 | 4 | 1 MPC | G1L9A | 3 | 0 | $N$ | \% area | groove \#1 8-9 lacquer area percent (\% area) |
| 2320 | 4 | 1 MPC | 61190 | 6 | 2 | $N$ | demerits | GROOVE \#1 8-9 LacQuer demerits (demerits) |
| 2330 | 4 | 1 MPC | G2L9A | 3 | 0 | $N$ | \% area | GROOVE \#2 8-9 Lacquer area percent (\% AREA) |
| 2340 | 4 | 1 MPC | G2L90 | 6 | 2 | $N$ | demerits | GROOVE \#2 8-9 LACQUER DEMERITS (DEMERITS) |
| 2350 | 4 | 1 MPC | G3L9A | 3 | 0 | $N$ | \% area | groove \#3 8-9 lacquer area Percent (\% area) |
| 2360 | 4 | 1 MPC | G3190 | 6 | 2 | $N$ | demerits | GROOVE \#3 8-9 LaCQuer demerits (DEMERITS) |
| 2370 | 4 | 1MPC | G4L9A | 3 | 0 | $N$ | \% AREA | groove \#4 8-9 lacquer area percent (\% area) |
| 2380 | 4 | 1MPC | G4L9D | 6 | 2 | N | DEMERITS | GROOVE \#4 8-9 LACQuER DEMERITS (DEMERITS) |
| 2390 | 4 | 1 MPC | L2L9A | 3 | 0 | $N$ | \% AREA | Land \#2 8-9 lacquer area percent (\% area) |
| 2400 | 4 | 1 MPC | L2L90 | 6 | 2 | N | DEMERITS | LAND \#2 8-9 LacQuer demerits (DEmerits) |
| 2410 | 4 | 1 MPC | L3L9A | 3 | 0 | $N$ | \% area | LAND \#3 8-9 Lacquer area percent (\% AREA) |
| 2420 | 4 | 1MPC | L3L90 | 6 | 2 | $N$ | demerits | LAND \#3 8-9 LACQuER DEMERITS (DEMERITS) |
| 2430 | 4 | 1 MPC | 14L9A | 3 | 0 | $N$ | \% area | Land \#4 8-9 lacouer area percent (\% area) |
| 2440 | 4 | 1 MPC | L4L90 | 6 | 2 | N | DEMERItS | LAND \#4 8-9 LACQUER DEMERITS (DEMERITS) |
| 2450 | 4 | 1 MPC | G1L8A | 3 | 0 | $N$ | \% AREA | GROOVE \#1 7-7.9 Lacquer area percent (\% area) |
| 2460 | 4 | 1MPC | G1L8D | 6 | 2 | $N$ | DEMERITS | GROOVE \#1 7-7.9 LACQUER DEMERITS (DEMERITS) |
| 2470 | 4 | 1MPC | G2L8A | 3 | 0 | $N$ | \% area | groove \#2 7-7.9 LacQuer area percent (\% area) |
| 2480 | 4 | 1 MPC | G2L8D | 6 | 2 | N | DEMERITS | GROOVE \#2 7-7.9 LACQUER DEMERITS (DEMERITS) |
| 2490 | 4 | 1 MPC | G3L8A | 3 | 0 | $N$ | \% AREA | GROOVE \#3 7-7.9 Lacquer area percent (\% area) |
| 2500 | 4 | 1MPC | G3L8D | 6 | 2 | $N$ | demerits | GROOVE \#3 7-7.9 LACQUER DEMERITS (DEMERITS) |
| 2510 | 4 | 1MPC | G4L8A | 3 | 0 | $N$ | \% area | GROOVE \#4 7-7.9 Lacquer area percent (\% area) |
| 2520 | 4 | 1 MPC | G4L8D | 6 | 2 | $N$ | demerits | GROOVE \#4 7-7.9 LACQUER DEMERITS (DEMERITS) |
| 2530 | 4 | 1 MPC | L2L8A | 3 | 0 | $N$ | \% AREA | LaND \#2 7-7.9 LACQUER AREA PERCENT (\% AREA) |
| 2540 | 4 | 1 MPC | L2L8D | 6 | 2 | $N$ | demerits | LAND \#2 7-7.9 LaCQuer demerits (DEMERITS) |
| 2550 | 4 | 1 MPC | L3L8A | 3 | 0 | $N$ | \% AREA | Land \#3 7-7.9 LacQuer area percent (\% area) |
| 2560 | 4 | 1 MPC | L3L8D | 6 | 2 | $N$ | DEMERITS | LAND \#3 7-7.9 LaCQuer demerits (DEMERITS) |
| 2570 | 4 | 1 MPC | L4L8A | 3 | 0 | $N$ | \% area | LAND \#4 7-7.9 LaCOUER AREA PERCENT (\% AREA) |
| 2580 | 4 | 1 MPC | L4L8D | 6 | 2 | $N$ | demerits | LAND \# 7 7-7.9 LaCQuer demerits (DEMERITS) |
| 2590 | 4 | 1 MPC | 61L7A | 3 | 0 | N | \% AREA | Groove \#1 6-6.9 lacquer area percent (\% area) |
| 2600 | 4 | 1 MPC | G1L70 | 6 | 2 | N | DEMERITS | GROOVE \#1 6-6.9 LACQUER DEMERITS (DEMERITS) |
| 2610 | 4 | 1 MPC | G2L7A | 3 | 0 | $N$ | \% area | GROOVE \#2 6-6.9 LaCQuer area percent (\% area) |
| 2620 | 4 | 1 MPC | G2L70 | 6 | 2 | $N$ | demerits | GROOVE \#2 6-6.9 LACQUER DEMERITS (DEMERITS) |
| 2630 | 4 | 1MPC | 63L7A | 3 | 0 | $N$ | \% area | groove \#3 6-6.9 lacquer area percent (\% area) |
| 2640 | 4 | 1 MPC | 63170 | 6 | 2 | $N$ | demerits | GROOVE \#3 6-6.9 LACQUER DEMERITS (DEMERITS) |
| 2650 | 4 | 1 MPC | G4L7A | 3 | 0 | N | \% AREA | groove \#4 6-6.9 lacouer area percent (\% area) |
| 2660 | 4 | 1 MPC | 64L70 | 6 | 2 | $N$ | demerits | GROOVE \#4 6-6.9 LACQUER DEMERITS (DEmerits) |
| 2670 | 4 | 1 MPC | L2L7A | 3 | 0 | N | \% AREA | LaND \#2 6-6.9 LacQuer area Percent (\% area) |
| 2680 | 4 | 1 MPC | L2L7D | 6 | 2 | $N$ | demerits | LAND \#2 6-6.9 LaCQuer demerits (DEMERITS) |
| 2690 | 4 | 1 MPC | L3L7A | 3 | 0 | N | \% area | LaND \#3 6-6.9 LacQuer area percent (\% AREA) |

N demerits
$\mathrm{N} \%$ area $N$ demerits $N \%$ area N DEMERITS \% area demerits \% AREA N DEmerits N \% AREA demerits N \% area N Demerits N \% area n demerits $N \%$ area demerits \% area demerits N \% area $n$ demerits $N \%$ AREA $n$ demerits N \% AREA $n$ demerits N \% area n demerits N \% AREA n demerits N \% AREA n demerits N \% AREA $N$ demerits N \% area N DEMERITS N \% area n demerits N \% AREA n demerits N \% area n demerits N \% area
N demerits N \% area n demerits N \% AREA n demerits N \% area n demerits N \% area $N$ demerits N \% area $n$ demerits N \% area

## Description

FIG. A3.1 Data Dictionary (continued)

| 22-sep-1998 |  |  |  |  |  |  | Report: ASTM Data Dictionary |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sequence Form |  | Test |  | Field Decimal Data |  |  |  |  |
|  |  | Area | Name | Leng | Size | Type | Units/Format | Description |
| 2700 | 4 | 1MPC | L3L7D | 6 | 2 | $N$ | DEMERITS | LAND \#3 6-6.9 LACQUER DEMERITS (DEMERITS) |
| 2710 | 4 | 1MPC | L4L7A | 3 | 0 | $N$ | \% AREA | LAND \#4 6-6.9 LACQUER AREA PERCENT (\% AREA) |
| 2720 | 4 | 1MPC | L4L7D | 6 | 2 | $N$ | DEMERITS | LAND \#4 6-6.9 LACQUER DEMERITS (DEMERITS) |
| 2730 | 4 | 1MPC | G1L6A | 3 | 0 | N | \% AREA | GROOVE \#1 5-5.9 LACQUER AREA PERCENT (\% AREA) |
| 2740 | 4 | 1 MPC | G1L60 | 6 | 2 | $N$ | DEMERITS | GROOVE \#1 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 2750 | 4 | 1MPC | G2L6A | 3 | 0 | N | \% AREA | GROOVE \#2 5-5.9 LACQUER AREA PERCENT (\% AREA) |
| 2760 | 4 | 1 MPC | G2L60 | 6 | 2 | N | DEMERITS | GROOVE \#2 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 2770 | 4 | IMPC | G3L6A | 3 | 0 | N | \% AREA | GROOVE \#3 5-5.9 LACQUER AREA PERCENT (\% AREA) |
| 2780 | 4 | 1 MPC | G3L60 | 6 | 2 | N | DEMERITS | GROOVE \#3 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 2790 | 4 | 1 MPC | 64L6A | 3 | 0 | N | \% AREA | GROOVE \#4 5-5.9 LACQUER AREA PERCENT (\% AREA) |
| 2800 | 4 | 1 MPC | G4L6D | 6 | 2 | N | DEMERITS | GROOVE \#4 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 2810 | 4 | 1 MPC | L2L6A | 3 | 0 | $N$ | \% AREA | LAND \#2 5-5.9 LACQUER AREA PERCENT (\% AREA) |
| 2820 | 4 | 1 MPC | L2L6D | 6 | 2 | N | DEMERITS | LAND \#2 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 2830 | 4 | 1 MPC | L3L6A | 3 | 0 | N | \% AREA | LAND \#3 5-5.9 LACQUER AREA PERCENT (\% AREA) |
| 2840 | 4 | 1 MPC | L3L60 | 6 | 2 | N | DEMERITS | LAND \#3 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 2850 | 4 | 1 MPC | L4L6A | 3 | 0 | N | \% AREA | LAND \#4 5-5.9 LACQUER AREA PERCENT (\% AREA) |
| 2860 | 4 | 1MPC | L4L60 | 6 | 2 | N | DEMERITS | LAND \#4 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 2870 | 4 | 1 MPC | G1L5A | 3 | 0 | $N$ | \% AREA | GROOVE \#1 4-4.9 LACQUER AREA PERCENT (\% AREA) |
| 2880 | 4 | 1 MPC | G1L5D | 6 | 2 | $N$ | DEMERITS | GROOVE \#1 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 2890 | 4 | 1 MPC | G2L5A | 3 | 0 | $N$ | \% AREA | GROOVE \#2 4-4.9 LACQUER AREA PERCENT (\% AREA) |
| 2900 | 4 | 1MPC | G2L5D | 6 | 2 | $N$ | DEMERITS | GROOVE \#2 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 2910 | 4 | 1MPC | G3L5A | 3 | 0 | $N$ | \% AREA | GROOVE \#3 4-4.9 LACQUER AREA PERCENT (\% AREA) |
| 2920 | 4 | 1 MPC | G3L50 | 6 | 2 | $N$ | DEMERITS | GROOVE \#3 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 2930 | 4 | 1 MPC | G4L5A | 3 | 0 | $N$ | \% AREA | GROOVE \#4 4-4.9 LACQUER AREA PERCENT (\% AREA) |
| 2940 | 4 | 1 MPC | G4L5D | 6 | 2 | $N$ | DEMERITS | GROOVE \#4 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 2950 | 4 | 1 MPC | L2L5A | 3 | 0 | $N$ | \% AREA | LAND \#2 4-4.9 LACQUER AREA PERCENT (\% AREA) |
| 2960 | 4 | 1 MPC | L2L5D | 6 | 2 | $N$ | DEMERITS | LAND \#2 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 2970 | 4 | 1 MPC | L3L5A | 3 | 0 | $N$ | \% AREA | LAND \#3 4-4.9 LACQUER AREA PERCENT (\% AREA) |
| 2980 | 4 | 1 MPC | L3L50 | 6 | 2 | $N$ | demerits | LAND \#3 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 2990 | 4 | 1 MPC | 14L5A | 3 | 0 | $N$ | \% AREA | LAND \#4 4-4.9 LACQUER AREA PERCENT (\% AREA) |
| 3000 | 4 | 1 MPC | L4L5D | 6 | 2 | $N$ | DEMERITS | LAND \#4 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 3010 | 4 | 1 MPC | G1L4A | 3 | 0 | $N$ | \% AREA | GROOVE \#1 3-3.9 LACQUER AREA PERCENT (\% AREA) |
| 3020 | 4 | 1 MPC | G1L4D | 6 | 2 | $N$ | DEMERITS | GROOVE \#1 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 3030 | 4 | 1 MPC | G2L4A | 3 | 0 | $N$ | \% AREA | GROOVE \#2 3-3.9 LACQUER AREA PERCENT (\% AREA) |
| 3040 | 4 | 1 MPC | G2L4D | 6 | 2 | $N$ | DEMERITS | GROOVE \#2 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 3050 | 4 | 1 MPC | 63L4A | 3 | 0 | $N$ | \% AREA | GROOVE \#3 3-3.9 LACQUER AREA PERCENT (\% AREA) |
| 3060 | 4 | 1 MPC | G3L4D | 6 | 2 | N | DEMERITS | GROOVE \#3 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 3070 | 4 | 1 MPC | G4L4A | 3 | 0 | $N$ | \% AREA | GROOVE \#4 3-3.9 LACQUER AREA PERCENT (\% AREA) |
| 3080 | 4 | 1 MPC | G414D | 6 | 2 | $N$ | DEMERITS | GROOVE \#4 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 3090 | 4 | 1 MPC | L.214A | 3 | 0 | $N$ | \% AREA | LAND \#2 3-3.9 LACQUER AREA PERCENT (\% AREA) |
| 3100 | 4 | 1MPC | L2L4D | 6 | 2 | $N$ | DEMERITS | LAND \#2 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 3110 | 4 | 1 MPC | L3L4A | 3 | 0 | $N$ | \% AREA | LAND \#3 3-3.9 LACQUER AREA PERCENT (\% AREA) |
| 3120 | 4 | 1 MPC | L3L4D | 6 | 2 | $N$ | DEMERITS | LAND \#3 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 3130 | 4 | 1 MPC | L4L4A | 3 | 0 | $N$ | \% AREA | LAND \#4 3-3.9 LACQUER AREA PERCENT (\% AREA) |
| 3140 | 4 | 1 MPC | L4L4D | 6 | 2 | $N$ | DEMERITS | LAND \#4 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 3150 | 4 | 1 MPC | G1L3A | 3 | 0 | $N$ | \% AREA | GROOVE \#1 2-2.9 LACQUER AREA PERCENT (\% AREA) |
| 3160 | 4 | 1 MPC | G1L3D | 6 | 2 | N | demerits | GROOVE \#1 2-2.9 LACQUER DEMERITS (DEMERITS) |
| 3170 | 4 | 1 MPC | G2L3A | 3 | 0 | $N$ | \% AREA | GROOVE \#2 2-2.9 LACQUER AREA PERCENT (\% AREA) |
| 3180 | 4 | 1 MPC | G2L3D | 6 | 2 | N | DEMERITS | GROOVE \#2 2-2.9 LACQUER DEMERITS (DEMERITS) |
| 3190 | 4 | 1 MPC | 63L3A | 3 | 0 | $N$ | \% AREA | GROOVE \#3 2-2.9 LACQUER AREA PERCENT (\% AREA) |
| 3200 | 4 | 1MPC | G3L3D | 6 | 2 | $N$ | DEMERITS | GROOVE \#3 2-2.9 LACQUER DEMERITS (DEMERITS) |
| 3210 | 4 | 1 MPC | G4L3A | 3 | 0 | $N$ | \% AREA | GROOVE \#4 2-2.9 LACQUER AREA PERCENT (\% AREA) |
| 3220 | 4 | 1 MPC | G4L3D | 6 | 2 | $N$ | DEMERITS | GROOVE \#4 2-2.9 LACQUER DEMERITS (DEMERITS) |
| 3230 | 4 | 1 MPC | L2L3A | 3 | 0 | $N$ | \% AREA | LAND \#2 2-2.9 LACQUER AREA PERCENT (\% AREA) |
|  |  |  |  |  | FIG. A3. |  | ta Dictionary |  |


$3240 \quad 4 \quad$ IMPC 12130


| 3780 | 4 | 1MPC | G1uwd | 6 | 2 | N | DEMERITS | GROOVE 1 UNWEIGHTED DEMERITS (DEMERITS) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3790 | 4 | 1MPC | G2UWD | 6 | 2 | $N$ | DEMERITS | GROOVE 2 UNWEIGHTED DEMERITS (DEMERITS) |
| 3800 | 4 | 1 MPC | G3UWD | 6 | 2 | $N$ | DEMERITS | GROOVE 3 UNWEIGHTED DEMERITS (DEMERITS) |
| 3810 | 4 | 1MPC | G4UWD | 6 | 2 | $N$ | DEMERITS | GROOVE 4 UNWEIGHTED DEMERITS (DEMERITS) |
| 3820 | 4 | 1MPC | L2UWD | 6 | 2 | $N$ | DEMERITS | LAND 2 UNWEIGHTED DEMERITS (DEMERITS) |
| 3830 | 4 | 1 MPC | L3ULD | 6 | 2 | $N$ | DEMERITS | LAND 3 UNUEIGHTED DEMERITS (DEMERITS) |
| 3840 | 4 | 1MPC | L4ULD | 6 | 2 | $N$ | DEMERITS | LAND 4 UNWEIGHTED DEMERITS (DEMERITS) |
| 3850 | 4 | 1 MPC | G1WD | 6 | 2 | $N$ | DEMERITS | GROOVE 1 WEIGHTED DEMERITS (DEMERITS) |
| 3860 | 4 | 1 MPC | G2WD | 6 | 2 | N | DEMERITS | GROOVE 2 WEIGHTED DEMERITS (DEMERITS) |
| 3870 | 4 | 1 MPC | G3WD | 6 | 2 | $N$ | DEMERITS | GROOVE 3 WEIGHTED DEMERITS (DEMERITS) |
| 3880 | 4 | 1 MPC | G4WD | 6 | 2 | $N$ | DEMERITS | GROOVE 4 WEIGHTED DEMERITS (DEMERITS) |
| 3890 | 4 | 1MPC | L2WD | 6 | 2 | $N$ | DEMERITS | LAND 2 WEIGHTED DEMERITS (DEMERITS) |
| 3900 | 4 | 1 MPC | L3WD | 6 | 2 | $N$ | DEMERITS | LAND 3 WEIGHTED DEMERITS (DEMERITS) |
| 3910 | 4 | 1 MPC | L4WD | 6 | 2 | $N$ | DEMERITS | LAND 4 WEIGHTED DEMERITS (DEMERITS) |
| 3920 | 4 a | 1 MPC | RATEWSIM | 70 | 0 | C |  | PISTON RATING WORKSHEET IMAGE |
| 3930 | 5 | 1 MPC | SKHCA | 3 | 0 | $N$ | \% AREA | SKIRT HEAVY CARBON(\% AREA) |
| 3940 | 5 | 1 MPC | SKMCA | 3 | 0 | $N$ | \% AREA | SKIRT MEDIUM CARBON(\% AREA) |
| 3950 | 5 | 1 MPC | SKLCA | 3 | 0 | N | \% AREA | SKIRT LIGHT CARBON(\% AREA) |
| 3960 | 5 | 1 MPC | SK9A | 3 | 0 | N | \% AREA | SKIRT DEPOSIT 9 - 8(\% AREA) |
| 3970 | 5 | 1MPC | SK8A | 3 | 0 | $N$ | \% AREA | SKIRT DEPOSIT 7.9 - 7(\% AREA) |
| 3980 | 5 | 1 MPC | SK7A | 3 | 0 | $N$ | \% AREA | SKIRT DEPOSIT 6.9-6(\% AREA) |
| 3990 | 5 | 1 MPC | SK6A | 3 | 0 | $N$ | \% AREA | SKIRT DEPOSIT 5.9 - 5(\% AREA) |
| 4000 | 5 | 1 MPC | SK5A | 3 | 0 | $N$ | \% AREA | SKIRT DEPOSIT 4.9 - 4 (\% AREA) |
| 4010 | 5 | 1 MPC | SK4A | 3 | 0 | N | \% AREA | SKIRT DEPOSIT 3.9-3 (\% AREA) |
| 4020 | 5 | 1 MPC | SK3A | 3 | 0 | $N$ | \% AREA | SKIRT DEPOSIT 2.9 - 2(\% AREA) |
| 4030 | 5 | 1 MPC | SK2A | 3 | 0 | $N$ | \% AREA | SKIRT DEPOSIT 1.9-1(\% AREA) |
| 4040 | 5 | 1MPC | SK1A | 3 | 0 | $N$ | \% AREA | SKIRT DEPOSIT 0.9 - O(\% AREA) |
| 4050 | 5 | 1 1MPC | SKCLNA | 3 | 0 | $N$ | \% AREA | SKIRT DEPOSIT CLEAN (\% AREA) |
| 4060 | 5 | 1 MPC | UCHCA | 3 | 0 | N | \% AREA | UNDER CROWN HEAVY CARBON(\% AREA) |
| 4070 | 5 | 1 MPC | UCMCA | 3 | 0 | $N$ | \% AREA | UNDER CROWN MEDIUM CARBON(\% AREA) |
| 4080 | 5 | 1 MPC | UCLCA | 3 | 0 | $N$ | \% AREA | UNDER CROWN LIGHT CARBON(\% AREA) |
| 4090 | 5 | 1 MPC | UC9A | 3 | 0 | $N$ | \% AREA | UNDER CROWN DEPOSIT 9 - 8(\% AREA) |
| 4100 | 5 | 1 MPC | UC8A | 3 | 0 | $N$ | \% AREA | UNDER CROWN DEPOSIT 7.9 - 7(\% AREA) |
| 4110 | 5 | 1 MPC | UC7A | 3 | 0 | N | \% AREA | UNDER CROWN DEPOSIT 6.9 - 6(\% AREA) |
| 4120 | 5 | 1MPC | UC6A | 3 | 0 | N | \% AREA | UNDER CROWN DEPOSIT 5.9 - 5(\% AREA) |
| 4130 | 5 | 1 MPC | UC5A | 3 | 0 | $N$ | \% AREA | UNDER CROWN DEPOSIT 4.9 - 4 (\% AREA) |
| 4140 | 5 | 1MPC | UC4A | 3 | 0 | $N$ | \% AREA | UNDER CROWN DEPOSIT 3.9-3(\% AREA) |
| 4150 | 5 | 1MPC | UC3A | 3 | 0 | N | \% AREA | UNDER CROWN DEPOSIT 2.9 - $2(\%$ AREA) |
| 4160 | 5 | 1MPC | UC2A | 3 | 0 | $N$ | \% AREA | UNDER CROWN DEPOSIT 1.9 - 1(\% AREA) |
| 4170 | 5 | 1 MPC | UC1A | 3 | 0 | N | \% AREA | UNDER CROWN DEPOSIT $0.9-0(\%$ AREA |
| 4180 | 5 | 1MPC | UCCLNA | 3 | 0 | $N$ | \% AREA | UNDER CROWN DEPOSIT CLEAN (\% AREA) |
| 4190 | 5 | 1MPC | LIHCA | 3 | 0 | $N$ | \% AREA | LINER ABOVE RING TRAVEL HEAVY CARBON(\% AREA) |
| 4200 | 5 | 1MPC | LIMCA | 3 | 0 | N | \% AREA | LINER ABOVE RING TRAVEL MEDIUM CARBON(\% AREA) |
| 4210 | 5 | 1MPC | LILCA | 3 | 0 | N | \% AREA | LINER ABOVE RING TRAVEL LIGHT CARBON(\% AREA) |
| 4220 | 5 | 1MPC | LI9A | 3 | 0 | $N$ | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 9 - 8(\% AREA) |
| 4230 | 5 | 1MPC | L18A | 3 | 0 | $N$ | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 7.9 - 7(\% AREA) |
| 4240 | 5 | 1MPC | L17A | 3 | 0 | $N$ | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 6.9 - $6(\%$ AREA) |
| 4250 | 5 | 1MPC | L16A | 3 | 0 | $N$ | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 5.9-5(\% AREA) |
| 4260 | 5 | 1 MPC | LI5A | 3 | 0 | $N$ | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 4.9 - 4 (\% AREA) |
| 4270 | 5 | 1MPC | LI4A | 3 | 0 | $N$ | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 3.9 - 3 (\% AREA) |
| 4280 | 5 | 1MPC | LI3A | 3 | 0 | N | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 2.9 - 2 (\% AREA) |
| 4290 | 5 | 1MPC | LI2A | 3 | 0 | N | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 1.9 - 1 (\% AREA) |
| 4300 | 5 | 1MPC | LIIA | 3 | 0 | $N$ | \% AREA | LINER ABOVE RING TRAVEL DEPOSIT 0.9 - O(\% AREA) |
| 4310 | 5 | 1MPC | LICLNA | 3 | $\begin{gathered} 0 \\ \text { FIG } \end{gathered}$ |  | \% AREA Data Diction | LINER ABOVE RING TRAVEL DEPOSIT CLEAN (\% AREA) ontinued) |

# ASM D 6618 



# ASM D 6618 

| 22-sep-1998 |  |  |  |  |  |  | Report: ASTM Data Dictionary |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Test | Field | Field | Decimal |  |  |  |
| Sequence | Form | Area | Name | Length | size |  | Units/Format | Description |
| 4860 | 5 | 1MPC | G2BLCA | 3 | 0 | $N$ | \% AREA | BOTTOM GROOVE 2 LIGHT CARBON(\% AREA) |
| 4870 | 5 | 1 MPC | G2B9A | 3 | 0 | $N$ | \% AREA | BOTTOM GROOVE 2 deposit 9-8(\% AREA) |
| 4880 | 5 | 1 MPC | G2B8A | 3 | 0 | $N$ | \% Area | Bottom groove 2 deposit $7.9-7(\%$ AREA) |
| 4890 | 5 | 1 MPC | G2B7A | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 2 DEPOSIT 6.9-6(\% AREA) |
| 4900 | 5 | 1 MPC | G2B6A | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 2 DEPOSIT 5.9-5(\% AREA) |
| 4910 | 5 | 1 MPC | G2B5A | 3 | 0 | $N$ | \% AREA | Bottom groove 2 deposit 4.9 - 4 (\% AREA) |
| 4920 | 5 | 1MPC | G2B4A | 3 | 0 | $N$ | \% ArEA | Bottom groove 2 DEPOSIT 3.9-3(\% AREA) |
| 4930 | 5 | 1 MPC | G2B3A | 3 | 0 | $N$ | \% area | Bottom groove 2 deposit 2.9 - 2 (\% area) |
| 4940 | 5 | 1MPC | G2B2A | 3 | 0 | N | \% Area | Bottom groove 2 deposit 1.9-1(\% AREA) |
| 4950 | 5 | 1 MPC | G2B1A | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 2 deposit 0.9 - 0(\% area) |
| 4960 | 5 | 1 MPC | g2bclna | 3 | 0 | $N$ | \% area | bottom groove 2 deposit clean (\% AREA) |
| 4970 | 5 | 1 MPC | G3thCA | 3 | 0 | $N$ | \% AREA | TOP GROOVE 3 HEAVY CARBON(\% AREA) |
| 4980 | 5 | 1 MPC | G3TMCA | 3 | 0 | $N$ | \% AREA | TOP GROOVE 3 MEDIUM CARBON(\% AREA) |
| 4990 | 5 | 1MPC | G3TLCA | 3 | 0 | N | \% AREA | TOP GROOVE 3 LIGHT CARBON(\% AREA) |
| 5000 | 5 | 1 MPC | G3T9A | 3 | 0 | $N$ | \% Area | TOP GROOVE 3 deposit 9 - 8(\% AREA) |
| 5010 | 5 | 1 MPC | G3T8A | 3 | 0 | $N$ | \% AREA | TOP GROOVE 3 DEPOSIT 7.9 - 7 \% AREA) |
| 5020 | 5 | 1 MPC | G3T7A | 3 | 0 | $N$ | \% AREA | TOP GROOVE 3 DEPOSIT 6.9 - 6(\% AREA) |
| 5030 | 5 | 1MPC | G3T6A | 3 | 0 | $N$ | \% Area | TOP GROOVE 3 DEPOSIT 5.9-5(\% AREA) |
| 5040 | 5 | 1 MPC | G3T5A | 3 | 0 | $N$ | \% area | TOP GROOVE 3 deposit 4.9 - 4 (\% AREA) |
| 5050 | 5 | 1 MPC | 6374A | 3 | 0 | $N$ | \% area | TOP GROOVE 3 DEPOSIT 3.9-3(\% AREA) |
| 5060 | 5 | 1MPC | G3T3A | 3 | 0 | $N$ | \% area | TOP GROOVE 3 DEPOSIT 2.9 - 2(\% AREA) |
| 5070 | 5 | 1 MPC | G3T2A | 3 | 0 | $N$ | \% area | TOP GROOVE 3 DEPOSIT 1.9-1(\% AREA) |
| 5080 | 5 | 1 MPC | G3T1A | 3 | 0 | $N$ | \% AREA | TOP GROOVE 3 DEPOSIT 0.9 - 0(\% AREA) |
| 5090 | 5 | 1 MPC | g3tclna | 3 | 0 | N | \% area | TOP GROOVE 3 DEPOSIT CLEAN (\% AREA) |
| 5100 | 5 | 1 MPC | G3внса | 3 | 0 | $N$ | \% AREA | BOTTOM GROOVE 3 HEAVY CARBON(\% AREA) |
| 5110 | 5 | 1 MPC | g3BMCA | 3 | 0 | $N$ | \% Area | BOTTOM GROOVE 3 MEDIUM CARBON(\% AREA) |
| 5120 | 5 | 1 MPC | G3BLCA | 3 | 0 | $N$ | \% AREA | BOTTOM GROOVE 3 LIGHT CARBON(\% AREA) |
| 5130 | 5 | 1 MPC | G389A | 3 | 0 | N | \% AREA | BOTTOM GROOVE 3 DEPOSIT 9-8(\% AREA) |
| 5140 | 5 | IMPC | G3B8A | 3 | 0 | N | \% AREA | BOTTOM GROOVE 3 DEPOSIT 7.9 - 7 (\% AREA) |
| 5150 | 5 | 1MPC | G3B7A | 3 | 0 | N | \% area | BOTTOM GROOVE 3 DEPOSIT 6.9 - 6 (\% AREA) |
| 5160 | 5 | 1 MPC | G3B6A | 3 | 0 | $N$ | \% Area | BOTTOM GROOVE 3 DEPOSIT 5.9-5(\% AREA) |
| 5170 | 5 | 1 MPC | G3B5A | 3 | 0 | $N$ | \% AREA | BOTTOM GROOVE 3 DEPOSIT 4.9 - 4 (\% AREA) |
| 5180 | 5 | 1 MPC | G3B4A | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 3 DEPOSIT 3.9-3(\% AREA) |
| 5190 | 5 | 1 MPC | G3B3A | 3 | 0 | N | \% Area | BOTTOM GROOVE 3 DEPOSIT $2.9-2(\%$ AREA) |
| 5200 | 5 | 1MPC | G3B2A | 3 | 0 | $N$ | \% AREA | BOTTOM GROOVE 3 deposit 1.9-1(\% AREA) |
| 5210 | 5 | 1 MPC | G3B1A | 3 | 0 | N | \% AREA | BOTTOM GROOVE 3 deposit $0.9-0(\%$ AREA) |
| 5220 | 5 | 1 MPC | g3BCLNA | 3 | 0 | $N$ | \% area | bottom groove 3 deposit clean (\% area) |
| 5230 | 5 | 1 MPC | G4THCA | 3 | 0 | N | \% AREA | TOP GROOVE 4 HEAVY CARBON(\% AREA) |
| 5240 | 5 | 1 MPC | G4TMCA | 3 | 0 | $N$ | \% AREA | TOP GROOVE 4 MEDIUM CARBON(\% AREA) |
| 5250 | 5 | 1MPC | G4TLCA | 3 | 0 | $N$ | \% AREA | TOP GROOVE 4 LITE CARBON(\% AREA) |
| 5260 | 5 | 1 MPC | G4T9A | 3 | 0 | N | \% Area | TOP GROOVE 4 deposit 9-8(\% AREA) |
| 5270 | 5 | 1 MPC | G4T8A | 3 | 0 | N | \% ArEA | TOP GROOVE 4 DEPOSIT 7.9 - 7 (\% AREA) |
| 5280 | 5 | 1 MPC | G4T7A | 3 | 0 | N | \% AREA | TOP GROOVE 4 DEPOSIT 6.9 - $6(\%$ AREA) |
| 5290 | 5 | 1 MPC | G4T6A | 3 | 0 | N | \% AREA | TOP GROOVE 4 DEPOSIT 5.9-5(\% AREA) |
| 5300 | 5 | 1MPC | G4T5A | 3 | 0 | $N$ | \% AREA | TOP GROOVE 4 DEPOSIT 4.9 - 4(\% AREA) |
| 5310 | 5 | 1MPC | G4T4A | 3 | 0 | $N$ | \% AREA | TOP GROOVE 4 DEPOSIT 3.9 - 3(\% AREA) |
| 5320 | 5 | 1 MPC | G4T3A | 3 | 0 | $N$ | \% Area | TOP GROOVE 4 DEPOSIT 2.9 - 2 (\% AREA) |
| 5330 | 5 | 1 MPC | G4T2A | 3 | 0 | N | \% AREA | TOP GROOVE 4 DEPOSIT 1.9-1(\% AREA) |
| 5340 | 5 | 1 MPC | G4T1A | 3 | 0 | N | \% AREA | TOP GROOVE 4 DEPOSIT 0.9 - 0(\% AREA) |
| 5350 | 5 | 1 MPC | G4TCLNA | 3 | 0 | $N$ | \% AREA | TOP GROOVE 4 dEPOSIT CLEAN (\% AREA) |
| 5360 | 5 | 1 MPC | G4BHCA | 3 | 0 | N | \% area | BOTTOM GROOVE 4 HEAVY CARBON(\% AREA) |
| 5370 | 5 | 1 MPC | G4BMCA | 3 | 0 | $N$ | \% ArEA | BOTTOM GROOVE 4 MEDIUM CARBON(\% AREA) |
| 5380 | 5 | 1MPC | G4BLCA | 3 | 0 | N | \% AREA | BOTTOM GROOVE 4 LITE CARBON(\% AREA) |
| 5390 | 5 | 1MPC | G489A | 3 | 0 | N | \% AREA | BOTTOM GROOVE 4 DEPOSIT 9 - 8(\% AREA) |
|  |  |  |  |  | G. A3.1 |  | Dictionary (cond |  |


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Test | Field | Field | Decimal |  |  |  |
| Sequence | Form | Area | Name | Length | size |  | Units/Format | Description |
| 5400 | 5 | 1 MPC | 6488A | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 4 deposit 7.9 - 7(\% area) |
| 5410 | 5 | 1 MPC | G487A | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 4 deposit 6.9-6(\% AREA) |
| 5420 | 5 | 1 MPC | G4B6A | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 4 DEPOSIT 5.9-5(\% AREA) |
| 5430 | 5 | 1 MPC | G485A | 3 | 0 | $N$ | \% Area | BOTTOM GROOVE 4 DEPOSIT $4.9-4(\%$ AREA) |
| 5440 | 5 | 1 MPC | G484A | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 4 DEPOSIT 3.9-3(\% AREA) |
| 5450 | 5 | 1 MPC | G483A | 3 | 0 | N | \% AREA | BOTTOM GROOVE 4 deposit 2.9 - 2(\% area) |
| 5460 | 5 | 1 MPC | G482A | 3 | 0 | N | \% AREA | BOTTOM GROOVE 4 DEPOSIT 1.9-1(\% AREA) |
| 5470 | 5 | 1MPC | G481A | 3 | 0 | N | \% area | BOTTOM GROOVE 4 DEPOSIT 0.9-0(\% AREA) |
| 5480 | 5 | 1 MPC | G4BCLNA | 3 | 0 | $N$ | \% area | BOTTOM GROOVE 4 dEPOSIT CLEAN (\% AREA) |
| 5490 | 5 | 1 MPC | R1THCA | 3 | 0 | $N$ | \% area | top Ring 1 HEAVY CARBON(\% AREA) |
| 5500 | 5 | 1 MPC | R1TMCA | 3 | 0 | $N$ | \% area | TOP RING 1 MEDIUM CARBON(\% AREA) |
| 5510 | 5 | 1 MPC | R1TLCA | 3 | 0 | $N$ | \% Area | TOP RING 1 LITE CARBON(\% AREA) |
| 5520 | 5 | 1 MPC | R1T9A | 3 | 0 | N | \% Area | TOP RING 1 DEPOSIT 9 - 8(\% AREA) |
| 5530 | 5 | 1 MPC | R1T8A | 3 | 0 | $N$ | \% area | TOP RING 1 DEPOSIT 7.9 - 7(\% AREA) |
| 5540 | 5 | 1 MPC | R1T7A | 3 | 0 | N | \% area | TOP RING 1 DEPOSIT 6.9-6(\% AREA) |
| 5550 | 5 | 1MPC | R1T6A | 3 | 0 | $N$ | \% area | TOP RING 1 DEPOSIT 5.9-5(\% AREA) |
| 5560 | 5 | 1 MPC | R1T5A | 3 | 0 | $N$ | \% area | TOP RING 1 DEPOSIT 4.9-4(\% AREA) |
| 5570 | 5 | 1 MPC | R1T4A | 3 | 0 | $N$ | \% area | TOP RING 1 DEPOSIT 3.9-3(\% AREA) |
| 5580 | 5 | 1 MPC | R1T3A | 3 | 0 | N | \% area | TOP RING 1 DEPOSIT 2.9 - 2 (\% AREA) |
| 5590 | 5 | 1 MPC | R1T2A | 3 | 0 | N | \% Area | TOP RING 1 DEPOSIT 1.9-1(\% AREA) |
| 5600 | 5 | 1 MPC | R1t1A | 3 | 0 | N | \% AREA | TOP RING 1 DEPOSIT 0.9 -0(\% AREA) |
| 5610 | 5 | 1 MPC | R1TCLNA | 3 | 0 | N | \% area | top ring 1 deposit clean (\% area) |
| 5620 | 5 | 1 MPC | R1BHCA | 3 | 0 | N | \% AREA | BOTTOM RING 1 HEAVY CARBON(\% AREA) |
| 5630 | 5 | 1MPC | R18MCA | 3 | 0 | $N$ | \% AREA | bottom ring 1 MEDIUM Carbon(\% AREA) |
| 5640 | 5 | 1 MPC | R1BLCA | 3 | 0 | $N$ | \% area | bottom Ring 1 LIte CARBON(\% AREA) |
| 5650 | 5 | 1 MPC | R189A | 3 | 0 | $N$ | \% area | Bottom ring 1 deposit 9-8(\% AREA) |
| 5660 | 5 | 1 MPC | R188A | 3 | 0 | $N$ | \% area | botrom ring 1 deposit $7.9-7(\%$ AREA) |
| 5670 | 5 | 1 MPC | R1B7A | 3 | 0 | N | \% AREA | BOTTOM RING 1 DEPOSIT 6.9 - 6 (\% AREA) |
| 5680 | 5 | 1 MPC | R1B6A | 3 | 0 | $N$ | \% area | Bottom ring 1 deposit 5.9-5(\% AREA) |
| 5690 | 5 | 1 MPC | R185A | 3 | 0 | $N$ | \% area | Bottom ring 1 DEPOSIT 4.9-4(\% AREA) |
| 5700 | 5 | 1 MPC | R184A | 3 | 0 | N | \% area | Botrom ring 1 deposit 3.9-3(\% AREA) |
| 5710 | 5 | 1MPC | R183A | 3 | 0 | N | \% area | Botrom ring 1 DEPOSIT 2.9 - 2(\% AREA) |
| 5720 | 5 | 1MPC | R1B2A | 3 | 0 | N | \% area | Bottom ring 1 deposit 1.9-1(\% AREA) |
| 5730 | 5 | 1MPC | R1B1a | 3 | 0 | $N$ | \% area | BOTTOM RING 1 deposit 0.9 - 0(\% AREA) |
| 5740 | 5 | 1 MPC | R1BCLNA | 3 | 0 | $N$ | \% area | bottom ring 1 deposit clean (\% area) |
| 5750 | 5 | 1MPC | R1BKHCA | 3 | 0 | N | \% area | BaCK RING 1 heavy CARBON(\% AREA) |
| 5760 | 5 | 1 MPC | R1BKMCA | 3 | 0 | N | \% AREA | back ring 1 medium carbon(\% area) |
| 5770 | 5 | 1 MPC | R1BKLCA | 3 | 0 | $N$ | \% Area | BACK RING 1 LITE CARBON(\% AREA) |
| 5780 | 5 | 1 MPC | R1BK9A | 3 | 0 | $N$ | \% area | back ring 1 deposit 9-8(\% AREA) |
| 5790 | 5 | 1 MPC | R1BK8A | 3 | 0 | N | \% area | BACK RING 1 DEPOSIT 7.9 - 7(\% AREA) |
| 5800 | 5 | 1 MPC | R1BK7A | 3 | 0 | N | \% area | BACK RING 1 DEPOSIT 6.9 - 6 (\% AREA) |
| 5810 | 5 | 1 MPC | R1BK6A | 3 | 0 | N | \% area | BACK RING 1 DEPOSIT 5.9-5(\% AREA) |
| 5820 | 5 | 1 MPC | R1BK5A | 3 | 0 | N | \% AREA | BACK RING 1 DEPOSIT 4.9-4(\% AREA) |
| 5830 | 5 | 1 MPC | R1BK4A | 3 | 0 | N | \% area | BACK RING 1 DEPOSIT 3.9 - 3(\% AREA) |
| 5840 | 5 | 1 MPC | R1BK3A | 3 | 0 | N | \% area | BACK RING 1 DEPOSIT 2.9 - 2(\% AREA) |
| 5850 | 5 | 1mPC | R1BK2A | 3 | 0 | $N$ | \% Area | back ring 1 deposit 1.9-1(\% AREA) |
| 5860 | 5 | 1MPC | R1BK1A | 3 | 0 | N | \% area | BACK RING 1 DEPOSIT 0.9 - O(\% AREA) |
| 5870 | 5 | 1 MPC | R1BKCLNA | 3 | 0 | N | \% AREA | BACK RING 1 deposit CLEAN (\% AREA) |
| 5880 | 5 | 1 MPC | R2thCA | 3 | 0 | N | \% area | TOP RING 2 heavy CARBON(\% AREA) |
| 5890 | 5 | 1 MPC | R2tMCA | 3 | 0 | $N$ | \% AREA | TOP RING 2 MEDIUM CARBON(\% AREA) |
| 5900 | 5 | 1 MPC | R2tLCA | 3 | 0 | N | \% area | TOP RING 2 LITE CARBON(\% AREA) |
| 5910 | 5 | 1 MPC | R2T9A | 3 | 0 | N | \% AREA | TOP RING 2 DEPOSIT 9 - 8(\% AREA) |
| 5920 | 5 | 1 MPC | R2T8A | 3 | 0 | N | \% AREA | TOP RING 2 DEPOSIT 7.9 - 7(\% AREA) |
| 5930 | 5 | 1 MPC | R2T7A | 3 | 0 | $N$ | \% AREA | TOP RING 2 DEPOSIT 6.9-6(\% AREA) |
|  |  |  |  |  | G. A3.1 | ata D | Dictionary (contir | d) |


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Test | Field | Field | Decimal | ata |  |  |
| Sequence | Form | Area | Name | Length | Size |  | Units/Format | Description |
| 5940 | 5 | 1MPC | R2T6A | 3 | 0 | $N$ | \% area | top ring 2 deposit 5.9 - 5(\% AREA) |
| 5950 | 5 | 1 MPC | R2T5A | 3 | 0 | $N$ | \% area | TOP RING 2 deposit 4.9 - 4(\% AREA) |
| 5960 | 5 | 1mPC | R2T4A | 3 | 0 | $N$ | \% area | TOP RING 2 DEPOSIT 3.9 - 3(\% AREA) |
| 5970 | 5 | 1MPC | R2T3A | 3 | 0 | $N$ | \% Area | TOP RING 2 deposit 2.9 - $2(\%$ AREA $)$ |
| 5980 | 5 | 1 MPC | R2T2A | 3 | 0 | $N$ | \% area | top ring 2 deposit 1.9-1(\% AREA) |
| 5990 | 5 | 1 MPC | R2T1A | 3 | 0 | $N$ | \% AREA | TOP RING 2 deposit 0.9 - O(\% AREA) |
| 6000 | 5 | 1 mPC | R2TCLINA | 3 | 0 | $N$ | \% area | top ring 2 deposit CLEAN (\% AREA) |
| 6010 | 5 | 1MPC | R2BHCA | 3 | 0 | $N$ | \% area | BOTTOM RING 2 heavy carbon(\% AREA) |
| 6020 | 5 | 1 MPC | R2BmCA | 3 | 0 | $N$ | \% area | Bottom ring 2 MEdium Carbon(\% AREA) |
| 6030 | 5 | 1 MPC | R2BLCA | 3 | 0 | $N$ | \% area | bottom ring 2 LIte Carbon(\% AREA) |
| 6040 | 5 | 1 MPC | R2B9A | 3 | 0 | $N$ | \% area | Bottom ring 2 deposit 9-8(\% area) |
| 6050 | 5 | 1 MPC | R2B8A | 3 | 0 | N | \% area | BOTTOM RING 2 DEPOSIT $7.9-7(\%$ AREA ) |
| 6060 | 5 | 1 MPC | R2B7A | 3 | 0 | N | \% area | Bottom ring 2 deposit 6.9-6(\% AREA) |
| 6070 | 5 | 1MPC | R2B6A | 3 | 0 | $N$ | \% Area | BOTTOM RING 2 DEPOSIT 5.9-5(\% AREA) |
| 6080 | 5 | 1 MPC | R285A | 3 | 0 | $N$ | \% AREA | BOTTOM RING 2 DEPOSIT 4.9 - 4(\% AREA) |
| 6090 | 5 | 1MPC | R2B4A | 3 | 0 | $N$ | \% area | BOTTOM RING 2 dEPOSIT 3.9-3(\% AREA) |
| 6100 | 5 | 1 MPC | R2B3A | 3 | 0 | $N$ | \% area | Bottom ring 2 dEPOSIT 2.9 - $2(\%$ AREA) |
| 6110 | 5 | 1mPC | R2B2A | 3 | 0 | $N$ | \% AREA | BOTTOM RING 2 DEPOSIT 1.9 - 1(\% AREA) |
| 6120 | 5 | 1 MPC | R2B1A | 3 | 0 | $N$ | \% AREA | Bottom ring 2 deposit 0.9 - 0(\% AREA) |
| 6130 | 5 | 1 MPC | R2BCLNA | 3 | 0 | $N$ | \% area | BOTTOM RING 2 dEPOSIT CLEAN (\% AREA) |
| 6140 | 5 | 1MPC | R2BKHCA | 3 | 0 | $N$ | \% area | baCK ring 2 heavy carbon \% AREA) |
| 6150 | 5 | 1 MPC | R2BKMCA | 3 | 0 | $N$ | \% AREA | baCk ring 2 MEDIUM CARBON(\% AREA) |
| 6160 | 5 | 1MPC | R2BKLCA | 3 | 0 | $N$ | \% AREA | back ring 2 LITE CARBON(\% AREA) |
| 6170 | 5 | 1 MPC | R2BK9A | 3 | 0 | $N$ | \% AREA | BACK RING 2 dEPOSIT 9 - 8(\% AREA) |
| 6180 | 5 | 1 MPC | R2BK8A | 3 | 0 | N | \% area | BACK RING 2 deposit 7.9-7(\% area) |
| 6190 | 5 | 1MPC | R2BK7A | 3 | 0 | $N$ | \% area | BACK RING 2 DEPOSIT 6.9 - 6 (\% AREA) |
| 6200 | 5 | 1 MPC | R2BK6A | 3 | 0 | $N$ | \% area | BACK RING 2 DEPOSIT 5.9-5(\% AREA) |
| 6210 | 5 | 1 MPC | R2BK5A | 3 | 0 | $N$ | \% area | BACK RING 2 DEPOSIT 4.9 - 4(\% AREA) |
| 6220 | 5 | 1 mPC | R2BK4A | 3 | 0 | N | \% area | BACK RING 2 DEPOSIT 3.9-3(\% AREA) |
| 6230 | 5 | 1 mPC | R2BK3A | 3 | 0 | $N$ | \% area | BACK RING 2 DEPOSIT 2.9 - 2 (\% AREA) |
| 6240 | 5 | 1 MPC | R2BK2A | 3 | 0 | $N$ | \% area | BACK RING 2 DEPOSIT 1.9 - $1(\%$ AREA) |
| 6250 | 5 | 1 MPC | R2BK1A | 3 | 0 | $N$ | \% area | BACK RING 2 DEPOSIT 0.9 - 0(\% AREA) |
| 6260 | 5 | 1MPC | R2BKCLNA | 3 | 0 | $N$ | \% AREA | baCk ring 2 deposit clean (\% area) |
| 6270 | 5 | 1MPC | R3THCA | 3 | 0 | N | \% AREA | TOP RING 3 HEAVY CARBON(\% AREA) |
| 6280 | 5 | 1MPC | R3TMCA | 3 | 0 | N | \% area | TOP RING 3 MEDIUM CARBON(\% AREA) |
| 6290 | 5 | 1 MPC | R3TLCA | 3 | 0 | $N$ | \% area | TOP RING 3 LITE CARBON(\% AREA) |
| 6300 | 5 | 1 MPC | R3T9A | 3 | 0 | $N$ | \% Area | TOP RING 3 DEPOSIT 9 - 8(\% AREA) |
| 6310 | 5 | 19PC | R3T8A | 3 | 0 | $N$ | \% AREA | TOP RING 3 DEPOSIT 7.9-7(\% AREA) |
| 6320 | 5 | 1 MPC | R3T7A | 3 | 0 | $N$ | \% AREA | TOP RING 3 DEPOSIT 6.9-6(\% AREA) |
| 6330 | 5 | 1 MPC | R3T6A | 3 | 0 | N | \% AREA | TOP RING 3 DEPOSIT 5.9-5(\% AREA) |
| 6340 | 5 | 1 MPC | R3T5A | 3 | 0 | $N$ | \% area | TOP RING 3 DEPOSIT 4.9 - 4(\% AREA) |
| 6350 | 5 | 1 MPC | R3T4A | 3 | 0 | $N$ | \% area | TOP RING 3 DEPOSIT 3.9-3(\% AREA) |
| 6360 | 5 | 1 MPC | R3T3A | 3 | 0 | $N$ | \% AREA | TOP RING 3 DEPOSIT 2.9 - 2(\% AREA) |
| 6370 | 5 | 1 MPC | R3T2A | 3 | 0 | $N$ | \% AREA | TOP RING 3 DEPOSIT 1.9-1(\% AREA) |
| 6380 | 5 | 1 MPC | R3T1A | 3 | 0 | $N$ | \% AREA | TOP RING 3 DEPOSIT 0.9 - O(\% AREA) |
| 6390 | 5 | 1 mPC | R3TCLNA | 3 | 0 | $N$ | \% AREA | TOP RING 3 DEPOSIT CLEAN (\% AREA) |
| 6400 | 5 | 1 MPC | R3BHCA | 3 | 0 | $N$ | \% area | BOTTOM RING 3 HEAVY CARBON(\% AREA) |
| 6410 | 5 | 1MPC | R3BMCA | 3 | 0 | N | \% AREA | BOTTOM RING 3 MEDIUM CARBON(\% AREA) |
| 6420 | 5 | 1 MPC | R3BLCA | 3 | 0 | N | \% area | Bottom ring 3 LITE CARBON(\% AREA) |
| 6430 | 5 | 1 MPC | R3B9A | 3 | 0 | $N$ | \% AREA | 80ttom ring 3 deposit 9-8(\% AREA) |
| 6440 | 5 | 1 MPC | R3B8A | 3 | 0 | $N$ | \% area | BOTTOM RING 3 DEPOSIT 7.9 - 7\% AREA) |
| 6450 | 5 | 1MPC | R3B7A | 3 | 0 | N | \% AREA | BOTTOM RING 3 DEPOSIT 6.9 - 6(\% AREA) |
| 6460 | 5 | 1 MPC | R3B6A | 3 | 0 | N | \% AREA | BOTTOM RING 3 DEPOSIT 5.9-5(\% AREA) |
| 6470 | 5 | 1MPC | R3B5A | 3 | 0 | N | \% AREA | BOTTOM RING 3 DEPOSIT 4.9 - 4(\% AREA) |

FIG. A3.1 Data Dictionary (continued)


| 6480 | 5 | 1MPC | R3B4A | 3 | 0 | $N$ | \% AREA | Bottom ring 3 deposit 3.9-3(\% AREA) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6490 | 5 | 1 MPC | R3B3A | 3 | 0 | $N$ | \% area | Bottom ring 3 DEPOSIT 2.9 - 2 (\% AREA) |
| 6500 | 5 | 1 MPC | R3B2A | 3 | 0 | N | \% area | Bottom ring 3 DEPOSIT 1.9-1(\% area) |
| 6510 | 5 | 1MPC | R381A | 3 | 0 | $N$ | \% area | Bottom ring 3 deposit 0.9 - 0(\% area) |
| 6520 | 5 | 1 MPC | R3BCLNA | 3 | 0 | $N$ | \% area | Bottom ring 3 deposit clean (\% area) |
| 6530 | 5 | 1MPC | R3BXHCA | 3 | 0 | N | \% area | BaCK RING 3 Heavycarbon(\% AREA) |
| 6540 | 5 | 1 MPC | R3BKMCA | 3 | 0 | $N$ | \% area | baCK RINg 3 MEDIUM CARBON(\% AREA) |
| 6550 | 5 | 1 MPC | R3BkLCA | 3 | 0 | $N$ | \% area | back ring 3 LIte Carbon(\% AREA) |
| 6560 | 5 | 1MPC | R3BK9A | 3 | 0 | $N$ | \% AREA | BACK RING 3 deposit 9-8(\% AREA) |
| 6570 | 5 | 1MPC | R3BK8A | 3 | 0 | $N$ | \% area | BACK RING 3 DEPOSIT 7.9-7(\% AREA) |
| 6580 | 5 | 1MPC | R3BK7A | 3 | 0 | $N$ | \% area | BACK RING 3 DEPOSIT 6.9 - 6(\% AREA) |
| 6590 | 5 | 1 MPC | R3B66A | 3 | 0 | N | \% area | back ring 3 deposit 5.9-5(\% AREA) |
| 6600 | 5 | 1 MPC | R3865A | 3 | 0 | $N$ | \% area | BACK RING 3 DEPOSIT 4.9 - 4(\% AREA) |
| 6610 | 5 | 1 MPC | R3BK4A | 3 | 0 | $N$ | \% area | BACK RING 3 DEPOSIT 3.9-3(\% AREA) |
| 6620 | 5 | 1MPC | R3BK3A | 3 | 0 | $N$ | \% area | BACK RING 3 DEPOSIT 2.9 - 2(\% AREA) |
| 6630 | 5 | 1 MPC | R38k2a | 3 | 0 | $N$ | \% area | back ring 3 deposit 1.9-1(\% area) |
| 6640 | 5 | 1 MPC | R3BK1A | 3 | 0 | $N$ | \% area | BACK RING 3 DEPOSIT 0.9 - 0(\% AREA) |
| 6650 | 5 | 1 MPC | R3BKCLINA | 3 | 0 | $N$ | \% area | BACK RING 3 DEPOSIT CLEAN (\% AREA) |
| 6660 | 5 | 1 MPC | R4THCA | 3 | 0 | $N$ | \% area | TOP RING 4 HEAVY CARBON(\% AREA) |
| 6670 | 5 | 1 MPC | R4TMCA | 3 | 0 | $N$ | \% area | TOP RING 4 MEDIUM CARBON(\% AREA) |
| 6680 | 5 | 1 MPC | R4TLCA | 3 | 0 | $N$ | \% area | TOP RING 4 LITE CARBON(\% AREA) |
| 6690 | 5 | 1 MPC | R4T9A | 3 | 0 | N | \% area | TOP RING 4 DEPOSIT 9-8(\% AREA) |
| 6700 | 5 | 1 MPC | R4T8A | 3 | 0 | $N$ | \% area | TOP RING 4 DEPOSIT 7.9 - 7(\% AREA) |
| 6710 | 5 | 1MPC | R4T7A | 3 | 0 | $N$ | \% area | TOP RING 4 DEPOSIT 6.9-6(\% AREA) |
| 6720 | 5 | 1 MPC | R4T6A | 3 | 0 | $N$ | \% area | TOP RING 4 DEPOSIT 5.9-5(\% AREA) |
| 6730 | 5 | 1 MPC | R4T5A | 3 | 0 | $N$ | \% area | TOP RING 4 DEPOSIT 4.9 - 4 (\% AREA) |
| 6740 | 5 | 1MPC | R4T4A | 3 | 0 | N | \% area | TOP RING 4 DEPOSIT 3.9-3(\% AREA) |
| 6750 | 5 | 1 MPC | R4T3A | 3 | 0 | N | \% AREA | TOP RING 4 DEPOSIT 2.9-2(\% AREA) |
| 6760 | 5 | 1MPC | R4T2A | 3 | 0 | $N$ | \% area | TOP RING 4 DEPOSIT 1.9-1(\% AREA) |
| 6770 | 5 | 1MPC | R4T1A | 3 | 0 | $N$ | \% AREA | TOP RING 4 DEPOSIT 0.9 - 0(\% AREA) |
| 6780 | 5 | 1MPC | R4TCLNA | 3 | 0 | $N$ | \% area | TOP RING 4 DEPOSIT CLEAN (\% AREA) |
| 6790 | 5 | 1 MPC | R4BHCA | 3 | 0 | $N$ | \% area | Bottom ring 4 HEAVY CARBON(\% AREA) |
| 6800 | 5 | 1MPC | R4BMCA | 3 | 0 | $N$ | \% area | BOTTOM RING 4 MEDIUM CARBON(\% AREA) |
| 6810 | 5 | 1 MPC | R4BLCA | 3 | 0 | $N$ | \% area | BOTtOM RING 4 LITE CARBON(\% AREA) |
| 6820 | 5 | 1MPC | R489A | 3 | 0 | $N$ | \% AREA | BOTTOM RING 4 DEPOSIT 9-8(\% AREA) |
| 6830 | 5 | 1 MPC | R488A | 3 | 0 | $N$ | \% area | Bottom ring 4 DEPOSIT 7.9-7(\% AREA) |
| 6840 | 5 | 1MPC | R487A | 3 | 0 | $N$ | \% area | BOTTOM RING 4 DEPOSIT 6.9-6(\% AREA) |
| 6850 | 5 | 1 MPC | R486A | 3 | 0 | $N$ | \% area | BOTTOM RING 4 DEPOSIT 5.9-5(\% AREA) |
| 6860 | 5 | 1MPC | R4B5A | 3 | 0 | $N$ | \% area | BOTTOM RING 4 DEPOSIT 4.9 - 4 (\% AREA) |
| 6870 | 5 | 1MPC | R484A | 3 | 0 | $N$ | \% area | Bottom ring 4 DEPOSIT 3.9-3(\% AREA) |
| 6880 | 5 | 1 MPC | R4B3A | 3 | 0 | N | \% area | Bottom ring 4 DEPOSIT 2.9 - 2(\% AREA) |
| 6890 | 5 | 1 MPC | R4B2A | 3 | 0 | $N$ | \% area | BOTTOM RING 4 DEPOSIT 1.9-1(\% AREA) |
| 6900 | 5 | 1 MPC | R481A | 3 | 0 | $N$ | \% area | BOTTOM RING 4 DEPOSIT 0.9-0(\% AREA) |
| 6910 | 5 | 1 MPC | R4BCLINA | 3 | 0 | $N$ | \% area | Bottom ring 4 DEPOSIT CLEAN (\% AREA) |
| 6920 | 5 | 1MPC | R4BKHCA | 3 | 0 | $N$ | \% AREA | BaCK RING 4 HEAVY CARBON(\% AREA) |
| 6930 | 5 | 1 MPC | R4BKMCA | 3 | 0 | $N$ | \% area | BACK RING 4 MEDIUM CARBON(\% AREA) |
| 6940 | 5 | 1 MPC | R4BKLCA | 3 | 0 | $N$ | \% area | BACK RING 4 LITE CARBON(\% AREA) |
| 6950 | 5 | 1 MPC | R4BK9A | 3 | 0 | N | \% Area | BACK RING 4 DEPOSIT 9-8 (\% AREA) |
| 6960 | 5 | 1 MPC | R4BK8A | 3 | 0 | $N$ | \% area | BACK RING 4 DEPOSIT $7.9-7(\%$ AREA $)$ |
| 6970 | 5 | 1 MPC | R4BK7A | 3 | 0 | N | \% area | BACK RING 4 DEPOSIT 6.9 - 6 (\% AREA) |
| 6980 | 5 | 1 MPC | R48K6A | 3 | 0 | $N$ | \% area | BACK RING 4 DEPOSIT 5.9-5(\% AREA) |
| 6990 | 5 | 1 MPC | R4BK5A | 3 | 0 | $N$ | \% area | BACK RING 4 DEPOSIT 4.9 - 4 (\% AREA) |
| 7000 | 5 | 1 MPC | R48K4A | 3 | 0 | $N$ | \% AREA | BACK RING 4 DEPOSIT 3.9-3(\% AREA) |
| 7010 | 5 | 1MPC | R4BK3A | 3 | 0 | N | \% AREA | BACK RING 4 DEPOSIT 2.9 - 2(\% AREA) |
|  |  |  |  |  |  |  | ctionary |  |



| 7020 | 5 | 1 MPC | R4BK2A | 3 | 0 | $N$ | \% area | back ring 4 deposit 1.9-1(\% area) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7030 | 5 | 1MPC | R4BK1A | 3 | 0 | $N$ | \% area | BACK RING 4 DEPOSIT 0.9 - 0(\% AREA) |
| 7040 | 5 | 1MPC | R4BKCLNA | 3 | 0 | N | \% area | back ring 4 deposit clean (\% area) |
| 7050 | 5 | 1 MPC | CROWNAD | 70 | 0 | c |  | ADDITIONAL DEPOSIT \& CONDITION RATINGS PISton Croun |
| 7060 | 5 | 1 MPC | SLOTSAD | 70 | 0 | c |  | additional deposit \& CONDItion ratings oil ring slots |
| 7070 | 5 | 1 MPC | SKIRTAD | 70 | 0 | C |  | ADDITIONAL DEPOSIT \& CONDITION RATINGS PISTON SKIRT |
| 7080 | 5 | 1MPC | LINERAD | 70 | 0 | c |  | Additional deposit \& Condition ratings liner |
| 7090 | 5 | 1MPC | RINGSAD | 70 | 0 | c |  | ADDITIONAL DEPOSIT \& CONDITION RATINGS RINGS |
| 7100 | 5 | 1 MPC | COMMAD | 70 | 0 | c |  | additional deposit \& condition ratings comment |
| 7110 | 5a | 1 MPC | RRNO | 10 | 0 | c |  | referee rating number |
| 7120 | 5a | 1 MPC | RRDATE | 8 | 0 | c | YYYYMMDD | REFEREE RATING DATE (YYYYMMdD) |
| 7130 | 5a | 1MPC | RRINIT | 3 | 0 | c |  | Referee rating initials |
| 7140 | 5a | 1 MPC | RRG1 HCA | 3 | 0 | $N$ | \% Area | Referee groove \#1 HC-1.0 carbon area Percent (\% area) |
| 7150 | 5a | 1 MPC | RRG1HCD | 6 | 2 | $N$ | DEMERITS | REFEREE GROOVE \#1 HC-1.0 CARBON DEMERITS (DEMERITS) |
| 7160 | 5a | 1 MPC | RRG2HCA | 3 | 0 | $N$ | \% AREA | REFEREE GROOVE \#2 HC-1.0 Carbon area percent (\% AREA) |
| 7170 | 5a | 1 MPC | RRG2 ${ }^{\text {HCD }}$ | 6 | 2 | $N$ | DEMERITS | Referee groove \#2 hc-1.0 carbon demerits (demerits) |
| 7180 | 5a | 1 MPC | RRG3HCA | 3 | 0 | $N$ | \% area | Referee groove \#3 hc-1.0 Carbon area percent (\% area) |
| 7190 | 5a | 1MPC | RRG3HCD | 6 | 2 | $N$ | DEMERITS | REFEREE GROOVE \#3 HC-1.0 CARBON DEMERITS (DEMERITS) |
| 7200 | 5a | 1 MPC | RRG4HCA | 3 | 0 | $N$ | \% AREA | referee groove \#4 hc-1.0 Carbon area percent (\% AREA) |
| 7210 | 5a | 1 MPC | RRG4HCD | 6 | 2 | $N$ | DEMERITS | REFEREE GROOVE \#4 HC-1.0 CARBON DEMERITS (DEMERITS) |
| 7220 | 5a | 1 MPC | RRL2HCA | 3 | 0 | $N$ | \% AREA | referee land \#2 hc-1.0 carbon area percent (\% area) |
| 7230 | 5a | 1MPC | RRL2HCD | 6 | 2 | $N$ | demerits | REFEREE LAND \#2 HC-1.0 CARBON DEMERITS (DEMERITS) |
| 7240 | 5a | 1MPC | RRL3HCA | 3 | 0 | $N$ | \% AREA | REFEREE LAND \#3 HC-1.0 CARBON AREA PERCENT (\% area) |
| 7250 | 5a | 1MPC | RRL3HCD | 6 | 2 | N | demerits | REFEREE LAND \#3 HC-1.0 CARBON DEMERITS (DEMERITS) |
| 7260 | 5a | 1MPC | RRL4HCA | 3 | 0 | N | \% AREA | referee land \#4 hc-1.0 carbon area percent (\% area) |
| 7270 | 5a | 1 MPC | RRL4HCD | 6 | 2 | $N$ | DEMERITS | REFEREE LAND \#4 HC-1.0 CARBON DEMERITS (DEMERITS) |
| 7280 | 5a | 1MPC | RRG1MCA | 3 | 0 | $N$ | \% AREA | REFEREE GROOVE \#1 MC-1.0 CARBON AREA PERCENT (\% area) |
| 7290 | 5a | 1MPC | RRG1MCD | 6 | 2 | N | DEMERITS | REFEREE GROOVE \#1 MC-1.0 CARBON DEMERITS (DEMERITS) |
| 7300 | 5a | 1MPC | RRGZMCA | 3 | 0 | $N$ | \% Area | Referee groove \#2 Mc-1.0 carbon area percent (\% area) |
| 7310 | 5a | 1MPC | RRG2MCD | 6 | 2 | $N$ | DEMERITS | Referee groove \#2 mc-1.0 CARBON DEMERItS (DEmerits) |
| 7320 | 5a | 1 MPC | RRG3MCA | 3 | 0 | $N$ | \% area | Referee groove \#3 Mc-1.0 carbon area percent (\% area) |
| 7330 | 5a | 1MPC | RRG3MCD | 6 | 2 | $N$ | DEMERITS | REFEREE GROOVE \#3 MC-1.0 CARBON DEMERITS (DEmerits) |
| 7340 | 5a | 1MPC | RRG4MCA | 3 | 0 | $N$ | \% AREA | Referee groove \#4 Mc-1.0 carbon area percent (\% area) |
| 7350 | 5a | MMPC | RRG4MCD | 6 | 2 | $N$ | DEMERITS | REFEREE GROOVE \#4 MC-1.0 CARBON DEMERITS (DEMERITS) |
| 7360 | 5a | 1 MPC | RRGILCA | 3 | 0 | $N$ | \% AREA | REFEREE GROOVE \#1 lc-1.0 CARBON AREA PERCENT (\% AREA) |
| 7370 | 5a | 1 MPC | RRG1LCD | 6 | 2 | N | DEmerits | REFEREE GROOVE \#1 LC-1.0 CARBON DEMERItS (DEmerits) |
| 7380 | 5a | 1MPC | RRG2LCA | 3 | 0 | $N$ | \% AREA | Referee groove \#2 lc-1.0 carbon area percent (\% area) |
| 7390 | 5 a | 1 MPC | RRG2LCD | 6 | 2 | $N$ | DEMERITS | REFEREE GROOVE \#2 LC-1.0 CARBON DEMERITS (DEmerits) |
| 7400 | 5 a | 1 MPC | RRG3LCA | 3 | 0 | $N$ | \% AREA | Referee groove \#3 lc-1.0 Carbon area percent (\% AREA) |
| 7410 | 5 a | 1 MPC | RRG3LCD | 6 | 2 | N | demerits | referee groove \#3 lc-1.0 carbon demerits (demerits) |
| 7420 | 5a | 1 MPC | RRG4LCA | 3 | 0 | $N$ | \% AREA | referee groove \#4 lc-1.0 carbon area percent (\% area) |
| 7430 | 5a | 1MPC | RRG4LCD | 6 | 2 | $N$ | DEMERITS | REFEREE GROOVE \#4 LC-1.0 CARBON DEMERITS (DEMERITS) |
| 7440 | 5a | 1MPC | RRL2LCA | 3 | 0 | $N$ | \% AREA | referee land \#2 lc-1.0 carbon area percent (\% area) |
| 7450 | 5a | 1 MPC | RRL2LCD | 6 | 2 | $N$ | demerits | Referee land \#2 LC-1.0 CARBON DEMERITS (DEMERITS) |
| 7460 | 5a | 1 MPC | RRL3LCA | 3 | 0 | N | \% AREA | referee land \#3 lc-1.0 carbon area percent (\% area) |
| 7470 | 5 a | 1 MPC | RRL3LCD | 6 | 2 | $N$ | DEmerits | Referee land \#3 lc-1.0 carbon demerits (DEmerits) |
| 7480 | 5a | 1 MPC | RRL4LCA | 3 | 0 | $N$ | \% AREA | REFEREE Land \# 4 LC-1.0 carbon area percent (\% area) |
| 7490 | 5 | 1 MPC | RRL4LCD | 6 | 2 | $N$ | demerits | REFEREE LAND \# 4 LC-1.0 CARBON DEMERITS (DEMERITS) |
| 7500 | 5a | 1 MPC | RG1aCtot | 3 | 0 | N | \% AREA | referee total groove \#1 Carbon area percent (\% area) |
| 7510 | 5 a | 1 MPC | RG1DCTOT | 6 | 2 | N | demerits | Referee total groove \#1 Carbon demerits (demerits) |
| 7520 | 5a | 1 MPC | RG2ACTOT | 3 | 0 | $N$ | \% area | Referee total groove \#2 carbon area percent (\% area) |
| 7530 | 5a | 1 MPC | RG2DCTOT | 6 | 2 | $N$ | demerits | referee total groove \#2 Carbon demerits (demerits) |
| 7540 | 5a | 1 MPC | RG3ACTOT | 3 | 0 | $N$ | \% AREA | Referee total groove \#3 Carbon area percent (\% area) |
| 7550 | 5a | 1 MPC | RG3DCTOT | 6 | 2 | $N$ | DEMERITS | Referee total groove \#3 Carbon demerits (demerits) |
|  |  |  |  |  | FIG. A3.1 Data Dictionary (continued) |  |  |  |

22-sep-1998
Test
Sequence Form Area

Report: ASTM Data Dictionary
Field Decimal Data Length Size Type Units/Format

## Description

7560 5a 1MPC RG4ACTOT
$\begin{array}{lll}7570 & 5 a & \text { 1MPC } \\ 7580 & 5 \mathrm{a} & \text { 1MPC }\end{array}$
7590 5a 1MPC

7600 5a 1MPC
7610 5a 1MPC
$\begin{array}{lll}7620 & 5 \mathrm{a} & \text { MMPC } \\ 7630 & 5 \mathrm{a} & \text { 1MPC } \\ 7640 & 5 \mathrm{a} & \text { MMPC }\end{array}$
$\begin{array}{lll}7640 & 5 a & \text { MPPC } \\ 7650 & 5 \mathrm{a} & \text { 1MPC }\end{array}$
7660 5a IMPC
$\begin{array}{lll}7670 & 5 a & \text { IMPC } \\ 7680 & 5 a & \text { MPC }\end{array}$
7690 5a 1MPC

7700 5a 1MPC
7710 5a 1MPC
$\begin{array}{lll}7720 & 5 a & \text { MPC } \\ 7730 & 5 a & \text { MPC }\end{array}$
$\begin{array}{lll}7730 & 5 a & \text { MMPC } \\ 7740 & 5 a & \text { MPPC }\end{array}$
7750 5a 1MPC
7760 5a 1MPC
7770 5a MMPC
$\begin{array}{lll}7780 & 5 a & \text { 1MPC } \\ 7790 & 5 a & \text { 1MPC }\end{array}$
7800 5a 1MPC
7810 5a 1MPC
7820 5a $\quad$ MPC
$\begin{array}{lll}7830 & 5 a & \text { 1MPC } \\ 7840 & 5 a & \text { 1MPC }\end{array}$
7850 5a 1MPC
7860 5a 1MPC
$\begin{array}{lll}7870 & 5 a & \text { IMPC } \\ 7880 & 5 a & \text { MPC }\end{array}$
$\begin{array}{lll}7880 & 5 a & \text { 1MPC } \\ 7890 & 5 a & \text { 1MPC }\end{array}$
7900 5a 1MPC
7910 5a IMPC
7920 5a 1MPC
$\begin{array}{lll}7930 & 5 a & \text { 1MPC } \\ 7940 & 5 a & \text { 1MPC }\end{array}$
$\begin{array}{lll}7950 & 5 a & 1 \text { MPC } \\ 7960 & 5 a & \text { 1MPC }\end{array}$
7970 5a 1MPC
$\begin{array}{llll}7980 & 5 a & 1 M P C & \\ 7990 & 5 a & 1 M P C & \end{array}$
$8000 \begin{array}{lll}795 & 5 a & \text { MPC }\end{array}$
8010 5a 1MPC
8020 5a 1MPC
$\begin{array}{lll}8030 & 5 a & \text { MMPC } \\ 8040 & 5 a & \text { MPC }\end{array}$
8050 5a TMPC
8060 5a 1MPC
$\begin{array}{lll}8070 & 5 a & \text { 1MPC } \\ 8080 & 5 a & \text { 1MPC } \\ 8090 & 5 a & 1 M P C\end{array}$
RG40CTOT
RLzactot
RL2DCTOT
RL3ACTOT
RL3DCTOT
RL4ACTOT
RL4DCTOT
RRG1L9A
RRG1L9D
RRG2L9A
RRG2L9D
RRG3L9A
RRG3L9D
RRG4L9A
RRG4L90
RRL2L9A
RRL2L9D
RRL3L9A RRL3L9D RRL4L9A RRL4L90 RRG1L8A RRG2L8A RRG2L8D RRG3L8A RRG3L8D
RRG4L8A RRG4L8D RRL2L8A
RRL2L8D
RRL3L8A
RRL3L8D
RRL4L8A
RRL4L8D

RRG1L7A

RRG1LTD 62 | N DEMERITS |
| :--- |

RRG2L7A $30 \quad \mathrm{~N}$ \% AREA
RRGZLTD 620 N DEMERITS
RRG3L7A $3 \quad 0 \quad N \quad$ \% AREA
RRG3LTD $6 \quad 2 \quad N$ DEMERITS
RRG4L7A $3 \quad 0 \quad N$ \% AREA
RRG4LTD $63 \quad 2 \quad$ N DEMERITS
RRL2L7A 3 N 0 AREA
RRL2LTD 6
RRL3L7A $3 \quad 0 \quad N$ \% AREA

RRL3L7D 6 RRL4L7A 3 N 0 AREA RRL4LTD 6 RRG1L6A $3 \quad 0 \quad N$ \% AREA
RRG1L6D 6 N DEMERITS
$\begin{array}{lllll}\text { RRG2L6A } & 3 & 0 & N & \text { \% AREA } \\ \text { RRG2L6D } & 6 & 2 & N & \text { DEMERITS }\end{array}$
referee total groove \#4 carbon area percent (\% area) referee total groove \#4 carbon demerits (demerits) referee total land \#2 carbon area percent (\% area) referee total land \#2 Carbon demerits (demerits) referee total land \#3 carbon area percent (\% area) referee total land \#3 carbon demerits (demerits) referee total land \#4 carbon area percent (\% area) referee total land \#4 CARBON DEMERITS (DEMERITS) referee groove \#1 8-9 lacouer area percent (\% area) referee groove \#1 8-9 lacquer demerits (demerits) referee groove \#2 8-9 Lacquer area percent (\% area) Referee groove \#2 8-9 lacquer demerits (demerits) REFEREE GROOVE \#3 8-9 LACQUER AREA PERCENT (\% AREA) referee groove \#3 8-9 lacquer demerits (demerits) referee groove \#4 8-9 lacquer area percent (\% area) referee groove \#4 8-9 lacquer demerits (demerits) referee land \#2 8-9 lacquer area percent (\% area) REFEREE LAND \#2 8-9 LACQUER DEMERITS (DEMERITS) referee land \#3 8-9 lacquer area percent (\% area) referee land \#3 8-9 lacauer demerits (demerits) referee land \#4 8-9 lacquer area percent (\% area) REFEREE LAND \#4 8-9 LACQUER DEMERITS (DEMERITS) referee groove \#1 7-7.9 lacQuer area percent (\% area) REFEREE GROOVE \#1 7-7.9 LACQUER DEMERITS (DEMERITS) referee groove \#2 7-7.9 LacQuer area percent (\% area) referee groove \#2 7-7.9 LacQuer demerits (Demerits) referee groove \#3 7-7.9 lacquer area percent (\% area) REFEREE GROOVE \#3 7-7.9 LACQUER DEMERITS (DEMERITS) referee groove \#4 7-7.9 LacQuer area percent (\% area) REFEREE GROOVE \#4 7-7.9 LACQUER DEMERITS (DEMERITS) referee land \#2 7-7.9 lacquer area percent (\% area) referee land \#2 7-7.9 lacquer demerits (demerits) REFEREE LAND \#3 7-7.9 LACQUER AREA PERCENT (\% AREA) referee land \#3 7-7.9 lacquer demerits (demerits) referee land \#4 7-7.9 Lacquer area percent (\% area) referee land \#4 7-7.9 lacquer demerits (demerits) referee groove \#1 6-6.9 lacquer area percent (\% area) REFEREE GROOVE \#1 6-6.9 LACQUER DEMERITS (DEMERITS) Referee groove \#2 6-6.9 lacquer area percent (\% area) REFEREE GROOVE \#2 6-6.9 LACQUER DEMERITS (DEMERITS) referee groove \#3 6-6.9 lacquer area percent (\% area) REFEREE GROOVE \#3 6-6.9 LACQUER DEMERITS (DEMERITS) referee groove \#4 6-6.9 lacQuer area percent (\% area) REFEREE GROOVE \#4 6-6.9 LACQUER DEMERITS (DEMERITS) referee land \#2 6-6.9 Lacquer area percent (\% area) referee land \#2 6-6.9 lacquer demerits (demerits) referee land \#3 6-6.9 lacquer area percent (\% area) REFEREE LAND \#3 6-6.9 LACQUER DEMERITS (DEMERITS) REFEREE LAND \#4 6-6.9 LACQUER AREA PERCENT (\% AREA) referee land \#4 6-6.9 lacquer demerits (demerits) referee groove \#1 5-5.9 lacquer area percent (\% area) referee groove \#1 5-5.9 lacquer demerits (demerits) referee groove \#2 5-5.9 lacquer area percent (\% area) REFEREE GROOVE \#2 5-5.9 LACQUER DEMERITS (DEMERITS)

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Field
Name

Report: ASTM Data Dictionary
Field Decimal Data Length Size Type Units/Format

Description

| 8100 | 5a | 1 MPC | RRG3L6A | 3 | 0 | $N$ | \% area | Refere | groove \#3 5-5.9 lacquer area percent (\% area) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8110 | 5a | 1 MPC | RRG3L6D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#3 5-5.9 LaCQuer demerits (DEMERITS) |
| 8120 | 5 | 1 MPC | RRG4L6A | 3 | 0 | N | \% area | Refere | Groove \#4 5-5.9 LacQuer area percent (\% area) |
| 8130 | 5a | 1 MPC | RRG4L6D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#4 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 8140 | 5a | 1 MPC | RRL2L6A | 3 | 0 | $N$ | \% AREA | REFERE | Land \#2 5-5.9 LacQuer area percent (\% area) |
| 8150 | 5a | 1MPC | RRL2L60 | 6 | 2 | $N$ | DEMERITS | Refere | LAND \#2 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 8160 | 5a | 1 MPC | RRL3L6A | 3 | 0 | $N$ | \% area | REFER | Land \#3 5-5.9 Lacquer area percent (\% area) |
| 8170 | 5a | 1 MPC | RRL3L6D | 6 | 2 | $N$ | DEMERITS | REFER | LAND \#3 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 8180 | 5a | 1 MPC | RRL4L6A | 3 | 0 | $N$ | \% Area | REFERE | LAND \#4 5-5.9 LaCQuer area percent (\% AREA) |
| 8190 | 5a | 1 MPC | RRL4L6D | 6 | 2 | $N$ | demerits | Refere | LAND \#4 5-5.9 LACQUER DEMERITS (DEMERITS) |
| 8200 | 5a | 1 MPC | RRG1L5A | 3 | 0 | $N$ | \% area | Refere | groove \#1 4-4.9 lacquer area percent (\% area) |
| 8210 | 5a | 1 MPC | RRG1L5D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#1 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 8220 | 5a | 1 MPC | RRG2L5A | 3 | 0 | $N$ | \% area | REFERE | GROOVE \#2 4-4.9 LaCQuer area percent (\% AREA) |
| 8230 | 5a | 1 MPC | RRG2L5D | 6 | 2 | $N$ | DEMERITS | Refere | GROOVE \#2 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 8240 | 5a | 1 MPC | RRG3L5A | 3 | 0 | $N$ | \% area | Refere | groove \#3 4-4.9 LacQuer area percent (\% area) |
| 8250 | 5a | 1 MPC | RRG3L5D | 6 | 2 | $N$ | DEmerits | REFERE | GROOVE \#3 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 8260 | 5a | 1 MPC | RRG4L5A | 3 | 0 | $N$ | \% area | REFERE | GROOVE \#4 4-4.9 LACQUER AREA PERCENT (\% AREA) |
| 8270 | 5a | 1 MPC | RRG4L5D | 6 | 2 | $N$ | DEMERITS | REFERE | GROOVE \#4 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 8280 | 5a | 1 MPC | RRL2L5A | 3 | 0 | $N$ | \% AREA | Refere | Land \#2 4-4.9 LacQuer area percent (\% area) |
| 8290 | 5a | 1MPC | RRL2L5D | 6 | 2 | $N$ | demerits | REFERE | LAND \#2 4-4.9 LACQuer demerits (Demerits) |
| 8300 | 5a | 1 MPC | RRL3L5A | 3 | 0 | N | \% area | REFERE | LaND \#3 4-4.9 LacQuer area percent (\% AREA) |
| 8310 | 5a | 1MPC | RRL3L5D | 6 | 2 | N | demerits | REFERE | LAND \#3 4-4.9 LacQuer demerits (demerits) |
| 8320 | 5a | 1 MPC | RRL4L5A | 3 | 0 | $N$ | \% area | Refere | Land \#4 4-4.9 lacouer area percent (\% AREA) |
| 8330 | 5a | 1 MPC | RRL4L5D | 6 | 2 | $N$ | demerits | REFERE | LAND \#4 4-4.9 LACQUER DEMERITS (DEMERITS) |
| 8340 | 5a | 1 MPC | RRG1L4A | 3 | 0 | $N$ | \% area | REFERE | GROOVE \#1 3-3.9 LACOUER AREA PERCENT (\% AREA) |
| 8350 | 5a | 1 MPC | RRG1L4D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#1 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 8360 | 5a | 1 MPC | RRG2L4A | 3 | 0 | $N$ | \% area | REFERE | GROOVE \#2 3-3.9 LaCQuer area percent (\% AREA) |
| 8370 | 5a | 1 MPC | RRG2L4D | 6 | 2 | $N$ | DEMERITS | REFERE | GROOVE \#2 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 8380 | 5a | 1 MPC | RRG3L4A | 3 | 0 | $N$ | \% AREA | REFERE | GROOVE \#3 3-3.9 LACQUER AREA PERCENT (\% AREA) |
| 8390 | 5a | 1 MPC | RRG3L4D | 6 | 2 | N | demerits | REFERE | GROOVE \#3 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 8400 | 5a | 1 MPC | RRG4L4A | 3 | 0 | $N$ | \% area | REFERE | Groove \#4 3-3.9 LaCQuer area percent (\% area) |
| 8410 | 5a | 1 MPC | RRG4L4D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#4 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 8420 | 5a | 1 MPC | RRL2L4A | 3 | 0 | $N$ | \% area | REFERE | LAND \#2 3-3.9 LacQuer area Percent (\% area) |
| 8430 | 5a | 1 MPC | RRL2L4D | 6 | 2 | N | DEmerits | REFERE | LAND \#2 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 8440 | 5 | 1 MPC | RRL3L4A | 3 | 0 | $N$ | \% area | REFERE | Land \#3 3-3.9 lacQuer area percent (\% AREA) |
| 8450 | 5a | 1 MPC | RRL3L4D | 6 | 2 | $N$ | DEMERITS | REFERE | LAND \#3 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 8460 | 5a | 1 MPC | RRL4L4A | 3 | 0 | $N$ | \% area | REFERE | Land \#4 3-3.9 LacQuer area percent (\% area) |
| 8470 | 5a | 1 MPC | RRL4L4D | 6 | 2 | N | Demerits | REFERE | LAND \#4 3-3.9 LACQUER DEMERITS (DEMERITS) |
| 8480 | 5a | 1 MPC | RRG1L3A | 3 | 0 | $N$ | \% area | REFERE | GROOVE \#1 2-2.9 LACQUER AREA PERCENT (\% AREA) |
| 8490 | 5 a | 1 MPC | RRG1L3D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#1 2-2.9 LaCQuer demerits (DEMERITS) |
| 8500 | 5a | 1 MPC | RRG2L3A | 3 | 0 | $N$ | \% AREA | REFERE | GROOVE \#2 2-2.9 LACQUER AREA PERCENT (\% AREA) |
| 8510 | 5a | 1 MPC | RRG2L3D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#2 2-2.9 LaCQuer demerits (DEMERITS) |
| 8520 | 5 | 1 MPC | RRG3L3A | 3 | 0 | $N$ | \% area | REFERE | GROOVE \#3 2-2.9 LaCQuer area Percent (\% AREA) |
| 8530 | 5a | 1MPC | RRG3L3D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#3 2-2.9 LACQUER DEMERITS (DEMERITS) |
| 8540 | 5a | 1 MPC | RRG4L3A | 3 | 0 | N | \% AREA | REFERE | Groove \#4 2-2.9 LacQuer area percent (\% area) |
| 8550 | 5a | 1 MPC | RRG4L3D | 6 | 2 | $N$ | demerits | REFERE | GROOVE \#4 2-2.9 LACQUER DEMERITS (DEMERITS) |
| 8560 | 5a | 1 MPC | RRL2L3A | 3 | 0 | $N$ | \% area | REFERE | land \#2 2-2.9 lacouer area percent (\% area) |
| 8570 | 5a | 1 MPC | RRL2L3D | 6 | 2 | $N$ | DEmerits | REFERE | LAND \#2 2-2.9 LacQuer demerits (DEmerits) |
| 8580 | 5a | 1 MPC | RRL3L3A | 3 | 0 | N | \% AREA | REFERE | Land \#3 2-2.9 LacQuer area percent (\% AREA) |
| 8590 | 5 a | 1 MPC | RRL3L3D | 6 | 2 | $N$ | demerits | REFERE | LaND \#3 2-2.9 LacQuer demerits (DEMERITS) |
| 8600 | 5a | 1 MPC | RRL4L3A | 3 | 0 | $N$ | \% AREA | REFERE | LaNd \#4 2-2.9 Lacouer area percent (\% AREA) |
| 8610 | 5 a | 1 MPC | RRL4L3D | 6 | 2 | N | DEMERITS | REFERE | LAND \#4 2-2.9 LaCQuer demerits (DEMERITS) |
| 8620 | 5a | 1 MPC | RRG1L2A | 3 | 0 | N | \% AREA | REFERE | GROOVE \#1 1-1.9 LaCQuer area percent (\% AREA) |
| 8630 | 5 | 1 MPC | RRG1L2D | 6 | 2 | N | DEMERITS | REFER | GROOVE \#1 1-1.9 LACQUER DEMERITS (DEMERITS) |

22-sep-1998
Test
Sequence Form Area

Field Name

Report: ASTM Data Dictionary
Field Decimal Data Length Size Type Units/Format

RRG2L2A RRG2L2D
RRG3L2A
RRG3L2D RRG4L2A RRG4L2D RRL2L2A
RRL2L2D
RRL3L2A RRL3L2A
RRL3L2D RRL4L2A $\begin{array}{lllll}\text { RRL4L2D } & 6 & 2 & N & \text { DEMERITS }\end{array}$ RRG1L1A $3 \quad 0 \quad N \quad$ \% AREA RRG1LID 6 N DEMERITS RRG2L1A 3 N 0 N AREA RRG2L1D 6 $\begin{array}{llll}\text { RRG3L1A } & 3 & 0 & N\end{array}$ \% AREA RRG3L1D $6 \quad 2 \quad N$ DEMERITS RRG4L1A $3 \quad 0 \quad N \quad$ \% AREA RRG4L1D 6 RRL2LIA $3 \quad 0 \quad N$ \% AREA $\begin{array}{llll}\text { RRL2LID } & 6 & 2 & N \\ \text { DEMERITS }\end{array}$ RRL3L1A 3 N 0 \% AREA RRL3L1D 6 N DEMERITS RRL4L1A 3 O 0 N AREA RRL4L1D 6 RRG1LCLA $3 \quad 0 \quad N \quad$ \% AREA $\begin{array}{llll}\text { RRG2LCLA } & 3 & 0 & N \\ \text { RRG3LCLA } & 3 & 0 & \text { N } \% \text { AREA }\end{array}$ RRG4LCLA $3 \quad 0 \quad N$ \% AREA RRL2LCLA 3 N 0 AREA $\begin{array}{llll}\text { RRL3LCLA } & 3 & 0 & N \\ \text { RRL4LCLA } & 3 & 0 & N\end{array}$ RG1ALTOT 3 O $\quad \mathbf{N}$ \% AREA RG1DLTOT $6 \quad 2 \quad N$ DEMERITS RG2ALTOT 3 N 0 N AREA RG2DLTOT 6 RG3ALTOT 3 N 0 N AREA RG3DLTOT $6 \quad 2 \quad N$ DEMERITS RG4ALTOT 3 N 0 N AREA RG4DLTOT 6 RLZALTOT 3 N $0 \quad N$ AREA $\begin{array}{lllll}\text { RLZDLTOT } & 6 & 2 & N & \text { DEMERITS }\end{array}$ RL3ALTOT 3 N 0 N AREA RL3DLTOT $6 \quad 2 \quad N$ DEMERITS RL4ALTOT 3 N 0 N AREA RL4DLTOT $6 \quad 2 \quad N$ DEMERITS $\begin{array}{llll}\text { RRGIUWD } & 6 & 2 & N \\ \text { DEMERITS }\end{array}$ RRG3UWD 6 RRG4UWD 6 RRL2UWD $6 \quad 2 \quad N$ DEMERITS $\begin{array}{lllll}\text { RRL3UWD } & 6 & 2 & N & \text { DEMERITS } \\ \text { RRL4UWD } & 6 & 2 & N & \text { DEMERITS }\end{array}$

## Description

REFEREE GROOVE \#2 1-1.9 LACQUER AREA PERCENT (\% AREA) REFEREE GROOVE \#2 1-1.9 LACQUER DEMERITS (DEMERITS) REFEREE GROOVE \#3 1-1.9 LACQUER AREA PERCENT (\% AREA) REFEREE GROOVE \#3 1-1.9 LACQUER DEMERITS (DEMERITS) REFEREE GROOVE \#4 1-1.9 LACQUER AREA PERCENT (\% AREA) REFEREE GROOVE \#4 1-1.9 LACQUER DEMERITS (DEMERITS) REFEREE LAND \#2 1-1.9 LACQUER AREA PERCENT (\% AREA) REFEREE LAND \#2 1-1.9 LACQUER DEMERITS (DEMERITS) REFEREE LAND \#3 1-1.9 LACQUER AREA PERCENT (\% AREA) REFEREELAND \#3 1-1.9 LACQUER DEMERITS (DEMERITS) REFEREE LAND \#4 1-1.9 LACQUER AREA PERCENT (\% AREA) REFEREE LAND \#4 1-1.9 LACQUER DEMERITS (DEMERITS) REFEREE GROOVE \#1 0-0.9 LACQUER AREA PERCENT (\% AREA) REFEREE GROOVE \#1 0-0.9 LACQUER DEMERITS (DEMERITS) REFEREE GROOVE \#2 0-0.9 LACQUER AREA PERCENT (\% AREA) REFEREE GROOVE \#2 0-0.9 LACQUER DEMERITS (DEMERITS) REFEREE GROOVE \#3 0-0.9 LACQUER AREA PERCENT (\% AREA) REFEREE GROOVE \#3 0-0.9 LACQUER DEMERITS (DEMERITS) REFEREE GROOVE \#4 0-0.9 LacQuer area percent (\% AREA) REFEREE GROOVE \#4 0-0.9 LACQUER DEMERITS (DEMERITS) REFEREE LAND \#2 0-0.9 LACQUER AREA PERCENT (\% AREA) REFEREE LAND \#2 0-0.9 LACQUER DEMERITS (DEMERITS) REfEREE LAND \#3 0-0.9 LACQUER AREA PERCENT (\% AREA) REFEREE LAND \#3 0-0.9 LACQUER DEMERITS (DEMERITS) REFEREE LAND \#4 0-0.9 LACQUER AREA PERCENT (\% AREA) REFEREE LAND \#4 0-0.9 LACQUER DEMERITS (DEMERITS) REFEREE GROOVE \#1 CLEAN LACQUER AREA PERCENT (\% AREA) referee groove \#2 CLEAN Lacquer area percent (\% area) REFEREE GROOVE \#3 CLEAN LACQUER AREA PERCENT (\% AREA) REFEREE GROOVE \# 4 CLEAN LACQUER AREA PERCENT (\% AREA) REFEREE LAND \#2 CLEAN LACQUER AREA PERCENT (\% AREA) REFEREE LAND \#3 CLEAN LACQUER AREA PERCENT (\% AREA) referee land \#4 clean lacquer area percent (\% area) REFEREE TOTAL GROOVE \#1 LACQUER AREA PERCENT (\% AREA) REFEREE TOTAL GROOVE \#1 LACQUER DEMERITS (DEMERITS) REFEREE TOTAL GROOVE \#2 LACQUER AREA PERCENT (\% AREA) REFEREE TOTAL GROOVE \#2 LACQUER DEMERITS (DEMERITS) REFEREE TOTAL GROOVE \#3 LACQUER AREA PERCENT (\% AREA) REFEREE TOTAL GROOVE \#3 LACQUER DEMERITS (DEMERITS) referee total groove \#4 lacQuer area percent (\% area) REFEREE TOTAL GROOVE * 4 LACQUER DEMERITS (DEMERITS) REFEREE TOTAL LAND \#2 LACQUER AREA PERCENT (\% AREA) REFEREE TOTAL LAND \#2 LACQUER DEMERITS (DEMERITS) referee total land \#3 lacQuer area percent (\% area) REFEREE TOTAL LAND \#3 LACQUER DEMERITS (DEMERITS) REFEREE TOTAL LAND \#4 LACQUER AREA PERCENT (\% AREA) REFEREE TOTAL LAND \# 4 LACQUER DEMERITS (DEMERITS) REfEREEE GROOVE 1 UNWEIGHTED DEMERITS (DEMERITS) REFEREE GROOVE 2 UNWEIGHTED DEMERITS (DEMERITS) REFEREE GROOVE 3 UNWEIGHTED DEMERITS (DEMERITS) REFEREE GROOVE 4 UNWEIGHTED DEMERITS (DEMERITS) REFEREE LAND 2 UNWEIGHTED DEMERITS (DEMERITS) REFEREE LAND 3 UNWEIGHTED DEMERITS (DEMERITS) REFEREE LAND 4 UNWEIGHTED DEMERITS (DEMERITS)

[^21]22-sep-1998

## Sequence Form Area

Field Field Decimal Data
Name
RRG1WD RRG2WD
RRG3WD
RRG4WD
RRL2WD
RRL4WD CF2G1WD CF2G2WD CF2L2WD CF2WTD DWNOCR DOWNHxxx
DDATHxxx DTIMHxxx DREAHxxx TOTLDOWN TOTCO OCOMHxxx
ringete
RINGGIE
ringgi2e
RINGGOE
$\begin{array}{lll}\text { RINGGI } 10 & 5 & 3\end{array}$
$\begin{array}{lll}\text { RINGGIZO } 5 & 5\end{array}$
RINGGOO 5
ISIDETPE 5
XSIDETPE 5
ISIDETPO 5
XSIDETPO 5
ISIDEIPE $5 \quad 3$

| XSIDEIPE | 5 | 3 |
| :--- | :--- | :--- |

ISIDE1PO 5
XSIDE1PO 5
ISIDE2PE 5

| XSIDE2PE | 5 | 3 |
| :--- | :--- | :--- |

ISIDE2PO 5
XSIDE2PO 5
ISIDEOPE 5
XSIDEOPE 5
ISIDEOPO $5 \quad 3$
XSIDEOPO 5
BBLONG1 7

| BBTRAN1 7 | 7 |
| :--- | :--- | :--- |


| BBOOR1 | 5 | 3 |
| :--- | :--- | :--- |

${ }_{\mathrm{N}}^{\mathrm{N}}$
N mm
mm
mmmmmmmm
mom
referee groove 1 weighted demerits (demerits) REFEREE GROOVE 2 WEIGHTED DEMERITS (DEMERITS) REFEREE GROOVE 3 HEIGHTED DEMERITS (DEMERITS) referee groove 4 WEighted demerits (demerits) referee land 2 weighted demerits (demerits) referee land 3 weighted demerits (demerits) REFEREE LAND 4 WEIGHTED DEMERITS (DEMERITS) Cf-2 rating groove 1 heighted demerits (demerits) cf-2 rating groove 2 heighted demerits (demerits) cf-2 rating land 2 weighted demerits (demerits) cf-2 rating total weighted demerits (demerits) NUMBER OF DOWNTIME OCCURENCES
DOUNTIME TEST HOURS (HH:MM)
DOUNTIME DATE (YYYYMMDD)
downtime time (hH:MM)
DOWNTIME REASON
DOWNTIME TIME TOTAL (HHH:MM)
TOTAL LINES OF COMMENTS \& OUTLIERS
OTHER DOWNTIME COMMENTS XXX
top ring gap pre-test (mm)
intermediate 1 RING gap pre-test (mm)
INTERMEDIATE 2 RING GAP PRE-TEST (mm)
OIL RING GAP PRE-TEST (mm)
TOP RING GAP POST-TEST (mm)
intermediate 1 ring gap post-test (mm)
intermediate 2 ring gap post-test (mm)
OIL RING GAP POST-TEST (mm)
minimum ring side clearance - top- pretest (mm)
maximum ring side clearance - top- pretest (m)
minimum ring side clearance posttest--0.114-0.185mm (mm)
maximum ring side clearance posttest--0.114-0.185mm (mm)
minimum ring side clearance - inti pretest- (mm)
maximum ring side clearance - inti pretest- (mm)
minimum ring side clearance- inti - posttest- (mm)
maximum ring side clearance- int1 - posttest- (mm)
minimum ring side clearance - intz - pretest (mm)
maximum ring side clearance - int2 - pretest (mm)
minimum ring side clearance - int2 - posttest (mm)
maximum ring side clearance - int2 - posttest (mm)
minimum ring side clearance - oil - pretest (mm)
maximum ring side clearance - oll - pretest (mm)
minimum ring side clearance - oil - posttest (mm)
maximum ring side clearance - oil - posttest (mm)
before test liner bore mea.--23 CM ht-Longitudinal (mm)
before test liner bore mea. --23 cm ht-transverse (mm)
before test liner bore mea. --23 cm ht -OUt of round (mm)
before test liner bore mea.--20.3 cm ht-Longitudinal (mm) before test liner bore mea.--20.3 cM ht-TRANSVERSE (mm) before test liner bore mea.--20.3 cM ht-out of round (mm) before test liner bore mea. --17.8 cm ht-longitudinal (mm) before test liner bore mea. --17.8 cm ht-transverse (mm) before test liner bore mea. --17.8 cm ht-out of round (mm) before test liner bore mea. --15.2 cM ht-LONGItudinal (mm) before test liner bore mea.--15.2 CM ht-transverse (mm)

| 22-sep-1998 |  | Test | Report: ASTM Data Dictionary |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Field | Field | Decimal | Data |  |
| Sequence | form |  | Area | Name | Length | Size | Type Units/Format | Description |
| 9720 | 9 | 1 MPC | BBOOR4 | 5 | 3 | N mm | before test liner bore mea. --15.2 cm ht-out of round (mm) |
| 9730 | 9 | 1 MPC | bblong | 7 | 3 | mm | before test liner bore mea. -12.7 cm ht-LONGItUdinal (mm) |
| 9740 | 9 | १MPC | bbtran5 | 7 | 3 | mm | before test liner bore mea.--12.7 CM ht-transverse (mm) |
| 9750 | 9 | 1MPC | BBCOR5 | 5 | 3 | mm | BEFORE TEST LINER BORE MEA.--12.7 CM HT-OUT OF ROUND (mm) |
| 9760 | 9 | 1 MPC | BBLONG6 | 7 | 3 | N mm | before test liner bore mea. $-10.2 \mathrm{cM} \mathrm{ht-LONGITUDinal} \mathrm{(mm)}$ |
| 9770 | 9 | 1MPC | 8Btrang | 7 | 3 | N mm | before test liner bore mea.--10.2 cm ht-transverse (mm) |
| 9780 | 9 | 1MPC | BBOOR6 | 5 | 3 | mm | BEFORE TEST LINER BORE MEA. $-10.2 \mathrm{cM} \mathrm{HT-OUT} \mathrm{OF} \mathrm{ROUND} \mathrm{(mm)}$ |
| 9790 | 9 | 1MPC | BBLONG7 | 7 | 3 | mm | BEFORE TEST LINER BORE MEA.--7.6 CM HT-LONGITUDINAL (mm) |
| 9800 | 9 | 1 MPC | bBtran7 | 7 | 3 | mm | BEFORE TEST LINER BORE MEA. -7.6 CM HT-TRANSVERSE (mm) |
| 9810 | 9 | 1MPC | BBCOR7 | 5 | 3 | N mm | BEFORE TEST LINER BORE MEA. --7.6 CM HT-OUT OF ROUND (mm) |
| 9820 | 9 | 1 MPC | BBLONG8 | 7 | 3 | N mm | before test liner bore mea. - 5.1 cm ht-longitudinal (mm) |
| 9830 | 9 | 1MPC | bBtran8 | 7 | 3 | mm | before test liner bore mea. -5.1 CM HT-transverse (mm) |
| 9840 | 9 | 1 MPC | bBoor8 | 5 | 3 | mm | BEFORE TEST LINER BORE MEA. -5.1 CM HT-OUT OF ROUND (mm) |
| 9850 | 9 | 1MPC | BBLONG9 | 7 | 3 | N mm | Before test liner bore mea. --2.5 CM HT-LONGITUDINAL (mm) |
| 9860 | 9 | 1MPC | bbtrang | 7 | 3 | $N \mathrm{~mm}$ | before test liner bore mea.--2.5 CM ht-transverse (mm) |
| 9870 | 9 | 1 MPC | BBOOR9 | 5 | 3 | mm | BEFORE TEST LINER BORE MEA. -2.5 CM HT-OUT OF ROUND (mm) |
| 9880 | 9 | 1MPC | Btaplong | 7 | 3 | mm | before test liner bore taper mea.--LONGItUdinal (mm) |
| 9890 | 9 | 1MPC | btaptran | 7 | 3 | N mm | before test liner bore taper mea.--transverse (mm) |
| 9900 | 9 | 1 MPC | MAXOOR | 5 | 3 | N mm | before test liner bore max out of round (mm) |
| 9910 | 9 | 1MPC | BBLFIN | 4 | 2 | micrometre | before test liner bore surface finish (micrometre) |
| 9920 | 9 | 1mPC | AWEARLF | 5 | 3 | N mm | AFter test liner bore wear step--LONGItUdinal front (mm) |
| 9930 | 9 | 1 MPC | awearlr | 5 | 3 | mm | after test liner bore wear step--Longitudinal rear (mm) |
| 9940 | 9 | 1 MPC | AWEARTT | 5 | 3 | mm | after test liner bore wear step--transverse T (mm) |
| 9950 | 9 | 1 MPC | ameartat | 5 | 3 | mm | after test liner bore wear step--transverse at (mm) |
| 9960 | 10 | 1MPC | RPMSENS | 17 | 0 | C | engine speed sensing device |
| 9970 | 10 | 1 MPC | RPMCALF | 13 | 0 | C | engine speed calibration frequency |
| 9980 | 10 | 1 MPC | RPMRECD | 16 | 0 | C | engine speed record device |
| 9990 | 10 | 1 MPC | RPMOBSF | 12 | 0 | C | ENGINE SPEED OBSERVATION FREQUENCY |
| 10000 | 10 | 1 MPC | RPMRECF | 12 | 0 | C | ENGINE SPEED RECORD FREQUENCY |
| 10010 | 10 | 1 MPC | RPMLOGF | 12 | 0 | c | Engine speed log frequency |
| 10020 | 10 | 1 MPC | RPMSYSR | 8 | 0 | C | engine speed srstem response |
| 10030 | 10 | 1 MPC | PWRSENS | 17 | 0 | c | engine power sensing device |
| 10040 | 10 | 1 MPC | PURCALF | 13 | 0 | c | engine power calibration frequency |
| 10050 | 10 | 1 MPC | PWRRECD | 16 | 0 | c | ENGINE POWER RECORD DEVICE |
| 10060 | 10 | 1MPC | PUROBSF | 12 | 0 | C | ENGINE POWER OBSERVATION FREQUENCY |
| 10070 | 10 | 1 MPC | PWRRECF | 12 | 0 | c | ENGINE POWER RECORD frequency |
| 10080 | 10 | 1 MPC | PWRLOGF | 12 | 0 | c | ENGINE POWER LOG frequency |
| 10090 | 10 | 1 MPC | PWRSYSR | 8 | 0 | c | ENGINE POWER SYSTEM Response |
| 10100 | 10 | 1 MPC | fflosens | 17 | 0 | c | fuel rate sensing device |
| 10110 | 10 | 1 MPC | FFLOCALF | 13 | 0 | C | fuel rate calibration frequency |
| 10120 | 10 | 1 MPC | FFLORECD | 16 | 0 | C | FUEL RATE RECORD DEVICE |
| 10130 | 10 | 1 MPC | FFLOOBSF | 12 | 0 | c | FUEL RATE OBSERVATION FREQUENCY |
| 10140 | 10 | 1 MPC | fflorecf | 12 | 0 | c | fuel rate record frequency |
| 10150 | 10 | 1 MPC | fflologf | 12 | 0 | c | fuel rate engine speed log frequency |
| 10160 | 10 | 1 MPC | FFLOSYSR | 8 | 0 | C | FUEL RATE SYSTEM RESPONSE |
| 10170 | 10 | 1 MPC | HUMSENS | 17 | 0 | c | humidity sensing device |
| 10180 | 10 | 1 MPC | HUMCALF | 13 | 0 | c | humidity calibration frequency |
| 10190 | 10 | 1 MPC | HumRecd | 16 | 0 | c | humidity record device |
| 10200 | 10 | 1 MPC | HUMOBSF | 12 | 0 | c | humidity observation frequency |
| 10210 | 10 | 1 MPC | humrecf | 12 | 0 | c | HUMIDITY RECORD FREQUENCY |
| 10220 | 10 | 1 MPC | HUMLOGF | 12 | 0 | c | humidity log frequency |
| 10230 | 10 | 1 PPC | HUMSYSR | 8 | 0 | C | humidity system response |
| 10240 | 10 | 1MPC | COTSENS | 17 | 0 | c | COOLANT OUT TEMPERATURE SENSING DEVICE |
| 10250 | 10 | 1MPC | cotcalf | 13 | 0 | c | coolant out temperature calibration frequency |
|  |  |  |  |  |  | IG. A3.1 Data Dicti | ary (continued) |


| 22-sep-1998 |  | Test | Report: ASTM Data Dictionary |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Field | Field | Decimal | Data |  |
| Sequence | Form |  | Area | Name | Length | Size | Type Units/Format | Description |
| 10260 | 10 | 1MPC | COTRECD | 16 | 0 | c | Coolant out temperature engine speed record device |
| 10270 | 10 | 1MPC | cotobsf | 12 | 0 | c | coolant out temperature observation frequency |
| 10280 | 10 | 1MPC | COTRECF | 12 | 0 | c | COOLANT OUT TEMPERATURE RECORD FREQUENCY |
| 10290 | 10 | 1MPC | Cotloge | 12 | 0 | C | coolant out temperature log frequency |
| 10300 | 10 | 1 MPC | COTSYSR | 8 | 0 | c | COOLANT OUT TEMPERATURE SYSTEM RESPONSE |
| 10310 | 10 | 1MPC | CONSENS | 17 | 0 | c | coolant in temperature sensing device |
| 10320 | 10 | 1 MPC | CONCALF | 13 | 0 | c | COOLANT IN TEMPERATURE CALIBRATION FREQUENCY |
| 10330 | 10 | 1MPC | CONRECD | 16 | 0 | c | COOLANT IN TEMPERATURE RECORD DEVICE |
| 10340 | 10 | 1MPC | CONOBSF | 12 | 0 | c | COOLANT IN TEMPERATURE OBSERVATION FREQUENCY |
| 10350 | 10 | 1 MPC | CONRECF | 12 | 0 | C | coolant in temperature record frequency |
| 10360 | 10 | 1 MPC | CONLOGF | 12 | 0 | c | coolant in temperature log frequency |
| 10370 | 10 | 1 MPC | CONSYSR | 8 | 0 | C | COOLANT in temperature system response |
| 10380 | 10 | 1 MPC | OBRGSENS | 17 | 0 | C | Oil to bearing temperature sensing device |
| 10390 | 10 | 1MPC | Obrgcalf | 13 | 0 | c | oil to bearing temperature calibration frequency |
| 10400 | 10 | 1MPC | OBRGRECD | 16 | 0 | c | Oil to bearing temperature record device |
| 10410 | 10 | 1 MPC | OBRGObSF | 12 | 0 | C | Oil to bearing temperatureobservation frequency |
| 10420 | 10 | 1 MPC | OBRGRECF | 12 | 0 | c | OIL to bearing temperature record frequency |
| 10430 | 10 | 1MPC | obrglogf | 12 | 0 | C | Oil to bearing temperature log frequency |
| 10440 | 10 | 1 MPC | OBRGSYSR | 8 | 0 | c | Oil to bearing temperature system response |
| 10450 | 10 | 1 MPC | OCOLSENS | 17 | 0 | C | Oil cooler in temperature sensing device |
| 10460 | 10 | 1MPC | OCOLCALF | 13 | 0 | c | OIL COOLER IN temperature calibration frequency |
| 10470 | 10 | 1 MPC | ocolrecd | 16 | 0 | c | Oil cooler in temperature record device |
| 10480 | 10 | 1MPC | OCOLOBSF | 12 | 0 | c | Oil cooler in temperature observation frequency |
| 10490 | 10 | 1 MPC | OCOLRECF | 12 | 0 | c | Oil cooler in temperature record frequency |
| 10500 | 10 | 1MPC | OCOLLOGF | 12 | 0 | c | OIL COOLER IN TEMPERTURE LOG FREQUENCY |
| 10510 | 10 | 1MPC | OCOLSYSR | 8 | 0 | c | oil cooler in temperature system response |
| 10520 | 10 | 1MPC | AIRTSENS | 17 | 0 | c | inlet air temperature sensing device |
| 10530 | 10 | 1MPC | AIrtcalf | 13 | 0 | c | inlet air temperature calibration frequency |
| 10540 | 10 | 1MPC | airtrecd | 16 | 0 | c | INLET AIR TEMPERATURE RECORD DEVICE |
| 10550 | 10 | 1MPC | airtobsf | 12 | 0 | c | inlet air temperature observation frequency |
| 10560 | 10 | 1MPC | AIRTRECF | 12 | 0 | c | inlet air temperature engine speed record frequency |
| 10570 | 10 | 1MPC | AIRTLOGF | 12 | 0 | c | inlet air temperature log frequency |
| 10580 | 10 | 1 MPC | Alrtsysr | 8 | 0 | c | inLet air temperature system response |
| 10590 | 10 | 1MPC | extsens | 17 | 0 | c | exhaust temperature sensing device |
| 10600 | 10 | 1MPC | EXTCALF | 13 | 0 | C | exhaust temperature calibration frequency |
| 10610 | 10 | 1 MPC | EXTRECD | 16 | 0 | c | EXHAUST TEMPERATURE RECORD DEVICE |
| 10620 | 10 | 1 MPC | Extobsf | 12 | 0 | c | EXHAUST TEMPERATURE OBSERVATION FREQUENCY |
| 10630 | 10 | 1 MPC | EXTRECF | 12 | 0 | c | EXHAUST TEMPERATURE RECORD frequency |
| 10640 | 10 | 1MPC | EXTLOGF | 12 | 0 | c | EXHAUST TEMPERATURE LOG FREQuency |
| 10650 | 10 | 1 MPC | EXTSYSR | 8 | 0 | c | EXhaust temperature system response |
| 10660 | 10 | 1MPC | OBRPSENS | 17 | 0 | c | Oil to bearing pressure sensing device |
| 10670 | 10 | 1 MPC | OBRPCALF | 13 | 0 | C | oil to bearing pressure calibration frequency |
| 10680 | 10 | 1 MPC | OBRPRECD | 16 | 0 | c | Oil to bearing pressure record device |
| 10690 | 10 | 1 MPC | OBRPOBSF | 12 | 0 | C | Oil to bearing pressure observation frequency |
| 10700 | 10 | 1 MPC | OBRPRECF | 12 | 0 | c | OIL to bearing pressure record frequency |
| 10710 | 10 | 1 MPC | OBRPLOGF | 12 | 0 | c | Oil to bearing pressure log frequency |
| 10720 | 10 | 1 MPC | OBRPSYSR | 8 | 0 | c | oil to bearing pressure system response |
| 10730 | 10 | 1 MPC | OJETSENS | 17 | 0 | c | ofl to jet pressure sensing device |
| 10740 | 10 | 1 MPC | OJETCALF | 13 | 0 | C | OIL TO JET PRESSURE CALIbration frequency |
| 10750 | 10 | 1 MPC | OJETRECD | 16 | 0 | c | OIL TO JET PRESSURE RECORD DEVICE |
| 10760 | 10 | 1 MPC | OJETOBSF | 12 | 0 | c | Oil to jet pressure observation frequency |
| 10770 | 10 | 1 MPC | OJETRECF | 12 | 0 | c | OIL TO JET PRESSURE RECORD FREQUENCY |
| 10780 | 10 | 1 MPC | OJETLOGF | 12 | 0 | C | Oil to jet pressure engine speed log frequency |
| 10790 | 10 | 1MPC | OJETSYSR | 8 | 0 | c | OIL TO JEt Pressure system response |
|  |  |  |  |  | FIG. | A3.1 Data Dictionar | (continued) |


| 22-sep-1998 |  | Report: ASTM Data Dictionary |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Test | Field | Field | Decimal |  |  |
| Sequence | Form | Area | Name | Length | Size | Type Units/Format | Description |
| 10800 | 10 | 1 MPC | AIRPSENS | 17 | 0 | c | inlet air pressure sensing device |
| 10810 | 10 | 1 MPC | AIRPCALF | 13 | 0 | c | inlet air pressure calibration frequency |
| 10820 | 10 | 1MPC | AIRPRECD | 16 | 0 | c | InLET AIR PRESSURE RECORD DEVICE |
| 10830 | 10 | 1MPC | AIRPOBSF | 12 | 0 | c | INLET AIR PRESSURE OBSERVATION FREQUENCY |
| 10840 | 10 | 1MPC | AIRPRECF | 12 | 0 | c | inlet air pressure record frequency |
| 10850 | 10 | 1MPC | AIRPLOGF | 12 | 0 | C | inlet air pressure log frequency |
| 10860 | 10 | 1MPC | AIRPSYSR | 8 | 0 | C | InLET AIR PRESSURE SYSTEM RESPONSE |
| 10870 | 10 | 1MPC | EXPSENS | 17 | 0 | c | EXHAUST PRESSURE SENSING DEvice |
| 10880 | 10 | 1 MPC | EXPCALF | 13 | 0 | c | exhaust pressure calibration frequency |
| 10890 | 10 | 1 MPC | EXPRECD | 16 | 0 | c | EXhaust pressure record device |
| 10900 | 10 | 1 MPC | EXPOBSF | 12 | 0 | c | EXHAUST PRESSURE OBSERVATION FREQUENCY |
| 10910 | 10 | 1MPC | EXPRECF | 12 | 0 | c | EXHAUST PRESSURE RECORD FREQUENCY |
| 10920 | 10 | 1 MPC | EXPLOGF | 12 | 0 | c | EXHAUST PRESSURE LOG FREQUENCY |
| 10930 | 10 | 1 MPC | EXPSYSR | 8 | 0 | c | EXhaust pressure system response |
| 10940 | 10 | 1MPC | FFilsens | 17 | 0 | C | fuel filter housing pressure sensing device |
| 10950 | 10 | 1MPC | FFILCALF | 13 | 0 | c | fuel filter housing pressure calibration frequency |
| 10960 | 10 | 1 MPC | FFILRECD | 16 | 0 | c | fuel filter housing pressure record device |
| 10970 | 10 | 1 MPC | ffilobsf | 12 | 0 | c | fuel filter housing pressure observation frequency |
| 10980 | 10 | 1 MPC | ffildecf | 12 | 0 | c | fuel filter housing pressure record frequency |
| 10990 | 10 | 1MPC | FFILLOGF | 12 | 0 | c | FUEL filter housing pressure log frequency |
| 11000 | 10 | 1MPC | FFILSYSR | 8 | 0 | C | fuel filter housing pressure system response |
| 11010 | 10 | 1MPC | ccvsens | 17 | 0 | c | Crankcase vacuum sensing device |
| 11020 | 10 | 1MPC | ccvealf | 13 | 0 | c | CRANKCASE Vacuum engine sped calibration frequency |
| 11030 | 10 | 1MPC | CCVRECD | 16 | 0 | c | CRankcase vacuum record device |
| 11040 | 10 | 1MPC | ccvorsf | 12 | 0 | c | CRANKCASE VACUUM OBSERVATION FREQUENCY |
| 11050 | 10 | 1MPC | ccvrecf | 12 | 0 | c | Crankcase vacuum record frequency |
| 11060 | 10 | 1 MPC | CCVLOGF | 12 | 0 | c | CRANKCASE VACUUM LOG FREQUENCY |
| 11070 | 10 | 1MPC | CCVSYSR | 8 | 0 | c | CRANKCASE VAClum system response |
| 11080 | 10 | 1 MPC | BLBYSENS | 17 | 0 | c | blowby sensing device |
| 11090 | 10 | 1MPC | BLBYCALF | 13 | 0 | c | blowby engine speed calibration frequency |
| 11100 | 10 | 1MPC | BLBYRECD | 16 | 0 | c | BLOWBY RECORD DEVICE |
| 11110 | 10 | 1 MPC | BLbYobsf | 12 | 0 | c | Blowby observation frequency |
| 11120 | 10 | 1 MPC | BLBYRECF | 12 | 0 | c | BLOWBY RECORD FREQUENCY |
| 11130 | 10 | 1 MPC | blbylogf | 12 | 0 | c | blowby log frequency |
| 11140 | 10 | 1MPC | BLBYSYSR | 8 | 0 | c | BLOWBY SYSTEM RESPONSE |
| 11150 | 10 | 1 MPC | CFLWSENS | 17 | 0 | c | coolant flow sensing device |
| 11160 | 10 | 1 MPC | CFLWCALF | 13 | 0 | c | COOLANT FLOW CALIbration frequency |
| 11170 | 10 | 1 MPC | CFLURECD | 16 | 0 | c | COOLANT FLOW RECORD DEVICE |
| 11180 | 10 | 1MPC | CFLWOBSF | 12 | 0 | c | COOLANT FLOH OBSERVATION FREQUENCY |
| 11190 | 10 | 1MPC | CFLWRECF | 12 | 0 | c | COOLANT FLOW ENGINE SPEED RECORD frequency |
| 11200 | 10 | 1MPC | CFLWLOGF | 12 | 0 | c | COOLANT FLOW LOG FREQUENCY |
| 11210 | 10 | 1 MPC | CFLWSYSR | 8 | 0 | C | coolant flow system response |
| 11220 | 11 | 1 MPC | INAIRIM | 70 | 0 | c | inlet air temperature plot image |
| 11230 | 11 | 1 MPC | OBEARIM | 70 | 0 | c | OIL To bearing temperature plot image |
| 11240 | 11 | 1MPC | COLINIM | 70 | 0 | c | coolant in temperature plot image |
| 11250 | 11 | 1MPC | COLOUTIM | 70 | 0 | c | coolant out temperature plot image |
| 11260 | 11 | 1MPC | EXHTMPIM | 70 | 0 | c | exhaust temperature plot image |
| 11270 | 11 | 1 MPC | frateim | 70 | 0 | c | FUEL RATE PLOT image |
| 11280 | 11 | 1 MPC | RPMIM | 70 | 0 | c | engine speed plot image |
| 11290 | 11 | 1MPC | POWERIM | 70 | 0 | c | POWER PLOT IMAGE |
| 11300 | 12 | 1MPC | OBEARPIM | 70 | 0 | c | Oil to bearing pressure plot image |
| 11310 | 12 | 1 MPC | OJETPIM | 70 | 0 | c | OIL to jet pressure plot image |
| 11320 | 12 | 1 MPC | INAIRPIM | 70 | 0 | c | inlet alr pressure plot image |
| 11330 | 12 | 1 MPC | EXHPIM | 70 | 0 | c | EXhaust pressure plot image |
|  |  |  |  |  |  | A3.1 Data Dictionary | (continued) |


|  |  | ASIM D 6618 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22-sep-1998 |  | Test | Field | Field | Decimal Data |  | Report: ASTM Data Dictionary |  |
|  |  |  |  |  |  |  |  |
| Sequence | Form |  | Area | Name | Length | Size |  | Units/Format | Description |
| 11340 | 12 | 1 MPC | humidim | 70 | 0 | c |  | humidity plot image |
| 11350 | 12 | 1 MPC | COLFLOIM | 70 | 0 | c |  | COOLANT FLOW PLOT IMAGE |
| 11360 | 12 | 1 MPC | ccvacim | 70 | 0 | c |  | CRANKCASE VACUUM PLOT IMAGE |
| 11370 | 12 | 1 MPC | blobyim | 70 | 0 | c |  | blowby plot image |
| 11380 | 13 | 1 MPC | OCPIM | 70 | 0 | c |  | OIL CONSUMPTION PLOT IMAGE |
| 11390 | 14 | 1 MPC | PRLIM | 70 | 0 | $c$ |  | PISTON AND RING PHOTOGRAPHS ImAGE |
| 11400 | 15 | 1 MPC | DTSTRxxx | 8 | 0 | c | YYYYMMDD | START USAGE DATES (YYYYMMDD) |
| 11410 | 15 | 1 MPC | DTTMRxxx | 6 | 0 | c | ннн:MM | time usage dates (hhH:MM) |
| 11420 | 15 | 1 MPC | wDZIRxxx | 7 | 3 | $N$ |  | WEIGHTED TOTAL DEMERITS LAB 21 |
| 11430 | 15 | 1 MPC | WDSARxxx | 6 | 1 | $N$ | DEMERITS | heighted total demerits severity adjustment (demerits) |
| 11440 | 15 | 1 MPC | tgzirxxx | 7 | 3 | $N$ |  | top groove filling lab 21 |
| 11450 | 15 | 1 MPC | tgsarxxx | 3 | 0 | $N$ | \% | top groove filling severity adjustment (\%) |
| 11460 | 16 | 1 MPC | fuelim | 70 | 0 | c |  | fuel batch analysis image |
| 11470 | 17 | 1 MPC | cCHIM | 70 | 0 | C |  | tmc control chart analysis image |
| FIG. A3.1 Data Dictionary (continued) |  |  |  |  |  |  |  |  |



```
DTIMHxxx DOWNHxxx DOWNHxxx DOWNTIME TIME (HH:MM)
DREAHxxx DOWNHxxx DOWNHxxx DOWNTIME REASON
OCOMHxxx OCOMHxxx OCOMHxxx OTHER DOWNTIME COMMENTS XXX
DTSTRxxx DTSTRxxx DTSTRxxx START USAGE DATES (YYYYMMDD)
DTTMRxxx DTSTRxxx DTSTRxxx TIME USAGE DATES (HHH:MM)
WDZIRxxx DTSTRxxx DTSTRxxx WEIGHTED TOTAL DEMERITS LAB ZI
WDSARxxx DTSTRxxx DTSTRxxx WEIGHTED TOTAL DEMERITS SEVERITY ADJUSTMENT (DEMERITS)
TGZIRxxx DTSTRxxx DTSTRxxx TOP GROOVE FILLING LAB ZI
TGSARxxx DTSTRxxx DTSTRxxx TOP GROOVE FILLING SEVERITY ADJUSTMENT (%)
    FIG. A3.2 Repeating Field Specifications (continued)
```

    A4. TEST FUEL INFORMATION
    A4.1 Test Fuel Specifications and an Example of Required Fuel Batch Analysis Data are shown in Fig. A4.1.



Approved by: $\qquad$ Analys $\qquad$
FIG. A4.1 Test Fuel Batch Analysis

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## APPENDIXES

(Nonmandatory Information)

## X1. CORRECTION FACTOR TABLES

X1.1 See Tables X1.1-X1.8 for humidity correction factors.
X1.2 The following calculations are an example of a perfect gas law equation for corrected humidity:

$$
\begin{gather*}
\text { or Humidity }=7000\left[\frac{18.0152}{28.96247}\right] \frac{P_{v}}{\left(P_{T}-P_{v}\right)}  \tag{X1.1}\\
\text { or Humidity }=4354.13 \frac{P_{v}}{\left(P_{T}-P_{v}\right)} \tag{X1.2}
\end{gather*}
$$

TABLE X1.1 Humidity, Grains/Pound Correction Factors for Non-standard Barometric Conditions (30.0-30.9 in. Hg)

|  | Barometric Pressure (in. Hg) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 30.9 | 30.8 | 30.7 | 30.6 | 30.5 | 30.4 | 30.3 | 30.2 | 30.1 | 30.0 |
| 65 | -3.1 | -2.8 | -2.5 | -2.2 | -1.9 | -1.6 | -1.2 | -0.9 | -0.6 | -0.3 |
| 66 | -3.2 | -2.9 | -2.6 | -2.2 | -1.9 | -1.6 | -1.3 | -1.0 | -0.6 | -0.3 |
| 67 | -3.3 | -3.0 | -2.6 | -2.3 | -2.0 | -1.7 | -1.3 | -1.0 | -0.7 | -0.3 |
| 68 | -3.4 | -3.1 | -2.7 | -2.4 | -2.0 | -1.7 | -1.4 | -1.0 | -0.7 | -0.3 |
| 69 | -3.5 | -3.2 | -2.8 | -2.5 | -2.1 | -1.8 | -1.4 | -1.1 | -0.7 | -0.4 |
| 70 | -3.7 | -3.3 | -3.0 | -2.6 | -2.2 | -1.9 | -1.5 | -1.1 | -0.7 | -0.4 |
| 71 | -3.8 | -3.4 | -3.0 | -2.7 | -2.3 | -1.9 | -1.5 | -1.1 | -0.8 | -0.4 |
| 72 | -3.9 | -3.5 | -3.1 | -2.7 | -2.3 | -2.0 | -1.6 | -1.2 | -0.8 | -0.4 |
| 73 | -4.1 | -3.7 | -3.3 | -2.9 | -2.5 | -2.1 | -1.6 | -1.2 | -0.8 | -0.4 |
| 74 | -4.2 | -3.8 | -3.4 | -2.9 | -2.5 | -2.1 | -1.7 | -1.3 | -0.8 | -0.4 |
| 75 | -4.4 | -4.0 | -3.5 | -3.1 | -2.6 | -2.2 | -1.8 | -1.3 | -0.9 | -0.4 |
| 76 | -4.5 | -4.1 | -3.6 | -3.2 | -2.7 | -2.3 | -1.8 | -1.4 | -0.9 | -0.5 |
| 77 | -4.7 | -4.2 | -3.8 | -3.3 | -2.8 | -2.4 | -1.9 | -1.4 | -0.9 | -0.5 |
| 78 | -4.9 | -4.4 | -3.9 | -3.4 | -2.9 | -2.5 | -2.0 | -1.5 | -1.0 | -0.5 |
| 79 | -5.0 | -4.5 | -4.0 | -3.5 | -3.0 | -2.5 | -2.0 | -1.5 | -1.0 | -0.5 |
| 80 | -5.2 | -4.7 | -4.2 | -3.6 | -3.1 | -2.6 | -2.1 | -1.6 | -1.0 | -0.5 |

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TABLE X1.2 Humidity, Grains/Pound Correction Factors for Non-standard Barometric Conditions (29.0-29.9 in. Hg)

| Dew Barometric Pressure (in. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Temp ${ }^{\circ} \mathrm{F}$ | 29.9 | 29.8 | 29.7 | 29.6 | 29.5 | 29.4 | 29.3 | 29.2 | 29.1 | 29.0 |
| 65 | 0.0 | 0.3 | 0.7 | 1.0 | 1.3 | 1.7 | 2.0 | 2.3 | 2.6 | 3.0 |
| 66 | 0.0 | 0.3 | 0.7 | 1.0 | 1.4 | 1.7 | 2.0 | 2.4 | 2.7 | 3.1 |
| 67 | 0.0 | 0.4 | 0.7 | 1.1 | .1.4 | 1.8 | 2.1 | 2.5 | 2.8 | 3.2 |
| 68 | 0.0 | 0.4 | 0.7 | 1.1 | 1.5 | 1.9 | 2.2 | 2.6 | 3.0 | 3.3 |
| 69 | 0.0 | 0.4 | 0.8 | 1.1 | 1.5 | 1.9 | 2.3 | 2.7 | 3.0 | 3.4 |
| 70 | 0.0 | 0.4 | 0.8 | 1.2 | 1.6 | 2.0 | 2.3 | 2.7 | 3.1 | 3.5 |
| 71 | 0.0 | 0.4 | 0.8 | 1.2 | 1.6 | 2.1 | 2.5 | 2.9 | 3.3 | 3.7 |
| 72 | 0.0 | 0.4 | 0.8 | 1.3 | 1.7 | 2.1 | 2.5 | 2.9 | 3.4 | 3.8 |
| 73 | 0.0 | 0.4 | 0.9 | 1.3 | 1.8 | 2.2 | 2.6 | 3.1 | 3.5 | 4.0 |
| 74 | 0.0 | 0.5 | 0.9 | 1.4 | 1.8 | 2.3 | 2.8 | 3.2 | 3.7 | 4.1 |
| 75 | 0.0 | 0.5 | 0.9 | 1.4 | 1.9 | 2.4 | 2.8 | 3.3 | 3.8 | 4.2 |
| 76 | 0.0 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 2.9 | 3.4 | 3.9 | 4.4 |
| 77 | 0.0 | 0.5 | 1.0 | 1.5 | 2.0 | 2.6 | 3.1 | 3.6 | 4.1 | 4.6 |
| 78 | 0.0 | 0.5 | 1.0 | 1.6 | 2.1 | 2.6 | 3.1 | 3.6 | 4.2 | 4.7 |
| 79 | 0.0 | 0.5 | 1.1 | 1.6 | 2.2 | 2.7 | 3.2 | 3.8 | 4.3 | 4.9 |
| 80 | 0.0 | 0.6 | 1.1 | 1.7 | 2.2 | 2.8 | 3.4 | 3.0 | 4.5 | 5.0 |

TABLE X1.3 Humidity, Grains/Pound Correction Factors for Non-standard Barometric Conditions (28.0-28.9 in. Hg)

| Dew Barometric Pressure (in. H |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Temp ${ }^{\circ} \mathrm{F}$ | 28.9 | 28.8 | 28.7 | 28.6 | 28.5 | 28.4 | 28.3 | 28.2 | 28.1 | 28.0 |
| 65 | 3.3 | 3.7 | 4.0 | 4.4 | 4.7 | 5.1 | 5.4 | 5.8 | 6.1 | 6.5 |
| 66 | 3.4 | 3.8 | 4.1 | 4.5 | 4.9 | 5.3 | 5.6 | 6.0 | 6.4 | 6.7 |
| 67 | 3.5 | 3.9 | 4.3 | 4.6 | 5.0 | 5.4 | 5.8 | 6.2 | 6.5 | 6.9 |
| 68 | 3.7 | 4.1 | 4.5 | 4.9 | 5.3 | 5.7 | 6.0 | 6.4 | 6.8 | 7.2 |
| 69 | 3.8 | 4.2 | 4.6 | 5.0 | 5.4 | 5.9 | 6.3 | 6.7 | 7.1 | 7.5 |
| 70 | 3.9 | 4.3 | 4.7 | 5.2 | 5.6 | 6.0 | 6.4 | 6.8 | 7.3 | 7.7 |
| 71 | 4.1 | 4.5 | 5.0 | 5.4 | 5.8 | 6.3 | 6.7 | 7.1 | 7.5 | 8.0 |
| 72 | 4.2 | 4.7 | 5.1 | 5.6 | 6.0 | 6.5 | 6.9 | 7.4 | 7.8 | 8.3 |
| 73 | 4.4 | 4.9 | 5.3 | 5.8 | 6.2 | 6.7 | 7.2 | 7.6 | 8.1 | 8.5 |
| 74 | 4.6 | 5.1 | 5.6 | 6.0 | 6.5 | 7.0 | 7.5 | 8.0 | 8.4 | 8.9 |
| 75 | 4.7 | 5.2 | 5.7 | 6.2 | 6.7 | 7.2 | 7.7 | 8.2 | 8.7 | 9.2 |
| 76 | 4.9 | 5.4 | 5.9 | 6.4 | 6.9 | 7.5 | 8.0 | 8.5 | 9.0 | 9.5 |
| 77 | 5.1 | 5.6 | 6.2 | 6.7 | 7.2 | 7.8 | 8.3 | 8.8 | 9.3 | 9.9 |
| 78 | 5.2 | 5.8 | 6.3 | 6.9 | 7.4 | 8.0 | 8.6 | 9.1 | 9.7 | 10.2 |
| 79 | 5.4 | 6.0 | 6.6 | 7.1 | 7.7 | 8.3 | 8.9 | 9.5 | 10.0 | 10.6 |
| 80 | 5.6 | 6.2 | 6.8 | 7.4 | 8.0 | 8.6 | 9.2 | 9.8 | 10.4 | 11.0 |

TABLE X1.4 Humidity, Grains/Pound Correction Factors for Non-standard Barometric Conditions (27.0-27.9 in. Hg)

|  | Barometric Pressure (in. Hg ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 27.9 | 27.8 | 27.7 | 27.6 | 27.5 | 27.4 | 27.3 | 27.2 | 27.1 | 27.0 |
| 65 | 6.8 | 7.2 | 7.5 | 7.9 | 8.2 | 8.6 | 8.9 | 9.3 | 9.6 | 10.0 |
| 66 | 7.1 | 7.5 | 7.9 | 8.3 | 8.7 | 9.1 | 9.4 | 9.8 | 10.2 | 10.6 |
| 67 | 7.3 | 7.7 | 8.1 | 8.5 | 8.9 | 9.4 | 9.8 | 10.2 | 10.6 | 11.0 |
| 68 | 7.6 | 8.0 | 8.4 | 8.9 | 9.3 | 9.7 | 10.1 | 10.5 | 11.0 | 11.4 |
| 69 | 7.9 | 8.3 | 8.8 | 9.2 | 9.6 | 10.1 | 10.5 | 10.9 | 11.3 | 11.8 |
| 70 | 8.1 | 8.6 | 9.0 | 9.5 | 9.9 | 10.4 | 10.9 | 11.3 | 11.8 | 12.2 |
| 71 | 8.1 | 8.9 | 9.3 | 9.8 | 10.3 | 10.8 | 11.2 | 11.7 | 12.2 | 12.6 |
| 72 | 8.7 | 9.2 | 9.7 | 10.2 | 10.7 | 11.2 | 11.6 | 12.1 | 12.6 | 13.1 |
| 73 | 9.0 | 9.5 | 10.0 | 10.5 | 11.0 | 11.6 | 12.1 | 12.6 | 13.1 | 13.6 |
| 74 | 9.4 | 9.9 | 10.4 | 11.0 | 11.5 | 12.0 | 12.5 | 13.0 | 13.6 | 14.1 |
| 75 | 9.7 | 10.2 | 10.8 | 11.3 | 11.9 | 12.4 | 12.9 | 13.5 | 14.0 | 14.6 |
| 76 | 10.0 | 10.6 | 11.1 | 11.7 | 12.3 | 12.9 | 13.4 | 14.0 | 14.6 | 15.1 |
| 77 | 10.4 | 11.0 | 11.6 | 12.2 | 12.8 | 13.4 | 13.9 | 14.5 | 15.1 | 15.7 |
| 78 | 10.8 | 11.4 | 12.0 | 12.6 | 13.2 | 13.9 | 14.5 | 15.1 | 15.7 | 16.3 |
| 79 | 11.2 | 11.8 | 12.5 | 13.1 | 13.7 | 14.4 | 15.0 | 15.6 | 16.2 | 16.9 |
| 80 | 11.6 | 12.3 | 12.9 | 13.6 | 14.2 | 14.9 | 15.5 | 16.2 | 16.8 | 17.5 |

TABLE X1.5 Humidity, Grams/Kilogram Correction Factors (101.6 to 104.6 kPa)

| Dew <br> Point <br> Temp ${ }^{\circ} \mathrm{C}$ | 104.6 | 104.3 | 104.0 | 103.6 | 103.3 | 102.9 | 102.6 | 102.1 | 101.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18.3 | -0.44 | -0.40 | -0.36 | -0.32 | -0.27 | -0.23 | -0.17 | -0.13 | -0.09 |
| 18.9 | -0.46 | -0.41 | -0.37 | -0.32 | -0.27 | -0.23 | -0.19 | -0.14 | -0.09 |
| 19.4 | -0.47 | -0.43 | -0.37 | -0.33 | -0.29 | -0.24 | -0.19 | -0.14 | -0.10 |
| 20.0 | -0.49 | -0.44 | -0.39 | -0.34 | -0.29 | -0.24 | -0.20 | -0.14 | -0.10 |
| 20.6 | -0.50 | -0.46 | -0.40 | -0.36 | -0.30 | -0.26 | -0.20 | -0.16 | -0.04 |
| 21.1 | -0.53 | -0.47 | -0.43 | -0.37 | -0.32 | -0.27 | -0.21 | -0.16 | -0.04 |
| 21.7 | -0.54 | -0.49 | -0.43 | -0.39 | -0.33 | -0.27 | -0.21 | -0.16 | -0.10 |
| 22.2 | -0.56 | -0.50 | -0.44 | -0.39 | -0.33 | -0.29 | -0.23 | -0.17 | -0.11 |
| 22.8 | -0.59 | -0.53 | -0.47 | -0.41 | -0.36 | -0.30 | -0.23 | -0.17 | -0.11 |
| 23.3 | -0.60 | -0.54 | -0.49 | -0.41 | -0.36 | -0.30 | -0.24 | -0.19 | -0.11 |
| 23.9 | -0.63 | -0.57 | -0.50 | -0.44 | -0.37 | -0.31 | -0.26 | -0.19 | -0.11 |
| 24.4 | -0.64 | -0.59 | -0.51 | -0.46 | -0.39 | -0.33 | -0.26 | -0.20 | -0.13 |
| 25.0 | -0.67 | -0.60 | -0.54 | -0.47 | -0.40 | -0.34 | -0.27 | -0.20 | -0.13 |
| 25.6 | -0.70 | -0.63 | -0.56 | -0.49 | -0.41 | -0.36 | -0.29 | -0.21 | -0.13 |
| 26.1 | -0.72 | -0.64 | -0.57 | -0.50 | -0.43 | -0.36 | -0.29 | -0.21 | -0.14 |
| 26.7 | -0.74 | -0.67 | -0.60 | -0.51 | -0.44 | -0.37 | -0.30 | -0.23 | -0.14 |

TABLE X1.6 Humidity, Grams/Kilogram Correction Factors (98.2 to 101.2 kPa )

| Dew Point | Barometric Pressure (kPa) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Temp ${ }^{\circ} \mathrm{C}$ | 101.2 | 100.9 | 100.6 | 100.2 | 99.9 | 99.5 | 99.2 | 98.9 | 98.5 | 98.2 |
| 18.3 | 0 | 0.04 | 0.10 | 0.14 | 0.19 | 0.24 | 0.29 | 0.33 | 0.37 | 0.43 |
| 18.9 | 0 | 0.04 | 0.10 | 0.14 | 0.20 | 0.24 | 0.29 | 0.34 | 0.39 | 0.44 |
| 19.4 | 0 | 0.06 | 0.10 | 0.16 | 0.20 | 0.26 | 0.30 | 0.36 | 0.40 | 0.46 |
| 20.0 | 0 | 0.06 | 0.10 | 0.16 | 0.21 | 0.27 | 0.32 | 0.37 | 0.43 | 0.47 |
| 20.6 | 0 | 0.06 | 0.11 | 0.16 | 0.21 | 0.27 | 0.33 | 0.39 | 0.43 | 0.49 |
| 21.1 | 0 | 0.06 | 0.11 | 0.17 | 0.23 | 0.29 | 0.33 | 0.39 | 0.44 | 0.50 |
| 21.7 | 0 | 0.06 | 0.11 | 0.17 | 0.23 | 0.30 | 0.36 | 0.41 | 0.47 | 0.53 |
| 22.2 | 0 | 0.06 | 0.11 | 0.19 | 0.24 | 0.30 | 0.36 | 0.41 | 0.49 | 0.54 |
| 22.8 | 0 | 0.06 | 0.13 | 0.19 | 0.26 | 0.32 | 0.37 | 0.44 | 0.50 | 0.57 |
| 23.3 | 0 | 0.07 | 0.13 | 0.20 | 0.26 | 0.33 | 0.40 | 0.46 | 0.53 | 0.59 |
| 23.9 | 0 | 0.07 | 0.13 | 0.20 | 0.27 | 0.34 | 0.40 | 0.47 | 0.54 | 0.60 |
| 24.4 | 0 | 0.07 | 0.14 | 0.21 | 0.29 | 0.36 | 0.41 | 0.49 | 0.56 | 0.63 |
| 25.0 | 0 | 0.07 | 0.14 | 0.21 | 0.29 | 0.37 | 0.44 | 0.51 | 0.59 | 0.66 |
| 25.6 | 0 | 0.07 | 0.14 | 0.23 | 0.30 | 0.37 | 0.44 | 0.51 | 0.60 | 0.67 |
| 26.1 | 0 | 0.07 | 0.16 | 0.23 | 0.32 | 0.39 | 0.46 | 0.54 | 0.61 | 0.70 |
| 26.7 | 0 | 0.09 | 0.16 | 0.24 | 0.32 | 0.40 | 0.49 | 0.56 | 0.64 | 0.72 |

TABLE X1.7 Humidity, Grams/Kilogram Correction Factors (94.8 to 97.9 kPa )

| DewPointTemp ${ }^{\circ} \mathrm{C}$ | Barometric Pressure (kPa) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 97.9 | 97.5 | 97.2 | 96.8 | 96.5 | 96.2 | 95.8 | 95.5 | 95.2 | 94.8 |
| 18.3 | 0.47 | 0.53 | 0.57 | 0.63 | 0.67 | 0.73 | 0.77 | 0.83 | 0.87 | 0.93 |
| 18.9 | 0.49 | 0.54 | 0.59 | 0.65 | 0.70 | 0.76 | 0.80 | 0.86 | 0.92 | 0.96 |
| 19.4 | 0.50 | 0.56 | 0.61 | 0.66 | 0.72 | 0.77 | 0.83 | 0.89 | 0.93 | 0.99 |
| 20.0 | 0.53 | 0.59 | 0.64 | 0.70 | 0.76 | 9.82 | 0.86 | 0.92 | 0.97 | 1.03 |
| 20.6 | 0.54 | 0.60 | 0.66 | 0.72 | 0.77 | 0.84 | 0.90 | 0.96 | 1.02 | 1.07 |
| 21.1 | 0.56 | 0.61 | 0.67 | 0.74 | 0.80 | 0.86 | 0.92 | 0.97 | 1.04 | 1.10 |
| 21.7 | 0.59 | 0.64 | 0.72 | 0.77 | 0.83 | 0.90 | 0.96 | 1.02 | 1.07 | 1.14 |
| 22.2 | 0.60 | 0.67 | 0.73 | 0.80 | 0.86 | 0.93 | 0.99 | 1.06 | 1.12 | 1.19 |
| 22.8 | 0.63 | 0.70 | 0.76 | 0.83 | 0.89 | 0.96 | 1.03 | 1.09 | 1.16 | 1.22 |
| 23.3 | 0.66 | 0.73 | 0.80 | 0.86 | 0.93 | 1.00 | 1.07 | 1.14 | 1.20 | 1.27 |
| 23.9 | 0.67 | 0.74 | 0.82 | 0.89 | 0.96 | 1.03 | 1.10 | 1.17 | 1.24 | 1.32 |
| 24.4 | 0.70 | 0.77 | 0.84 | 0.92 | 0.99 | 1.07 | 1.14 | 1.22 | 1.29 | 1.36 |
| 25.0 | 0.73 | 0.80 | 0.89 | 0.96 | 1.03 | 1.12 | 1.19 | 1.26 | 1.33 | 1.42 |
| 25.6 | 0.74 | 0.83 | 0.90 | 0.99 | 1.06 | 1.14 | 1.23 | 1.30 | 1.39 | 1.46 |
| 26.1 | 0.77 | 0.86 | 0.94 | 1.02 | 1.10 | 1.19 | 1.27 | 1.36 | 1.43 | 1.52 |
| 26.7 | 0.80 | 0.89 | 0.97 | 1.06 | 1.14 | 1.23 | 1.32 | 1.40 | 1.49 | 1.57 |

TABLE X1.8 Humidity, Grams/Kilogram Correction Factors (91.4 to 94.5 kPa )


TABLE X1.9 Saturation Vapor Pressure Over Water (Smithsonion Tables) ${ }^{A}$

| Dew Point Temp ${ }^{\circ} \mathrm{F}$ | Vapor Press. in. Hg | Dew Point Temp ${ }^{\circ} \mathrm{F}$ | Vapor Press in. Hg |
| :---: | :---: | :---: | :---: |
| 60 | 0.52160 | 75 | 0.87506 |
| 61 | 0.54047 | 76 | 0.90472 |
| 62 | 0.55994 | 77 | 0.93524 |
| 63 | 0.58002 | 78 | 0.96666 |
| 64 | 0.60073 | 79 | 0.99900 |
| 65 | 0.62209 | 80 | 1.03230 |
| 66 | 0.64411 | 81 | 1.06650 |
| 67 | 0.66681 | 82 | 1.10170 |
| 68 | $0.69021$ | 83 | $1.13800$ |
| 69 | 0.71432 | 84 | 1.17520 |
| 70 | 0.73916 | 85 | 1.21360 |
| 71 | 0.76467 | 86 | 1.25300 |
| 72 | 0.79113 | 87 | 1.29350 |
| 73 | 0.81829 | 88 | 1.33510 |
| 74 | 0.84626 | 89 | 1.37790 |

${ }^{\text {AR Reprinted from Selecting Humidity Sensors for Industrial Processes Handbook, General Eastern Instrument Corp., March, } 1982 .}$

## X2. REPORT FORMS

X2.1 Examples of report forms making up the 1M-PC final report are shown in Figs. X2.1 and X2.2.

| LAB: OK | IEOT DATE: | 1980101 | END TIME: | 15:05 |
| :---: | :---: | :---: | :---: | :---: |
| STAND: |  | RUN NUMBER: | 34 |  |
| FORMULATION |  |  |  |  |
| OIL CODE/CMIR: |  |  |  |  |



FIG. X2.1 Form 14 (Example)—Piston and Ring Photographs

| LAB: OK | EOT DATE: | 1980101 | END TIME: | 15:05 |
| :--- | :--- | :--- | :--- | :--- |
| STAND: | 3 | RUN NUMBER: | 34 |  |
| FORMULATION STAND CODE: |  |  |  |  |
|  |  |  |  |  |




STAND is Calibrated: YES MO (Circle Required)
Colibration Expiration Date: $\qquad$ or 14 Tests

- InC Validity Code: $\qquad$
$\qquad$ STAND PULLED FRON LTMS (Check REquired)
Reviewer Initials: $\qquad$
- Based on review of call-in report of operational date and LTMS analyais shown above.

FIG. X2.2 Form 17 (Example)—TMC Control Chart Analysis

X3.1 If testing candidate lubricants in accordance with Specification D 4485, the results of multiple testing should be reported on the form shown as Fig. X3.1.

| OIL CODE NO. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ENGINE |  |  | LAB UNADJUSTED RATING |  | $\begin{gathered} \text { LAB SA } \\ \text { ADJUSTED } \end{gathered}$ |  | RING <br> SIDE <br> CLEAR. <br> LOSS <br> (mm) |
| $\begin{aligned} & \text { TEST } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { DATE } \\ & \text { TEST } \\ & \text { COMP. } \end{aligned}$ | $\begin{gathered} \text { OIL } \\ \text { CODE } \end{gathered}$ NO. | $\begin{aligned} & \hline \text { TEST } \\ & \text { LAB } \end{aligned}$ | $\begin{aligned} & \text { SERIAL } \\ & \text { NO, } \end{aligned}$ | $\begin{array}{c\|} \hline \text { STAND } \\ \text { NO. } \end{array}$ | $\begin{aligned} & \hline \text { RUN } \\ & \text { NO. } \end{aligned}$ | WTD | TGF | WTD | TGF |  |
| $1^{\text {ST }}$ |  |  |  |  |  |  |  |  |  |  |  |
| 2 |  |  |  |  |  |  |  |  |  |  |  |
| 3 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 2 |  |  |  |  |  |  |  |  |  |  |  |
| 3 |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  | . | 【"..... |  | \% | (\%. |  |  |  |
| 2 TEST AVERAGE WITH OUTLIER REMOVED 3 TEST AVERAGE WITH OUTLIER REMOVED |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

FIG. X3.1 1M-PC Multiple Test Data Summary Sheet

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[^0]:    ${ }^{1}$ This test method is under the jurisdiction of ASTM Committee D02 on Petroleum Products and Lubricants and is the direct responsibility of Subcommittee D02.B on Automotive Lubricants. The test engine sequences were originally developed in 1956 by ASTM Committee D-2. Subsequently, the procedures were published in an ASTM Special Technical Publication.

    Current edition approved Dec. 10, 2000. Published March 2001.
    ${ }^{2}$ ASTM Test Monitoring Center, 6555 Penn Avenue, Pittsburgh, PA 15206-4489.

[^1]:    ${ }^{3}$ Annual Book of ASTM Standards, Vol 05.01.

[^2]:    ${ }^{4}$ Annual Book of ASTM Standards, Vol 05.05 .
    ${ }^{5}$ Annual Book of ASTM Standards, Vol 05.02.
    ${ }^{6}$ Annual Book of ASTM Standards, Vol 05.03.
    ${ }^{7}$ Annual Book of ASTM Standards, Vol 14.03.
    ${ }^{8}$ Available from Society of Automotive Engineers, 400 Commonwealth Drive, Warrendale, PA 15096.
    ${ }^{9}$ Available from Standardization Documents Order Desk, Building 4, Section D, 700 Robbins Avenue, Philadelphia, PA 19111-5904, Attn: NPODS.

[^3]:    ${ }^{10}$ Send P-tubes to be inspected to Perkin Elmer Automotive Research, 5404 Bandera Road, San Antonio, TX 78238.

[^4]:    ${ }^{11}$ Southwest Research Institute, 6220 Culebra Road, P.O. Drawer 28510, San Antonio, TX 78228-0510.
    ${ }^{12}$ Available from J. P. Bushnell, 3436 Lindell Blvd., St. Louis, MO.
    ${ }^{13}$ The sole source of supply of the apparatus known to the committee at this time is noted in the adjoining footnote. If you are aware of alternative suppliers, please provide this information to ASTM Headquarters. Your comments will receive careful consideration at a meeting of the responsible tecnical committee, ${ }^{1}$ which you may attend.
    ${ }^{14}$ Available from Micro Motion, Inc., 7070 Winchester Circle, Boulder, CO 80301.
    ${ }^{15}$ Available from Asco, Florham Park, New Jersey 07932.

[^5]:    ${ }^{16}$ Caterpillar Inc., Engine System Technology Department, P.O. Box 610, Mossville, IL 61552.
    ${ }^{17}$ Caterpillar Inc., Tech Center TC-L, Wing 4, Room 405, 14009 Old Galena Rd., Mossville, IL 61552.

[^6]:    ${ }^{18}$ Crankcase paint in one gallon cans as Yellow Primer Paint Cat Part \#IE2083A, Primer \#A123590, Serial \#BIM0115877, B.A.S.F. Part \#U27TD005 is available from B.A.S.F. Coating and Cocorant Division, P.O. Box 1297, Morganton, NC 28655; and as Glyptal 1201 Red Enamel, Brownell Outlet, 84 Executive Avenue, Edison, NJ 08817.
    ${ }^{19}$ Available from Howell Hydrocarbons and Chemicals, Inc., 1201 South Sheldon Road, P.O. Box 429, Channel View, TX 77530.
    ${ }^{20}$ Available directly from Nalco, 4639 Corona Drive, Suite 61, Corpus Christi, TX 78441.
    ${ }^{21}$ Available from The Lubrizol Corporation, 29400 Lakeland Blvd., Cleveland, OH 44092.

[^7]:    ${ }^{A}$ This check list is made to cover the maintenance to be performed before and during each test. Included are those parts, in addition to the piston rings and liner, to be installed new at the beginning of each test. Replace all gaskets that are disturbed during such disassembly and assembly that takes place between tests or at intermediate inspections. Carefully inspect seals before their reuse.
    ${ }^{B}$ ENGINE: 1 Y73 130 mm ( 5.125 in .) bore, 165 mm ( 6.5 in .) stroke.
    ${ }^{c}$ Leakdown time $8-45 \mathrm{~s}$ for 3.175 mm ( 0.125 in .) plunger travel under a $22.68 \mathrm{~kg}(50 \mathrm{lb})$ load and filled with kerosene having a viscosity of 35 sus at $21.1^{\circ} \mathrm{C}\left(70^{\circ} \mathrm{F}\right)$.

[^8]:    ${ }^{22}$ TEI CLR engine oil filter housing \#2418 and filter element \#3105 have been found satisfactory for this use. Available from Test Engineering, Inc., 12758 Cimarron Path, Suite 102, San Antonio, TX 78429.
    ${ }^{23}$ Available from UNOCAL Chemicals Division, 7010 Mykawa Street, Houston, TX 77033.

[^9]:    ${ }^{24}$ Non-compounded oil ISO VG (SAE 20) (see Classification D 2422) is available from lubricant marketers. One supplier is Mobile Corporation. The Mobile product is designated EF-411 and is available from Mobile Corporation, Illinois Order Board, P.O. Box 66940, AMF O’Hare, IL 60666. Ask for P/N 47503-8.

[^10]:    ${ }^{25}$ Parts P-180 (Honall Head and Driver Group), PK-16-A (Adapter), JK 16-495AS (Mandrel), LN 3703 (Stone Retainer), K16-J68 (Stones), S-495 (Truing Stone), MAN-845-5 (Honing Oil), P-300 (Dial Bore Gauge), and P-500 (Gauge Probe) are available from Valve Guide Honing \& Measurement Equipment, Sunnen Products Company, 7910 Manchester Road, St. Louis, MO 63143. Ringmaster Set 067-30-010-3 (used to set P-300 gauge) available from Ralmike's Tool-A-Rama, 4505 South Clinton Avenue, South Plainfield, NJ 07080. D-30LR-4 Air Drill-400r/ min available from Stanley Tools Division, 700 Beta Drive, Cleveland, OH 44141. Pd-3-3/8 Air Drill and Small Parts Washers available from Local Distributors of Snap-On Tools, Kenosha, WI.

[^11]:    ${ }^{A}$ Follow standard cool down procedure (see Table 8).
    ${ }^{B}$ Measure blowby over last 15 min of the break-in record.

[^12]:    ${ }^{26}$ Available from Coordinating Research Council, 219 Perimeter Ctr. Pkwy., Atlanta, GA 30346.
    ${ }^{27}$ Available from Newark Electrical Corp., 500 N. Pulaski Road, Chicago, IL 60624.

[^13]:    ${ }^{28}$ A list of approved desiccants can be obtained from CRC. No-Wrap Rust Inhibitor Rectangle has been found satisfactory. Available from Alling and Cory Co., 12555 Berea Road, Cleveland, OH 44111.

[^14]:    ${ }^{A}$ This example is for 21 test hours, using humidity measured in grains/lb.

[^15]:    ${ }^{29}$ Caterpillar Inc., Tech Center, Bldg. L, 100 N.E. Adams Street, Peoria, IL 61629

[^16]:    ${ }^{A} 40^{\circ} \mathrm{F}$ per turn - normally closed - contacts open with increase of temperature. Turning screw counter-clockwise causes contacts to open at a higher temperature.
    ${ }^{B}$ Set to" pop off" at $137.9 \pm 3.4 \mathrm{kPa}(20 \pm 0.5 \mathrm{psi}$.
    ${ }^{C}$ Make gasket to fit top ring (2-2) and pad (2-6).
    ${ }^{D}$ Terminal on element goes to inside of barrel on inner rings and to outside of barrel on outer rings.

[^17]:    Notes: $\quad{ }_{B}^{A}$ Non-reference tests only
    ${ }^{B}$ Reference tests only

[^18]:    A Number blow "E" located on top of piston
    B Number on top of "E" located on top of piston
    ${ }^{C}$ Four alphanumeric characters (NNAN) on liner O.D.
    D Four digit number on liner O.D.
    E Three or four digit number on white label on ring set box
    F NN-NN from part number label on ring set box

[^19]:    (5) DATA AREA OBSERVED BUT ONLY RECORDED IF OFF SPEC.
    (6) DATA ARE RECORDED BUT ARE NOT RETAINED ATA LOGGED AS PERMANENT RECORD, NOTE SPECIFY IF

    SS - SNAPSHOT TAKEN AT SPECIFIED FREQUENCY
    AG/X AVERAGE OF X DATA POINTS AT SPECIFIED FR
    (8) TIME FOR THE OUTPUT TO REACH $63.2 \%$ OF FINAL VALUE FOR STEP CHANGE AT INPUT

    ATURE, PRESSURE
    (1) OPERATING PARAMETER
    (2) THE TYPE OF DEVICE USED TO MEASURE TEMPERATURE, PRESSURE OR FLOW
    (3) FREQUENCY AT WHICH THE MEASUREMENT SYSTEM IS CALIBRATED
    (4) THE TYPE OF DEVICE WHERE DATA IS RECORDED

    LG - HANDLOG SHEET
    DL - AUTOMATIC DATA LOGGER
    SC - STRIP CHART RECORDER
    C/M - COMPUTER, USING MANU
    FIG. A2.13 Form 10—Characteristics of Data Acquisition System

    SC - STRIP CHART RECORDER
    C/M - COMPUTER, USING MANUAL DATA ENTRY
    C/D - COMPUTER, USING DIRECT I/O ENTRY

[^20]:    FIG. A3.1 Data Dictionary (continued)

[^21]:    FIG. A3.1 Data Dictionary (continued)

