

Designation: D 6681 - 01

Standard Test Method for Evaluation of Engine Oils in a High Speed, Single-Cylinder Diesel Engine—Caterpillar 1P Test Procedure¹

This standard is issued under the fixed designation D 6681; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

INTRODUCTION

Any properly equipped laboratory without outside assistance can use the test method described in this standard. However, the ASTM Test Monitoring Center (TMC)² provides calibration oils and an assessment of the test results obtained on those oils by the laboratory. By this means the laboratory will know whether their use of the test method gives results statistically similar to those obtained by other laboratories. Furthermore, various agencies require that a laboratory utilize the TMC services in seeking qualification of oils against specifications. For example, the U.S. Army has such a requirement in some of its engine oil specifications. Accordingly, this test method is written for those laboratories that use the TMC services. Laboratories that choose not to use these services should ignore those portions of the test method that refer to the TMC. Information Letters issued periodically by the TMC may modify this method.³ In addition, the TMC may issue supplementary memoranda related to the test method.

1. Scope

- 1.1 This test method is required to evaluate the performance of engine oils intended to satisfy certain American Petroleum Institute (API) C service categories (included in Specification D 4485). It is performed in a laboratory using a standardized high-speed, single-cylinder diesel engine.⁴ Piston and ring groove deposit-forming tendency and oil consumption is measured. The piston, the rings, and the liner are also examined for distress and the rings for mobility.
- 1.2 The values stated in SI units are to be regarded as the standard.
- 1.3 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use. Being an engine test method, this standard does have definite hazards that require safe practices (see Appendix X2 on Safety).

1.4 The following is the Table of Contents:

| | Section |
|--|---------|
| Scope | 1 |
| Referenced Documents | 2 |
| Terminology | 3 |
| Summary of Test Method | 4 |
| Significance and Use | 5 |
| Apparatus and Installation | 6 |
| Intake Air System | 6.2.1 |
| Exhaust System | 6.2.2 |
| Fuel System | 6.2.3 |
| Oil Consumption System | 6.2.4 |
| Engine Oil System | 6.2.5 |
| Oil Heating System | 6.2.5.1 |
| Oil Sample Valve | 6.2.5.2 |
| Engine Coolant System | 6.2.6 |
| Engine Instrumentation | 6.2.7 |
| Reagents and Materials | 7 |
| Oil Samples | 8 |
| Preparation of Apparatus | 9 |
| General Engine Assembly Practices | 9.1 |
| Complete Engine Inspection | 9.2 |
| Copper Components | 9.3 |
| Engine Lubricant System Flush | 9.4 |
| Engine Piston Cooling Jets | 9.5 |
| Engine Measurements and Inspections | 9.6 |
| Cylinder Head | 9.7 |
| Valve Guide Bushings | 9.8 |
| Fuel Injector | 9.9 |
| Piston and Rings | 9.10 |
| Cylinder Liner | 9.11 |
| Compression Ratio | 9.12 |
| Engine Timing | 9.13 |
| Engine Coolant System Cleaning Procedure | 9.14 |
| Calibration and Standardization | 10 |
| Test Cell Instrumentation | 10.1 |
| Instrumentation Standards | 10.2 |

¹This test method is under the jurisdiction of ASTM Committee D02 on Petroleum Products and Lubricants and is the direct responsibility of Subcommittee D02.B0.02 on Heavy Duty Engine Oils.

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² ASTM Test Monitoring Ctr., 6555 Penn Ave., Pittsburgh, PA 15206–4489.

³ This edition incorporates revisions contained in all information letters through 99-1. Users of this test method shall contact the ASTM Test Monitoring Center to obtain the most recent information letters.

⁴ Available from Caterpillar Inc., Engine System Technology Development, P.O. Box 610, Mossville, IL 61552-0610.



| | Section |
|--|----------------------|
| Coolant Flow | 10.3 |
| Re-calibration Requirements | 10.4 |
| Fuel Injectors | 10.5 |
| Air Flow | 10.6 |
| Intake Air Barrel | 10.7 |
| Fuel Filter | 10.8 |
| Oil Scale Flow Rates | 10.9 |
| Calibration of Test Stands | 10.10 |
| Extending Test Stand Calibration Period | 10.11 |
| Test Run Numbering Humidity Calibration Requirements | 10.12 10.13 |
| Calibration of Piston Deposit Raters | 10.13 |
| Procedure | 10.14 |
| Engine Break-in Procedure | 11.1 |
| Cool-down Procedure | 11.2 |
| Warm-up Procedure | 11.3 |
| Shutdowns and Lost Time | 11.4 |
| Periodic Measurements | 11.5 |
| Engine Control Systems | 11.6 |
| Engine Coolant | 11.6.1 |
| Engine Fuel System | 11.6.2 |
| Engine Oil Temperature | 11.6.3 |
| Exhaust Pressure | 11.6.4 |
| Intake Air | 11.6.5 |
| Post-Test Procedures | 11.7 |
| Piston Ring Side Clearances | 11.7.1 |
| Piston Ratings | 11.7.2 |
| Referee Ratings | 11.7.2.1 |
| Ring End Gap Increase | 11.7.3 |
| Cylinder Liner Wear | 11.7.4 |
| Cylinder Liner Bore Polish | 11.7.5 |
| Photographs | 11.7.6 |
| Calculation and Interpretation of Results | 12 |
| Test Validity Calculations | 12.1 12.2 |
| Quality Index | 12.2.1 |
| Oil Consumption | 12.2.2 |
| Report | 13 |
| Forms and Data Dictionary | 13.1 |
| Test Validity | 13.2 |
| Report Specifics | 13.3 |
| Precision and Bias | 14 |
| Precision | 14.1 |
| Bias | 14.2 |
| Keywords | 15 |
| Annexes | |
| Engine and Parts Warranty | Annex A1 |
| Instrument Locations, Measurements, and Calculations | Annex A2 |
| Cooling System Arrangement | Annex A3 |
| Intake Air Mass Flow Sensor Installation | Annex A4 |
| Fuel System Design and Required Components | Annex A5 |
| Oil System | Annex A6 |
| Exhaust and Intake Barrel Piping | Annex A7 |
| Humidity Probe Installation (Location) Return Goods Authorization (Claim Form) | Annex A8 Annex A9 |
| Engine Assembly Information | Annex A10 |
| Flushing Instructions and Apparatus | Annex A11 |
| Warm-up, Cool-down and Testing Conditions | Annex A12 |
| Piston and Liner Rating Modifications | Annex A13 |
| Additional Report Forms | Annex A14 |
| Test Report Forms | Annex A15 |
| Test Report Data Dictionary | Annex A16 |
| Appendixes | |
| Various Examples for Reference Purposes | Appendix X1 |
| Safety | Appendix X2 |
| | |

2. Referenced Documents

2.1 ASTM Standards:

D 86 Test Method for Distillation of Petroleum Products at Atmospheric Pressure⁵

D 93 Test Methods for Flash Point by Pensky-Martens Closed Cup Tester⁵

⁵ Annual Book of ASTM Standards, Vol 05.01.

- D 97 Test Method for Pour Point of Petroleum Products⁵
- D 130 Test Method for Detection of Copper Corrosion from Petroleum Products by the Copper Strip Tarnish Test⁵
- D 235 Specification for Mineral Spirits (Petroleum Spirits) (Hydrocarbon Dry Cleaning Solvent)⁶
- D 445 Test Method for Kinematic Viscosity of Transparent and Opaque Liquids (the Calculation of Dynamic Viscosity)⁵
- D 482 Test Method for Ash from Petroleum Products⁵
- D 524 Test Method for Ramsbottom Carbon Residue of Petroleum Products⁵
- D 613 Test Method for Cetane Number of Diesel Fuel Oil⁷
- D 664 Test Method for Acid Number of Petroleum Products by Potentiometric Titration⁵
- D 1319 Test Method for Hydrocarbon Types in Liquid Petroleum Products by Fluorescent Indicator Adsorption⁵
- D 2274 Test Method for Oxidation Stability of Distillate Fuel Oil (Accelerated Method)⁵
- D 2425 Test Method for Hydrocarbon Types in Middle Distillates by Mass Spectrometry⁵
- D 2500 Test Method for Cloud Point of Petroleum Products⁵
- D 2622 Test Method for Sulfur in Petroleum Products by Wavelength Dispersive X-ray Fluorescence Spectrometry⁵
- D 2709 Test Method for Water and Sediment in Middle Distillate Fuels by Centrifuge⁵
- D 3227 Test Method for (Thiol Mercaptan) Sulfur in Gasoline, Kerosine, Aviation Turbine, and Distillate Fuels (Potentiometric Method)⁵
- D 3524 Test Method for Diesel Fuel Diluent in Used Diesel Engine Oils by Gas Chromatography⁸
- D 4175 Terminology Relating to Petroleum, Petroleum Products, and Lubricants⁸
- D 4052 Test Method for Density and Relative Density of Liquids by Digital Density Meter⁸
- D 4485 Specification for Performance of Engine Oils⁸
- D 4739 Test Method for Base Number Determination by Potentiometric Titration⁸
- D 4863 Test Method for Determination of Lubricity of Two-Stroke-Cycle Gasoline Engine Lubricants⁸
- D 5185 Test Method for Determination of Additive Elements, Wear Metals and Contaminants in Used Lubricating Oils and Determination of Selected Elements in Base Oils by Inductively Coupled Plasma Atomic Emission Spectrometry (ICP-AES)⁸
- D 5302 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Deposit Formation and Wear in a Spark-Ignition Internal Combustion Engine Fueled with Gasoline and Operated Under Low-Temperature, Light-Duty Conditions⁸
- D 5844 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Rusting (Sequence IID)⁹
- D 5862 Test Method for Evaluation of Engine Oils in the

⁶ Annual Book of ASTM Standards, Vol 06.04.

Annual Book of ASTM Standards, Vol 05.05.
 Annual Book of ASTM Standards, Vol 05.02.

⁹ Annual Book of ASTM Standards, Vol 05.03.

- Two-Stroke Cycle Turbo-Supercharged 6V92TA Diesel Engine⁹
- D 6202 Test Method for Automotive Engine Oils on the Fuel Economy of Passenger Cars and Light-Duty Trucks in the Sequence VIA Spark-Ignition Engine⁹
- E 29 Practice for Using Significant Digits in Test Data to Determine Conformance with Specifications¹⁰
- E 344 Terminology Relating to Thermometry and Hydrometry¹¹
- G 40 Terminology Relating to Wear and Erosion¹²
- 2.2 SAE Standard:
- SAE J183 Engine Oil Performance and Engine Service Classification¹³
- 2.3 API Standard:
- API 1509 Engine Service Classification and Guide to Crankcase Oil Selection¹⁴

3. Terminology

- 3.1 Definitions:
- 3.1.1 *additive*, *n*—a material added to another, usually in a small amount, to impart or enhance desirable properties or to suppress undesirable properties. **D 4175**
- 3.1.2 *automotive*, *adj*—descriptive of equipment associated with self-propelled machinery, usually vehicles driven by internal combustion engines. **D** 4485
- 3.1.3 *blind reference oil*, *n*—- a reference oil, the identity of which is unknown by the test facility. **D 5844**
- 3.1.3.1 *Discussion*—This is a coded reference oil which is submitted by a source independent from the test facility.
- 3.1.4 *blowby*, *n*—*in internal combustion engine*, the combustion products and unburned air-and-fuel mixture that enter the crankcase. **D 5302**
- 3.1.5 *calibrate*, *v* to determine the indication or output of a measuring device with respect to that of a standard. **E 344**
- 3.1.6 calibrated test stand, n—a test stand on which the testing of reference material(s), conducted as specified in the standard, provided acceptable test results. **Sub. B Glossary**¹⁵
- 3.1.6.1 *Discussion*—In several automotive lubricant standard test methods, the ASTM Test Monitoring Center provides testing guidance and determines acceptability.
- 3.1.7 *candidate oil*, *n*—an oil which is intended to have the performance characteristics necessary to satisfy a specification and is to be tested against that specification. **D 5844**
- 3.1.7.1 *Discussion*—These oils are mainly submitted for testing as *candidates* to satisfy a specified performance; hence the designation of the term.
- 3.1.8 debris, n—in internal combustion engines, solid contaminant materials unintentionally introduced into the engine or resulting from wear.

 D 5862
 - ¹⁰ Annual Book of ASTM Standards, Vol 14.02.
 - ¹¹ Annual Book of ASTM Standards, Vol 14.03.
 - ¹² Annual Book of ASTM Standards, Vol 03.02.
- ¹³ Available from the Society of Automotive Engineers Inc., 400 Commonwealth Drive, Warrendale, PA 15096.
- ¹⁴ Available from the American Petroleum Institute, 1220 L Street NW, Washington D.C., 20005.
- ¹⁵ Available from the Test Monitoring Center (TMC), 6555 Penn Avenue, Pittsburgh, PA 15206–4489.

- 3.1.9 *disperant*, *n*—*in engine oil*, an additive that reduces deposits on oil-wetted surfaces primarily through suspension of particles. **D 4175**
- 3.1.10 *engine oil*, n—a liquid that reduces friction or wear, or both, between the moving parts within an engine; removes heat, particularly from the underside of pistons; and serves as a combustion gas sealant for the piston rings. **D** 5862
- 3.1.10.1 *Discussion*—It may contain additives to enhance certain properties. Inhibition of engine rusting, deposit formation, valve train wear, oil oxidation and, foaming are examples.
- 3.1.11 heavy-duty, adj—in internal combustion engine operation, characterized by average speeds, power output, and internal temperatures that are close to the potential maximums.

D 4485

- 3.1.12 *lubricant*, *n*—any material interposed between two surfaces that reduces the friction or wear, or both, between them. **D 5862**
- 3.1.13 *lubricating oil*, *n*—a liquid lubricant, usually comprising several ingredients, including a major portion of base oil and minor portions of various additives.

 Sub. B Glossarv¹⁵
- 3.1.14 *oxidation*, *n*—*of engine oil*, the reaction of the oil with an electron acceptor, generally oxygen, that can produce deleterious acidic or resinous materials often manifested as sludge formation, varnish formation, viscosity increase, or corrosion, or a combination thereof.

 Sub. B Glossary¹⁵
- 3.1.15 *non-reference oil*, *n*—any oil other than a reference oil; such as a research formulation, commercial oil, or candidate oil. **D 5844**
- 3.1.16 *purchaser*, *n*—*of an ASTM test*, person or organization that pays for the conduct of an ASTM test method on a specified product. **D 6202**
- 3.1.17 *reference oil*, *n*—an oil of known performance characteristics, used as a basis for comparison. **D 5844**
- 3.1.17.1 *Discussion*—Reference oils are used to calibrate testing facilities, to compare the performance of other oils, or to evaluate other material (such as seals) that interact with oils.
- 3.1.18 scoring, n—in tribology, a severe form of wear characterized by the formation of extensive grooves and scratches in the direction of sliding.

 G 40
- 3.1.19 *scuff, scuffing, n—in lubrication*, damage caused by instantaneous localized welding between surfaces in relative motion that does not result in immobilization of the parts.

D 4863

- 3.1.20 *sponsor*, *n*—*of an ASTM test method*, an organization that is responsible for ensuring supply of the apparatus used in the test procedure portion of the test method. Sub. B Glossary¹⁵
- 3.1.20.1 *Discussion*—In some instances, such as a test method for chemical analysis, an ASTM working group can be the sponsor of the test method. In other instances, a company with a self-interest may or may not be the developer of the test procedure used within the method, but is the sponsor of the test method.
- 3.1.21 *used oil*, *n*—any oil that has been in a piece of equipment (for example, an engine, gearbox, transformer, or turbine), whether operated or not. **D 4175**

- 3.1.22 *varnish*, *n*—in internal combustion engines, a hard, dry, generally lustrous deposit that can be removed by solvents but not by wiping with a cloth. **D 5302**
- 3.1.23 *wear*, *n*—the loss of material from, or relocation of material on, a surface. **D** 5302
- 3.1.23.1 *Discussion*—Wear generally occurs between two surfaces moving relative to each other, and is the result of mechanical or chemical action, or by a combination of mechanical and chemical actions.

4. Summary of Test Method

4.1 Prior to each test, the power section of the engine is disassembled, solvent-cleaned, measured, and rebuilt in strict accordance with the specifications. A new piston, ring assembly, and cylinder liner are measured and installed for each test. The engine crankcase is solvent-cleaned and worn or defective parts are replaced. The test stand is equipped with feedback control systems for fuel rate, engine speed, and other engine operating conditions. A suitable system for filtering, compressing, humidifying, and heating the inlet air shall be provided along with a system for controlling the engine exhaust pressure. Test operations involve the control of the single-cylinder diesel test engine for a total of 360 h at specified speeds and fuel rate input using the test oil as a lubricant. A defined break-in precedes each test and is also used when restarting an engine. At the end of the test, the piston deposits are rated, the piston, rings and liners are photographed, inspected and measured, oil consumption is calculated and the oil is analyzed to determine the test results. Critical engine conditions are statistically analyzed to determine if the test was precisely operated. Test acceptability parameters for each calibration test are also statistically analyzed to determine if the engine/test stand produce the specified results.

5. Significance and Use

5.1 This is an accelerated engine oil test, performed in a standardized, calibrated, stationary single-cylinder diesel engine that gives a measure of (1) piston and ring groove deposit forming tendency, (2) piston, ring and liner scuffing and (3) oil consumption. The test is used in the establishment of diesel engine oil specification requirements as cited in Specification D 4485 for appropriate API Performance Category C oils (API 1509). The test method can also be used in diesel engine oil development.

6. Apparatus and Installation

- 6.1 The test engine is an electronically controlled, direct injection, in-head camshaft, single-cylinder diesel engine with a four-valve arrangement. The engine has a 137.2 mm bore and a 165.1 mm stroke resulting in a displacement of 2.4 L.
- 6.1.1 The electronic control module (ECM) defines the desired engine fuel timing, monitors and limits maximum engine speed, maximum engine power, minimum oil pressure, and, optionally, maximum engine crankcase pressure. The ECM also controls the fuel injection duration that defines the engine fuel rate based on set conditions from the test cell feedback control systems. The oil pressure is also set by the ECM with signals to the 1Y3867 engine air pressure controller

- (Mamac) to modulate the facility air supply to the 1Y3898 Johnson Controls relief valve.
- 6.1.2 The 1Y3700 engine arrangement also consists of inlet air piping and hoses from the cylinder head to the air barrel and exhaust piping and bellows from the cylinder head to the exhaust barrel that are specifically designed for oil testing.¹⁶
- 6.2 Equip the engine test stand with the following accessories or equipment:
- 6.2.1 *Intake Air System*—The intake air system components from the cylinder head to the air barrel are a part of the basic 1Y3700 engine arrangement. These components consisting of an adapter, elbow, hose, clamps, and flanged tube can be found in the 1Y3700 Parts Book.¹⁷
- 6.2.1.1 The 1Y3978 intake air barrel (which is almost identical to the exhaust barrel except for the top cover) has been specifically designed and shall be purchased from one of the three approved manufacturers. ¹⁸ Install the intake air barrel at the location shown in Annex A7. Do not add insulation to the barrel.
- 6.2.1.2 Paint the inside of the intake air piping with Caterpillar yellow primer or red Glyptal prior to installation.¹⁹
- 6.2.1.3 Install the air heater elements in the intake air barrel as specified in Annex A7 (even if they will not be supplied with electricity).²⁰
- 6.2.1.4 Use an air filter capable of 10 μ (or smaller) filtration.
- 6.2.1.5 Use a Sierra Model 780 airflow meter with Feature 1 = F6, Feature 2 = CG and calibration temperature = 60°C to measure intake airflow for each calibration test.²¹ Annex A4 shows the piping requirements for the installation of the Sierra Model 780 airflow meter.
- 6.2.1.6 Measure the inlet air temperature at the location shown in Annex A2. Measure the inlet air pressure at the air barrel as shown in Annex A7. The location of the 1Y3977 humidity probe is shown in Annex A8. The sample line may require insulation to prevent dropping below dew point temperature and shall not be hygroscopic. Drain taps may be installed at the low points of the combustion air system.
- 6.2.1.7 Use feedback-equipped controls to maintain filtered, compressed, and humidified inlet air at the conditions specified in Annex A12.
- 6.2.2 Exhaust System—The exhaust system components from the cylinder head to the exhaust barrel are part of the basic 1Y3700 engine arrangement. These components consisting of an adapter, elbow, bellows, flange, and clamps can be found in the 1Y3700 Parts Book.

¹⁶ See the Caterpillar Service Manual. Available from Caterpillar Inc., Engine System Technology Development, P.O. Box 610, Mossville, IL 61552-0610.

¹⁷ Available from Caterpillar Inc., Engine System Technology Development, P.O. Box 610, Mossville, IL 61552-0610.

¹⁸ Cimino Machinery Corp., 5958 South Central Ave., Chicago, IL 60638; Gaspar Inc., 4106 Mahoning Rd. N.E., Canton, OH 44705; M.L. Wyrick Welding, 2301 Zanderson Highway 16 N, Jourdanton, TX 78026.

¹⁹ Crankcase Paint Primer: BASF Coating and Colorant Div., P.O. Box 1297, Morganton, NC 28655. (Primer No.A123590 and BASF Part No.U27YD005, Yellow CAT Primer Part No.IE2083A.)

²⁰ Watlow Air Heaters, Chicago, IL 708-490-3900.

²¹ Sierra Instruments, Inc., 5 Harris Ct., Monterey, CA 93940.

- 6.2.2.1 The 1Y3976 exhaust barrel (which is almost identical to the intake barrel except for the top cover) has been specifically designed and shall be purchased from one of the three approved manufacturers. ¹¹ Install the exhaust barrel at the location shown in Annex A7. Do not add insulation to the barrel.
- 6.2.2.2 Install a restriction valve downstream from the exhaust barrel. The distance between the valve and barrel is not specified. The location of the exhaust thermocouple is shown in Annex A2. Measure the exhaust pressure at the exhaust barrel shown in Annex A7.
- 6.2.2.3 Use feedback-equipped controls to maintain the exhaust gases at the pressure specified in Annex A12.
- 6.2.3 Fuel System—The fuel system schematic is shown in Annex A5. Desired fuel injection timing is controlled by the engine computer at 13° BTC. Measure the fuel rate using micro motion device with a 90 kg/h maximum range scaled to the 1P operation range specified in Annex A12.²² Use the day tank specified in Annex A5. Measure fuel temperature at the fuel filter base as shown in Annex A2 and control it using the cell facility feedback system. Use the required fuel heat exchanger(s) and arrange them as specified in Annex A5. Use the Fisher regulator specified in Annex A5.
- 6.2.4 *Oil Consumption System*—Use an oil scale system to accurately measure oil consumption (see Figs. A6.2 and A6.3). The oil scale system shall have a resolution as listed in Annex A2. Use flexible hoses similar to Aeroquip flexible hose, FC352-08, to-and-from the oil scale reservoir to eliminate measurement errors.²³ Use No.5 TFE-fluorocarbon, steel-braided hoses to and from the oil scale pumps. The hose length to-and-from the oil scale cart shall not exceed 2.7 m. Use the special oil pan adapter described in Fig. A6.4. The flow rates for the oil consumption oil scale pumps shall be 23.6-24.9 kg/h for the oil being pumped from the oil pan to the oil scale, and 16.3-17.7 kg/h for the oil being pumped from the oil scale to the oil pan. See Annex A6 for the procedure to verify these flow rates.
- 6.2.5 Engine Oil System—A schematic of the oil system is shown in Fig. A6.1. Measure oil pressure at the engine oil manifold (see Annex A2). An engine oil pressure sensor transmits a signal to the ECM that maintains oil pressure at 415 kPa. The ECM transmits a signal to an engine-mounted Mamac air pressure controller. The Mamac modulates the facility air pressure of 280 kPa to levels that vary between 0 to 140 kPa and directs it to the normally closed Johnson Controls relief valve. Because the engine oil pressure sensor calibration may vary from the cell data acquisition transducer, vary the oil pressure adjust signal to the ECM to maintain the oil pressure at the test specifications. See the Electronic Installation and Operation manual for additional information. The ECM maintains the oil pressure regardless of engine speed. Measure the oil temperatures at locations shown in Annex A2.
- 6.2.5.1 *Oil Heating System*—Use an external oil heating system provided by the test facility to maintain the engine oil manifold temperature specified in Annex A12. An example

system is shown in Appendix X1. A special 1Y3908 oil cooler bonnet has been designed to allow separate fluids to the engine coolant tower arrangement (see Fig. A6.9). Plug the 1Y3660 oil cooler adapter and 1Y3908 heat exchanger bonnet as shown in Annex A6. Use Paratherm NF for the heating fluid.²⁴ The temperature of the Paratherm NF is measured by the thermocouple shown in Annex A2.

- 6.2.5.2 *Oil Sample Valve*—Refer to Annex A2 for the installation location and component makeup of the oil sample valve. Use of alternate equivalent components for the sample valve is permitted.
- 6.2.6 Engine Coolant System—The coolant system schematic is shown in Annex A3. Control the coolant temperature out of the engine using a cell facility feedback system. Use a 1Y3898 Johnson Controls valve or equivalent fail-open valve to regulate the coolant temperature out of the engine as shown by the schematic in Annex A3. If the 1Y3898 Johnson valve is used, supply facility air pressure at 280 kPa to the controller that regulates air pressure to the valve at 0-140 kPa. Install a feedback-equipped control system to pneumatically adjust the valve. Remove the 1Y3832 hose originally supplied with the engine and install a sight glass using the components shown in Annex A3.
- 6.2.7 Engine Instrumentation—Use feedback-equipped systems to control the engine operating temperatures, pressures, and flow rates. Measure the engine operating conditions at the locations shown in Annex A2. For temperature measurements, use thermocouples 1Y468 (intake air), 1Y467 (engine exhaust) and 1Y466 (fluids-water, oil, and fuel) or equivalent thermocouples as specified in Annex A2. Instrument measurement and reporting resolutions are shown in Annex A2.
- 6.2.8 A dynamometer with feedback control to maintain engine load and speed. Use a starting system capable of at least 136 Nm breakaway and 102 Nm sustained torque at 200 r/min.
- 6.2.9 Compressed air at 35 kPa to the top of the coolant tower as specified in Annex A3 to ensure water does not boil out of the antifreeze mixture and result in less heat rejection from the engine.
- 6.2.10 Measure engine blowby down stream of the engine breather housing by measuring the delta pressure across an orifice or an equivalent device.
- 6.2.11 The crankcase pressure is above atmospheric pressure with this engine arrangement. Measure it at the location shown in Annex A2.
- 6.3 Obtain information concerning the test engine, engine electronics system, new engine parts, replacement parts, and permissible substitution or replacement parts from Caterpillar, Inc.
- 6.4 Engine and parts warranty information can be found in Annex A1. Use the form listed in Annex A9 for returning defective parts.

7. Reagents and Materials

7.1 *Purity of Reagents*—Reagent grade chemicals shall be used in all tests. Unless otherwise indicated, it is intended that all reagents conform to the specifications of the Committee on

²² Micro Motion, Inc. 7070 Winchester Circle, Boulder, CO 80301.

²³ Aeroquip Industrial Div, 1225 W. Main Street, Van Wert, OH 45891.

²⁴ Paratherm NF Oil, Conshohocken, PA 19428.

Analytical Reagents of the American Chemical Society where such specifications are available.²⁵ Other grades may be used, provided it is first ascertained that the reagent is of sufficiently high purity to permit its use without lessening the accuracy of the determination.

- 7.2 Diesel Piston Rating Booth, as described by CRC Manual 18.²⁶
- 7.3 Diesel Piston Rating Lamp, as described by CRC Manual 18.
 - 7.4 Dispersant Engine Cleaner.²⁷
- 7.5 Engine Coolant—Use a mixture of 50 % mineral-free water and 50 % Caterpillar brand coolant (P/N 8C684 for 1 gal or 8C3686 for 55 gal drum) for engine coolant. Mineral-free water is defined as water having a mineral content no higher than 34.2 ppm total dissolved solids. The coolant mixture may be reused for up to 1600 h. Keep the mixture at a 50:50 ratio as determined by using either Caterpillar testers 5P3514 or 5PO957 or an equivalent tester. Keep the coolant mixture contamination free. Total solids shall remain below 5000 ppm. Keep the additive level correct using Caterpillar test kit P/N 8T5296.
- 7.6 *Lead Shot*, commercial grade, approximately 5 mm in diameter.
 - 7.7 Light Grease.
- 7.8 *Mobil EF-411*, as supplied by Mobil for engine assembly and calibration of the oil scale pump flow rates.²⁸
- 7.9 Paratherm NF, as supplied by Paratherm and used as the fluid to heat the engine oil. 24
- 7.10 *Pentane (Solvent)*, 99 + %, high-performance, liquid chromatography grade.
- 7.11 Reference Oil, as supplied by the TMC for calibration of the test stand.
- 7.12 *REO 217*, as supplied by the CRC and used when any copper components are changed.
 - 7.13 Sodium Bisulfate (NaHSO₄), commercial grade.
 - 7.14 Stoddard Solvent, Specification D 235, Part 1.
- 7.15 *Test Fuel*—The specified test fuel is Specified Fuels & Chemicals LSRD-4 diesel test fuel. The specifications are shown in Annex A14.
- 7.16 *Test Oil*—The total amount of oil needed for each lubricant test is approximately 42 L.
 - 7.17 Trisodium Phosphate (Na_3PO_4), commercial grade.
 - 7.18 5.4000 in. Ring Bore Standard Class Z Master.²⁹

8. Oil Samples

8.1 Take a 250 mL purge sample at 48, 72, 120, 144, 168, 192, 216, 264, 312 and 336 h. Following removal of the purge

sample, remove a 30 mL sample, then add 317 \pm 10 g of new oil. It is not necessary to perform analysis on these 30 mL samples. Use the purge sample to return to the full mark. At 0 (new), 24, 96, 240, 288 and 360 h, take a 250 mL purge sample. Following removal of the purge sample, remove a 90 mL sample and add 370 \pm 10 g of new oil. Analyze all 90 mL samples for 100 and 40 °C viscosity by Test Method D 445, TBN by Test Method D 4739, TAN by Test Method D 664, and the wear metals Al, Cr, Cu, Fe, Pb, Si by Test Method D 5185. Analyze the 24, 240, and 360 hour samples for fuel dilution by Test Method D 3524. See Figs. A6.7 and A6.8 for two graphical examples and a sample worksheet.

9. Preparation of Apparatus

- 9.1 General Engine Assembly Practices—As a part of good laboratory practice, inspect all components and assemblies that are exposed when the engine is disassembled and record the information for future reference. Inspect valve train components, bearings, journals, housings, seals and gaskets, and so forth and replace as needed. Assemble the engine with components and bolt torques as specified in the 1Y3700 engine Service Manual (see Annex A10 for a partial list). It is the intent of this procedure for all engine assemblies and adjustments to be targeted to the mean of the specified values. Clean and lubricate the components in keeping with good assembly practices. Keep airborne dirt and debris to a minimum in the assembly area. Maintain standard engine assembly techniques and practices (such as staggering piston ring gap positions, and so forth).
- 9.2 Complete Engine Inspection—Perform a complete engine inspection at intervals of 13 000 h. Ensure that wearing surfaces such as main bearings and journals, rod bearings and journals, camshaft bearings, valve train components, fuel system components, and so forth all are within manufacturer's specifications. Refer to the 1Y3700 Service Manual for disassembly, assembly, inspections, and specifications. Paint crankcases as necessary with either Caterpillar yellow primer or red Glyptal.¹⁹
- 9.3 *Copper Components*—Anytime a copper part is replaced, run an engine test using REO 217 until two consecutive 12-h periods show a stable copper level.
- 9.4 Engine Lubricant System Flush-Flush the engine of used oil before every test. Annex A11 shows the engine flush procedure and apparatus. A flushing instruction sheet shown in Annex A11 gives the step-by-step process required for flushing. The 1Y3700 engine arrangement includes five flushing nozzles in the crankcase and front cover (see Annex A11). These nozzles are piped in parallel with the 1Y3935 filter flushing adapter (or equivalent) from a laboratory provided manifold that pressurizes fluids supplied by a flush cart (see Appendix X1). Seal the gear train housing during flush with a 1Y3917 round plug with a 117-8801 o-ring as shown in Annex A11. Seal the crankcase using a 1Y3979 block flush cover with an internal bleed passage for the cam oil supply. Bolt a 1Y3980 plastic jet aiming fixture to the flush cover that is also used for flushing (see Annex A11). If the test oil is not available at engine assembly, Mobil EF411 oil may be substituted.
- 9.5 Engine Piston Cooling Jets—The piston cooling jets are flow-checked at the supplier and serialized to ensure proper

²⁵ Reagent Chemicals, American Chemical Society Specifications, American Chemical Society, Washington, DC. For suggestions on the testing of reagents not listed by the American Chemical Society, see Analar Standards for Laboratory Chemicals, BDH Ltd., Poole, Dorset, U.K., and the United States Pharmacopia and National Formulary, U.S. Pharmacopeial Convention, Inc. (USPC), Rockville, MD.

²⁶ Available from the Coordinating Research Council Inc., 3650 Mansell Road Suite 140, Atlanta, GA 30022-8246.

 $^{^{\}rm 27}$ Available from The Lubrizol Corp., 29400 Lakeland Blvd., Cleveland, OH 44092

²⁸ Mobil EF-411 may be purchased from Golden West Oil Co., 3010 Aniol St., San Antonio, TX 78219.

²⁹ Available from Morse-Hemco, 457 Douglas Ave., Holland, MI 49423.

performance, but the rod clearances are minimal which may result in jet movement during assembly. Verify proper jet flow positioning using EF-411 before each test with the 1Y3980 plastic jet aiming fixture and 415 kPa oil pressure to the manifold. Record the cooling jet serial number.

9.6 Engine Measurements and Inspections—Measure and inspect the engine components prior to each test (see Table A10.2 for partial specification list). Refer to the 1Y3700 Service Manual for information concerning component reusability and assembly not found in this procedure. The part numbers of components that need replacing are found in the 1Y3700 Parts Manual. Record the crankshaft angles at the specified maximum injector lift, exhaust, and intake maximum lift before each test using the reference listed in Fig. A10.7. Record component part numbers and serial numbers and other required measurements as shown in the test report. Inspect and reuse the rocker arm roller followers and camshaft lobe surfaces based on Caterpillar Service Publication SEBF8256.¹⁷

9.7 Cylinder Head—A reconditioned head is required for each test. Measurements after reconditioning shall be within specifications as shown in the 1Y3700 Service Manual. Do not swap the cylinder head/jug assembly from test stand-to-test stand. Use the head/jug assembly used to calibrate the stand for all non-reference oil testing in that stand. Fig. A10.1 shows the cylinder head nut torque sequence.

9.8 Valve Guide Bushings—Clean the valve guide bushings with a solvent and bristle brush prior to assembly. Lubricate the bushings and valve stems with Mobil EF-411 prior to assembly. See the 1Y3700 Service Manual for guide reusability specifications. Install new valve guide seals for each test.

9.9 Fuel Injector—Remove the fuel injector from the cylinder head before reconditioning commences. Refer to the 1Y3700 Service Manual for removal and assembly. Return defective fuel injectors to Caterpillar for warranty and failure-mode testing using the form listed in Annex A9.

9.10 Piston and Rings—Use a new piston (1Y3400 iron crown, 1Y3659 aluminum skirt) and new rings (1Y3802, 1Y3803, 1Y3804) for each test. Clean all three rings with pentane and a lint-free 100% cotton towel. Measure the ring side clearances and ring end gaps for all three rings (see Fig. A10.1 and Table A10.1). Keystone ring side clearance measurements require the ring to be confined in a dedicated slotted liner (see Appendix X1) or a 137.16 mm ring gage.²¹ Measure the side clearances using four feeler gages of equal width and 0.01 mm thickness at 90° intervals around the piston. Measure the rectangular ring side clearance this way as well. Measure the minimum side clearance as specified in CRC Manual 18. Record the measurements for these parts before and after each test. Compare the measurements before the test and after the test to determine the amount of wear. Assemble the piston with the part number toward the camshaft.

9.11 Cylinder Liner—Use a new 1Y3805 cylinder liner for each test. After removing the protective oil/grease with Stoddard solvent, clean the liner bore with a hot tap water and heavy-duty clothes washing detergent solution, then rinse with hot tap water. Measure and record the liner surface finish. Oil the liner bore with only Mobil EF-411. Assemble the cylinder liner, block and head with the torque specification shown in the

1Y3700 Service Manual or Fig. A10.1. Measure the liner with a dial bore gage to ensure that the out-of-round and taper conditions are within specified tolerances measured at seven intervals as shown in Fig. A10.3. Measure the cylinder liner projection using the modified indicator shown in Fig. A10.4. Torque the cylinder liner support ring using the procedure shown in Fig. A10.5.

9.12 Compression Ratio—Before starting each test, measure the piston-to-head clearance to ensure the proper compression ratio is used. Determine this dimension by using approximately 3.5 mm diameter lead balls. Locate four lead balls on the top of the piston at 90° intervals on the major and minor piston diameters. Hold them in place with light grease. With the piston near the top of the stroke, install the head and block assembly and torque to specifications. Turn the engine over top center by hand to compress the lead balls then remove the head and block assembly and measure the thickness of the lead balls to obtain the average piston-to-head clearance. The piston-to-head clearance specification is 1.62 mm \pm 0.07 mm. Use multiple 1Y3817 block gaskets to adjust the clearance. If the piston-to-head measurement exceeds the tolerance specification, check the crankshaft main and rod journals, connecting rod and main bearings, and piston pin and rod bushing for excessive wear. The specified compression ratio for the 1Y3700 engine is 16.2 to 1.

9.13 Engine Timing—The engine ECM sets desired fuel injection timing to 13° BTC. Record this timing using the engine technician service tool. Mechanically time the actual engine components as shown in Annex A10. Install the electronic sensors as shown in the Electronic Installation and Operation manual. Both the mechanical and electrical systems shall be correctly assembled to produce the desired fuel timing.

9.14 Engine Coolant System Cleaning Procedure—Clean the coolant system when visual inspections show the presence of any oil, grease, mineral deposits, or rust following the procedure listed in Annex A3.

9.15 After the engine components have been prepared and assembled, perform the following:

9.15.1 Fill the crankcase with 5800 ± 50 g of test oil.

9.15.2 Install a new 1R0713 oil filter.

9.15.3 Fill the coolant system with coolant specified in Section 7.

9.15.4 Ensure the facility coolant to the engine heat exchanger is operational.

9.15.5 Pressurize the fuel system to remove air, then return the system to a non-pressurized state before starting engine.

9.15.6 Ensure all other systems and facilities are operational before starting the engine break-in.

10. Calibration and Standardization

10.1 Test Cell Instrumentation—Calibrate all facility readout instrumentation used for the test immediately prior to subsequent stand calibration. Instrumentation calibration prior to subsequent stand calibration tests (that is, those that follow a failed or invalid first attempt) are at the discretion of the test laboratory. Refer to Annex A2 for calibration tolerances and allowable system time constants.

10.2 *Instrumentation Standards*—Calibrate all temperature, pressure, flow, and speed measurement *standards* on a yearly

basis. The calibration of all standards shall be traceable to a national bureau of standards. Maintain all calibration records for a minimum of two years.

10.3 Coolant Flow—Calibrate the coolant flow rate as follows: (1) calibrate the differential pressure transducer as outlined in 10.1 and 10.2 and, (2) replace the Barco venturi every two years. We the following relationships as conversion factors from the differential pressure across the Barco venturi to L/min: 3.0 in. $H_2O = 24.3$ L/min, 7.1 in. $H_2O = 37.8$ L/min and 28 in. $H_2O = 75.7$ L/min or use Eq 1 where ΔP is measured in in. H_2O .

$$L/min = \sqrt{\Delta P} 14.44 - 0.69$$
 (1)

10.4 Re-calibration Requirements—Re-calibration due to parts replacement is not required unless the engine crankcase or crankshaft, or both, require replacing or regrinding, or the crankshaft is removed for any other purpose besides bearing replacement, or the head/jug suffer a failure for any reason during the calibration period.

10.5 Fuel Injectors—The fuel injectors are calibrated during the manufacturing process. These fuel injectors can not be re-calibrated in the usual manner and require special test equipment to ensure proper flow, timing response, and spray patterns. Therefore, replace the fuel injector at the start of every calibration test (unless that test is the second of two required tests for a new stand or is a re-run of a previous calibration attempt). If the fuel injector is replaced on a calibrated stand, re-calibration is not required.

10.6 Air Flow—Install the Sierra Model 780 airflow meter to measure intake airflow. This meter should be calibrated yearly at a temperature of 60 °C. Measure the intake airflow during the break-in of every calibration test. Record the last value recorded during step five of the break-in as shown in Annex A12.

10.7 *Intake Air Barrel*—Prior to each stand calibration test, inspect the intake air barrel for rust or debris. This may be done through either of the pipe flanges using a borescope or some other optical means.

10.8 Fuel Filter—Change the fuel filter before every calibration test.

10.9 *Oil Scale Flow Rates*—Verify the oil scale flow rates before the start of every calibration test using the procedure listed in Annex A6.

10.10 Calibration of Test Stands—A stand calibration test is required every nine months with the test results falling within the required values before non-reference oils are run. Use a blind calibration oil from the TMC to calibrate the engine stand every nine months. The nine-month calibration period begins at the start of the last acceptable calibration test. Actual test completion dates may differ from scheduled completion dates because of unexpected downtime. Accordingly, if the last non-reference test before a new calibration is interrupted because of unscheduled shutdowns, stand calibration will continue through the completion of this non-reference test. The intention is that the non-reference test be started in time to

finish within the nine-month period, had the unscheduled shutdowns not occurred. A test stand is considered calibrated when the test results are within the acceptability limits as published by TMC and the test is operationally acceptable. The TMC may request stand checks on calibration tests that fail because of statistical reasons. Laboratory and referee rate piston deposits for all operationally valid calibration tests. Use the laboratory rating results to determine test acceptability and use the referee rating as a secondary measurement. For calibration tests, electronically send the test data to the TMC within seven days from end-of-test (EOT) in order for the test to be considered valid. The TMC will issue to the testing laboratory a control chart analysis for each calibration test (see Annex A14). The test stand is not considered calibrated for invalid or non-interpretable calibration tests.

10.11 Extending Test Stand Calibration Period—There may be occasions when laboratories conduct a large portion of calibration tests in a short period of time. This may result in an unacceptably large time frame when very few calibration tests are conducted. To ensure proper severity and precision monitoring, calibration tests shall be conducted throughout the year. The TMC is permitted to move up or extend calibration tests to enhance calibration test program design and test severity monitoring. An extensive test stand check will be required for any engines having extended test stand calibration periods.

10.12 *Test Run Numbering*—Number each test to identify the test stand number and the test run number. Number all runs sequentially. Append repeat calibration runs with a letter that is also sequential (that is, number the first re-run of test 45 as 46A, the second as 47B, and so forth). Maintain the letter suffix sequencing for each calibration test until the calibration has been accepted. Increment the run number for any test start.

10.13 Humidity Calibration Requirements—The accuracy of the laboratory's primary humidity measurement system shall be within \pm 0.6 g of the humidity measuring chilled mirror dew point hygrometer. Calibrate the primary laboratory humidity measurement system during the first 24 h of each calibration test at each stand using a chilled mirror dew point hygrometer with an accuracy of at least ± 0.55 °C at a 24°C dew point. The calibration consists of a series of paired comparison measurements between the primary system and the chilled mirror dew point hygrometer. The comparison period lasts from 20 min to 2 h with measurements taken at 1 min to 6 min intervals, for a total of 20 paired measurements. The measurement interval should be appropriate for the time constant of the humidity measuring instruments. Ensure that the flow rate is within the equipment manufacturer's specification. Take all measurements made with the dew point hygrometer at atmospheric pressure and correct them to standard pressure conditions (101.12 kPa). Compute the difference between each pair of measurements and calculate the mean and standard deviation of the differences. The absolute value of the mean difference shall not exceed 0.6 g and the standard deviation shall be less than or equal to 0.3 g. The primary humidity measurement system is deemed calibrated only if both of these requirements are met. If either of these requirements is not met, investigate the cause, make repairs, and recalibrate. Maintain the calibration data for a minimum of two years.

³⁰ Available from Hyspan Precision Products, Inc., 1685 Brandywine Avenue, Chula Vista, CA 91911.

10.14 Calibration of Piston Deposit Raters—The piston deposit raters shall be trained by the CRC Rating Task Force and maintain rating expertise by attending the rating seminars. Each calendar year, each facility shall send at least one Heavy Duty Diesel Piston Rater to either the Task Force meeting held every Spring or the expanded Heavy Duty Piston Rating Workshop held every Fall. Each rater shall rate a minimum of six diesel pistons. If this schedule is not suitable to a particular rater or test laboratory, then make alternative arrangements as soon as possible to have the rater calibrated.

11. Procedure

- 11.1 Engine Break-in Procedure—Open any drain taps at the low points of the combustion air system (if they are installed) during the start of the break-in and warm-ups, and following any shutdowns. The engine break-in and operational conditions are specified in Annex A12. The total break-in time is 85 min. During the break-in, fix all leaks and make adjustments to ensure proper engine operation. Record the ECM personality module part number and release date. After the break-in period and while the engine is hot, drain the oil from the crankcase, oil cooler, engine oil filter, and weigh scale for 30 min. Then weigh 5800 ± 50 g of new test oil into the engine. Start the engine, warm it up, and operate it for 360 h at the test conditions specified in step five of Annex A12 with no oil changes. Turn on the oil scale pumps once the engine has reached the beginning of Step 5 of the warm-up sequence. Record the oil weight in the oil scale as the full mark at the end of the first test hour. Throughout the test, record the oil scale reading at least once every 6 min. Count test time from the moment the warm-up time is completed. The oil sample frequency is described in section eight. Do not remove the cylinder head, piston, or power assembly from the engine during a test.
- 11.1.1 Reinitialize engine timing calibration after the cam shaft/gear or cylinder head has been removed. See the electronic installation and operation manual. Complete this during the first step of the break-in.
- 11.2 Cool-down Procedure—Except for emergency (uncontrolled) stops, shut the engine down by operating it at conditions shown in Steps 4, 3, 2, and then 1 in Annex A12.
- 11.3 *Warm-up Procedure*—Use the same procedure used for engine break-in to warm-up the engine for all subsequent starts throughout the test.
- 11.4 Shutdowns and Lost Time—Record the test h, date, and length of off-test conditions for all occurrences. Record when the engine has early inspections or early test termination with the reasons for the occurrences. If the cool down procedure is not used, identify the shutdown as an Emergency Shutdown. A maximum of 125 h of off-test conditions is allowed. If the engine shuts down, immediately stop the oil scale pumps. In the event of an emergency shutdown, leave the engine shut down for 2 h (or more) to allow complete engine cool down before restarting. In order to limit foreign matter entering the combustion chamber and to protect piston deposits, rotate the engine to top dead center of the compression stroke during downtime.
- 11.5 Periodic Measurements—Record all engine conditions listed in Step 5 of Annex A12 as a snapshot at least once every

- 6 min. Record humidity readings using the laboratory's primary humidity measurement system. Correct the recorded humidity values to standard pressure conditions of 101.12 kPa. Record the fuel position as indicated by the electronic technician at test hours 24, 240, and 360.
 - 11.6 Engine Control Systems:
- 11.6.1 Engine Coolant—Pressurize the coolant system to 35.0 ± 7 kPa as shown in Annex A3 to ensure the water does not boil out of the antifreeze. Manually adjust the coolant flow rate by turning the valve on top of the coolant tower to maintain the conditions specified in Annex A12.
- 11.6.2 Engine Fuel System—Control the fuel rate by modifying the fuel limit adjusting the ECM using a facility controller that compares the actual fuel rate to the specified fuel rate listed in Annex A12. See the Electronic Installation and Operation manual for more details. Manually adjust the Fisher regulator to control fuel pressure. Maintain the fuel pressure and temperature as specified in Annex A12.
- 11.6.3 Engine Oil Temperature—Maintain the oil manifold temperature to test specifications as shown in Annex A12. The temperature of the Paratherm NF shall not exceed 165 °C at any time during break-in, warm-up, or testing. Shut off the external oil heater (but not its circulating pump) the moment the engine goes to cool-down.
- 11.6.4 Exhaust Pressure—Set the pressure as specified in Annex A12 using a facility feedback-controlled restrictor valve.
- 11.6.5 *Intake Air*—Filter, compress, and humidify the inlet air to the conditions specified in Annex A12. Heat (or cool, if necessary) the inlet air to the conditions in Annex A12.
- 11.7 *Post-Test Procedures*—Remove the piston and ring assembly from the engine. Mark the location of the ring gaps on top of the piston.
- 11.7.1 Piston Ring Side Clearances—Measure the piston ring side clearances prior to removal of the rings to determine the level of deposit formation (see Annex A10). Align ring gaps to the EOT ring gap marks on the top of the piston. Do not force the feeler gages between the ring and groove to disturb or remove the deposits.
- 11.7.2 Piston Ratings—Immerse the piston assembly in Stoddard solvent and air-dry it prior to any rating. Process and measure the piston deposits according to the Modified CRC Diesel Piston Rating Method described in CRC Manual No. 18 modified by the directions listed in Annex A13. Rate only two levels of carbon (heavy and light) on the second groove and all lands, and only one level of carbon (light) for the under-crown and cooling groove. Use a combined varnish rating method for the third groove, third land, fourth land, under-crown, and cooling groove (see Annex A13). An example rating worksheet is shown in Appendix X1. Another heavy-duty engine deposit rater shall verify all piston deposit ratings done by the testing laboratory. In special cases where another rater is not available, the rating may be verified by other qualified laboratory personnel. Record the initials of both the rater and the verifying rater.
- 11.7.2.1 *Referee Ratings*—The referee laboratory rates the entire piston. Wrap all pistons to be referee-rated in paper with CRC desiccant chips. Then place them in plastic and seal

before shipping to the referee laboratory. Report referee ratings to the TMC within ten days of EOT for calibration tests. Referee-rate piston deposits for all non-reference tests reviewed by Caterpillar.

11.7.3 *Ring End Gap Increase*—Remove all carbon from the rings. If scraping of the rings is necessary, use only a wooden instrument or equivalent. Measure and record the ring end gaps.

11.7.4 Cylinder Liner Wear—Use a surface profile measurement to determine the liner wear step in both transverse and longitudinal directions relative to the crankshaft. Remove deposits on the liner above the piston ring travel. Take transverse and longitudinal measurements at the wear step location approximately 13 mm from the top of the liner at four locations. Record the measurements as the liner wear step.

11.7.5 Cylinder Liner Bore Polish—Section the cylinder liner through the front and rear axis and measure the cylinder liner to determine the amount of bore polishing. Use the liner rating method listed in Annex A13.

11.7.6 *Photographs*—Photograph the piston and rings showing the thrust, anti-thrust, front, rear, and undercrown positions (see Appendix X1). Place the rings on top of the piston to show ring gaps (thrust view) and 180° from gaps (anti-thrust view). Show the piston from the crown down to at least the bottom of the pin bore. Photograph the piston crown and skirt as one assembly. Photograph the bore ID of the sectioned liner (see Appendix X1).

12. Calculation or Interpretation of Results

12.1 Test Validity—If a test was run for 360 h according to this test method, declare the test valid. If a test was not run as specified by this test method, then the test is operationally invalid. Some examples of an invalid test are: use of nonspecified hardware, non-specified assembly methods, a test run whose downtime is greater than 125 h, a test that has a Quality Index value for a controlled parameter below the threshold of zero (see DACA II Report),³¹ and so forth. If a test has greater than four consecutive hours without data acquisition on any controlled parameter, the test will be considered operationally invalid. If a test completes 360 h and the piston, rings, or liner exhibit distress, then consider the test to be non-interpretable. Likewise, if the test is terminated *prior* to completing 360 h for reasons including purchaser request, excessive oil consumption, or piston, ring, or liner distress, then consider the test non-interpretable.

12.2 *Calculations*—Use the same set of data for all calculations and graphs in the test report.

12.2.1 *Quality Index*—Calculate and plot the Quality Index according to the instructions in Annex A2.

12.2.2 *Oil Consumption*—Calculate oil consumption in g/h over 24 h intervals. Delete the first 4 h of readings after an oil add from the linear regression. The linear regression technique is shown in Figs. A6.5 and A6.6. Calculate the overall average oil consumption, the initial average oil consumption, and end-of-test (EOT) average oil consumption. The initial average

is the average of the 24th and 48th h data points from the oil consumption graph. The EOT average is the average of the 336th and 360th h data points for a full length test, or for a short-term test it is the average of the last two data points from the oil consumption graph. Calculate the natural logarithmic transformation of the average and EOT oil consumption values using the following equations:

transformed average oil consumption = ln(average oil consumption)

transformed EOT oil consumption = ln(EOT oil consumption) (3)

12.2.3 For a 24-h period including a shutdown, calculate the oil consumption as follows:

12.2.3.1 Do not include the first 4-h oil weight readings after a shutdown in the linear regression.

12.2.3.2 Calculate the linear regression for the period before the shutdown.

12.2.3.3 Calculate the linear regression for the period after the shutdown.

12.2.3.4 Calculate a time weighted average from both regressions to obtain the oil consumption for that 24–h period. For example, a test experiences a 7-h shutdown at test hour 12. The slope for the first 8-h period (hour 4 to 12) is 10.7 g/h, and the slope for the second 8-h period (hour 16 to 24) is 2.1 g/h. The weighted average is calculated as follows:

weighted average =
$$\frac{(10.7g/h)(8h) + (2.1g/h)(8h)}{8h + 8h}$$
 (4)

13. Report

13.1 Forms and Data Dictionary—Refer to Annex A15 and Annex A16 for the forms and data dictionary used by this test method. Test report forms should closely resemble those listed in Annex A15. Report values for all the field names listed in the report forms. Some fields may be blank for short-term tests. Report all deposits, wear, and engine operational data as shown in the test report. The data dictionary defines the field lengths, decimal size, data type, units and format for the field names listed in the test report forms.

13.2 Test Validity—Document on the first sheet of the test report in Annex A15 whether the test is Valid, Invalid, or Non-interpretable. For a valid stand calibration run, report the test data to TMC who will include the test data in the operationally valid database and determine statistical validity using the LTMS method.³² For an invalid or non-interpretable stand calibration run, report the test data to TMC with comments describing why the test is considered invalid or non-interpretable. TMC will not include the test data in the operationally valid database. All operationally invalid and non-interpretable calibration tests are reported by the TMC to the ASTM Single Cylinder Diesel Surveillance Panel in periodic testing summaries. For a valid CMA Registered Oil Test, report the data to Registration Systems, Inc. (RSI).³³ For

³¹ Available from ASTM Test Monitoring Ctr., 6555 Penn Ave., Pittsburgh, PA 15206-4489.

³² The LTMS method tracks the severity and precision of stand and laboratory test results. For a complete definition, refer to the LTMS manual which is available from ASTM Test Monitoring Center, 6555 Penn Avenue, Pittsburgh, PA 15206-4489.

³³ Registration Systems, Inc., CMA Monitoring Agency, 4139 Gardendale, Suite 205, San Antonio, TX 78229.

an *invalid or non-interpretable CMA Registered Oil Test*, report the test data to RSI with supporting comments describing why the test is considered invalid or non-interpretable. When non-calibration oil tests are presented to Caterpillar for review, include the data from all tests that were registered with RSI as part of the program.

13.3 Report Specifics:

13.3.1 If more than one fuel batch is used, report the fuel batch analysis that is most representative of the fuel in the tank.

13.3.2 Report any causes for any missing or bad test data in the comment section of Form 7. If any alternative data acquisition method is used, document it in the comment section of Form 7.

13.3.3 If a calibration period is extended beyond the normal nine-month period, make a note in the comment section of Form 7 and attach a written confirmation from the TMC to the test report. List the outcomes of previous calibration runs in the comment section of Form 7.

13.3.4 Include the fuel analysis provided by the fuel supplier as Form 14. For calibration tests, include a copy of the TMC control chart analysis as Form 17. It is recommended that test purchasers include the form shown in Fig. X1.8 as Form 18 when presenting the test results against specification limits, such as those in Specification D 4485 or military specifications.

14. Precision and Bias

14.1 *Precision*—Test precision is established on the basis of operationally valid reference oil test results monitored by the

ASTM Test Monitoring Center. Table 1 summarizes reference oil precision and reproducibility of the test as of February 13, 2001.

14.1.1 *Intermediate Precision (IP)*—The difference between two results obtained by the same operator or laboratory using the same test method on the same oil would, in the long run, in the normal and correct conduct of the test method, exceed the values shown in Table 1 in only one case in twenty.

14.1.2 Reproducibility (R)—The difference between two single and independent results obtained by different operators working in different laboratories on the same oil would, in the long run, in the normal and correct conduct of the test method, exceed the values shown in Table 1 in only one case in twenty.

14.2 *Bias*—Bias is determined by applying an accepted statistical technique to reference oil test results, and when a significant bias is determined, a severity adjustment is permitted for non-reference oil test results. Currently, there are two types of severity adjustments - Industry and Laboratory. There are no test stand severity adjustments. Industry severity adjustments are determined by the Single Cylinder Surveillance Panel under ASTM Committee D02, Subcommittee B. Laboratory severity adjustments are determined by the instructions listed in the Lubricant Test Monitoring System (LTMS) document.³¹

15. Keywords

15.1 caterpillar 1P test procedure; oil consumption; piston deposits; single cylinder oil test

TABLE 1 Reference Oil Test Precision

Note-Legend:

 S_{ip} = standard deviation for intermediate precision

 $I\dot{P}$ = intermediate precision

 S_r = standard deviation for reproducibility

R = reproducibility

| Test Parameter | S_{ip} | IP | S_r | R |
|--|----------|--------|--------|--------|
| WDP (weighted demerits for the 1P test method) | 46.06 | 128.97 | 49.79 | 139.41 |
| TGC (top groove carbon piston deposits) | 8.15 | 22.82 | 8.15 | 22.82 |
| TLC (top land carbon piston deposits) | 10.06 | 28.17 | 10.07 | 28.17 |
| LN(AOC) (natural log of the average oil consumption) | 0.2633 | 0.7372 | 0.2994 | 0.8383 |
| LN(FOC) (natural log of the final oil consumption) | 0.4816 | 1.3485 | 0.4816 | 1.3485 |

ANNEXES

(Mandatory Information)

A1. ENGINE AND PARTS WARRANTY

- A1.1 Engine Warranty—Caterpillar Inc. warrants single cylinder test engines sold by it to be free from defects in material and workmanship for a period of 12 months starting from the date of delivery to the first user. If a defect in material or workmanship is found during the warranty period, Caterpillar will provide the replacement parts to be installed by the user. There will be no charge to the user for parts furnished by Caterpillar. User at its own expense, shall return all defective parts to Caterpillar at Caterpillar's request. User will be responsible for giving Caterpillar timely notice of a warranty failure. User will also be responsible for labor costs and any applicable local taxes. Caterpillar is not responsible for failures resulting from abuse, neglect, and/or improper repair. THIS WARRANTY IS EXPRESSLY IN LIEU OF ANY OTHER WARRANTIES, EXPRESSED OR IMPLIED, INCLUDING ANY WARRANTY OF MERCHANTABILITY OR FITNESS FOR PARTICULAR PURPOSE. REMEDIES UNDER THIS WARRANTY ARE LIMITED TO THE PROVISION OF PARTS AS SPECIFIED HEREIN. CATERPILLAR IS NOT RESPONSIBLE FOR INCIDENTAL OR CONSEQUENTIAL DAMAGES.
- A1.2 Engine Parts Warranty—All parts for the 1Y3700 engine which are nonconforming by reason of faulty manufacture should be discussed with Engine System Technology Development (ESTD).
- A1.2.1 The test laboratories should contact ESTD (R.A. Riviere, Telephone: 309-636-5247, Fax: 309-675-1598) when they believe a part is nonconforming:

- A1.2.2 ESTD will determine if they want the part returned, or provide warranty without viewing the part.
- A1.2.3 If ESTD determines that the part is nonconforming without viewing the part, the test laboratories will be asked to return the part to their Caterpillar dealer. ESTD will contact the Dealer and let them know the part is coming and to provide warranty for it.
- A1.2.4 If ESTD wants to view the part, they will issue a Return Goods Authorization No. (RGA) to the test laboratory. The laboratory will fill out the form shown in Annex A9 and send the part and the form to Caterpillar Inc., Tech Center TC-L, Wing 4 - Rm 406, 14009 Old Galena Rd., Mossville, IL 61552, Att: A.C. Hahn.
- A1.2.5 The test laboratories should fax a copy of the RGA claim form to Caterpillar Inc., Tech Services Div., Tech Center Bldg L, Fax: 309-578-4232, Att: A.C. Hahn.
- A1.2.6 If ESTD determines that the part is nonconforming, they will contact the dealer for the test laboratory and have the dealer provide warranty.
- A1.2.7 A sample of the RGA claim form is shown in Annex A9 and should include: return goods authorization no., part name, hours on the part, part no., quantity, engine serial no., date purchased, test laboratory that purchased the part and contact person's name, phone, fax, and address, dealer's name that sold the part, measurements or photographs, or both, to document the nonconformance.

A2. INSTRUMENT LOCATIONS, MEASUREMENTS, AND CALCULATIONS

- A2.1 Tables A2.1-A2.6 and Figs. A2.1-A2.5 provide detailed information.
 - A2.2 Requirements for the Quality Index Calculation:
- A2.2.1 Round the recorded values in accordance with the specifications listed in Table A2.5.
- A2.2.2 Use the values listed in Table A2.6 for all calculations.
 - A2.2.3 Use 6-min data to calculate the Quality Index.
- A2.2.4 Reset data that is greater than the high values listed in Table A2.6 from the Over and Under Range Values column to the high value for that particular parameter.
- A2.2.5 Reset data that is less than the low values listed in Table A2.6 from the Over and Under Range Values column to the low value for that particular parameter.
 - A2.2.6 Round the Quality Index values to the nearest 0.001.

- A2.2.7 Report Quality Index values on Form 2 of the test report.
- Note A2.1—Refer to the DACA II Final Report for calculating the Quality Index involving the loss of test data or bad quality test data.
 - A2.3 Formula to calculate the Quality Index:

$$QI = 1 - \frac{1}{n} \sum \left(\frac{U + L - 2X_i}{U - L} \right)^2$$
 (A2.1)

where:

 X_i = recorded test measurement parameter, U = upper specification for that parameter,L = lower specification for that parameter, and

= total number of data points taken as determined from test length and procedural specified sampling rate.

TABLE A2.1 Instrument Locations

| Parameter | Data Acquisition and Control | Engine Computer Sensors | Facility Feedback Control (if separate sensor is required) |
|--|------------------------------|----------------------------|--|
| Cam speed and timing sensor | | A | |
| Crankshaft speed and timing sensor | | В | (at dyno) |
| Coolant pressure to jug | 1 | | |
| Coolant temperature to jug | 2 | | |
| Oil temperature to cooler | 3 | | |
| Atmospheric pressure | | С | |
| Crankcase pressure | 4 | D | |
| Facility air pressure to cooling tower | 5 | | |
| Oil manifold temperature | 6 | E | 6 or W |
| Oil sampling valve | 7 | | |
| Oil manifold pressure | 8 | F | |
| Coolant temperature from engine | 9 | Н | 9 or X |
| Coolant pressure from engine | | G | |
| Coolant flow barco delta pressure | 10 | | |
| Air inlet manifold pressure | (at barrel) | I | (at barrel) |
| Air inlet manifold temperature | 11 | | 11 or Y |
| Fuel temperature from filter | Z | | 12 |
| Fuel pressure from head | 13 | | |
| Fuel flow rate | (at micro motion) | | (at micro motion) |
| Exhaust manifold temperature | 14 | J | |
| Exhaust manifold pressure | (at barrel) | | (at barrel) |
| Humidity | (at barrel) | | (at barrel) |
| Air flow rate | (at meter) | | |
| Blowby flow rate | (at meter) | | |

TABLE A2.2 Thermocouple Diameters, Lengths and Immersion Depths

| Location | Diameter, in. | Length, in., max | Depth, \pm 3 mm |
|----------------------|----------------|------------------|-------------------|
| Oil to manifold | not applicable | 6 | 22 |
| Oil to cooler | not applicable | 6 | 27 |
| External heating oil | not applicable | 6 | 27 |
| Coolant in | not applicable | 6 | 40 |
| Coolant out | not applicable | 6 | 26 |
| Inlet air | not applicable | 6 | 57 |
| Exhaust | not applicable | 6 | 67 |
| Fuel | not applicable | 6 | 34 |
| | | | |

TABLE A2.3 Calibration Tolerances

| Parameters | Tolerance |
|----------------------|---|
| Load | not applicable due to differences within the industry; TMC will verify each laboratory it visits |
| Fuel flow rate | 0.4 g/min |
| Air flow rate | ±2 % of reading from 10-100 % of calibrated range; |
| | ±0.5 % of FS below 10 % of calibrated range |
| Humidity | listed in this test method |
| Temperatures | °C |
| Fuel at filter | 0.5 |
| Coolant to jug | 0.25 |
| Coolant from engine | 0.25 |
| Oil to cooler | 0.5 |
| Oil manifold | 0.5 |
| External heating oil | 0.5 |
| Air inlet manifold | 0.5 |
| Exhaust manifold | 1.0 |
| Pressures | kPa |
| Fuel from head | 0.7 |
| Oil manifold | 0.7 |
| Air inlet | 0.3 |
| Exhaust | 0.3 |
| Crankcase | 0.02 |

TABLE A2.4 Maximum Allowable System Time Constants

| Measurements | Time, s |
|----------------------|---------|
| Speed | 3.0 |
| Fuel flow rate | 20.0 |
| Air flow rate | 3.0 |
| Oil weight | TBD |
| Temperatures | |
| Fuel at filter | 3.0 |
| Coolant to jug | 3.0 |
| Coolant from engine | 3.0 |
| Oil to cooler | 3.0 |
| Oil manifold | 3.0 |
| External heating oil | 3.0 |
| Air inlet manifold | 3.0 |
| Exhaust manifold | 3.0 |
| Pressures | |
| Fuel from head | 3.0 |
| Oil manifold | 3.0 |
| Air inlet | 3.0 |
| Exhaust | 3.0 |
| Crankcase | 3.0 |

TABLE A2.5 Measurement and Reporting Resolutions

| Parameter | Units | Tol | Specification | Minimum Measurement Resolution | Round Values to the Nearest Whole Number |
|------------------------|-------|---------------|---------------|-----------------------------------|---|
| Speed | RPM | ±3 | 1800 | 1 | whole number |
| Power | kW | approximately | 55 | 0.1 | tenth |
| Torque | N⋅m | approximately | 285 | 0.1 | tenth |
| Fuel rate | g/min | ±1 | 185 | 0.1 | tenth |
| Fuel timing | BTC | | 13 | | |
| Humidity | g/kg | ±1.7 | 17.8 | 0.1 | tenth |
| Oil weight | g | | | 2 | whole number |
| Temperatures °C | Č | | | | |
| Fuel into head | | ±3 | 42 | 0.1 | tenth |
| Coolant into jug | | approximately | 86 | 0.1 | tenth |
| Coolant from head | | ±3 | 90 | 0.1 | tenth |
| Oil to cooler | | approximately | 128 | 0.1 | tenth |
| Oil manifold | | ±3 | 130 | 0.1 | tenth |
| External heating oil | | | 165 max | 0.1 | tenth |
| Inlet air manifold | | ±3 | 60 | 0.1 | tenth |
| Exhaust manifold | | approximately | 480 | 1 | whole number |
| Pressures kPa | | | | | |
| Fuel from head | | ±20 | 275 | 1 | whole number |
| Coolant into jug | | approximately | 81 | 1 | whole number |
| Oil manifold | | ±20 | 415 | 1 | whole number |
| Inlet air barrel (abs) | | ±1 | 272 | 0.1 | tenth |
| Exhaust barrel (abs) | | ±1 | 265 | 0.1 | tenth |
| Crankcase | | approximately | 0.10 | 0.01 | hundredth |
| Flows | | | | | |
| Coolant | L/min | ±2 | 75 | 0.1 | tenth |
| Blowby | L/min | approximately | 35 | 1 | whole number |
| Air | kg/h | approximately | 315 | 0.1 | tenth |

TABLE A2.6 Quality Index Calculation Values and Plotting Axis Scale Definitions

| | | Quality Index U and L Values ^A Over and Under Range Values | | r Range Values ^B | | C | | |
|--------------------------|-------|---|----------|-----------------------------|------|------|------|-----------|
| Controlled Parameters | units | L | U | low | high | min | max | increment |
| Speed | r/min | 1798.530 | 1801.470 | 1710 | 1890 | 1770 | 1830 | 10 |
| Fuel flow | g/min | 183.970 | 186.030 | 125 | 245 | 175 | 200 | 5 |
| Humidity | g/kg | 16.780 | 18.820 | 5 | 21 | 5 | 40 | 5 |
| Coolant flow | L/min | 73.060 | 76.940 | 0 | 82 | 60 | 90 | 5 |
| Coolant out | °C | 89.379 | 90.622 | 55 | 125 | 70 | 110 | 5 |
| temperature | | | | | | | | |
| Oil to Manifold | °C | 128.798 | 131.202 | 60 | 200 | 120 | 150 | 5 |
| Temperature | | | | | | | | |
| Inlet air | °C | 59.360 | 60.640 | 20 | 100 | 50 | 70 | 5 |
| temperature | | | | | | | | |
| Fuel into head | °C | 40.885 | 43.116 | 0 | 75 | 30 | 60 | 5 |
| temperature | | | | | | | | |
| Oil to manifold | kPa | 404.384 | 425.616 | 0 | 690 | 380 | 450 | 10 |
| pressure | | | | | | | | |
| Inlet air pressure | kPa | 271.449 | 272.551 | 242 | 302 | 265 | 280 | 5 |
| Exhaust pressure | kPa | 264.150 | 265.850 | 215 | 315 | 250 | 280 | 5 |
| Fuel pressure | kPa | 271.471 | 278.529 | 125 | 425 | 230 | 300 | 10 |
| Uncontrolled Parame | ters | | | | | | | |
| Power | kW | | | | | 50 | 60 | 1 |
| Torque | N⋅m | | | | | 230 | 310 | 10 |
| Blowby | L/min | | | | | 5 | 65 | 5 |
| Coolant in | °C | | | | | 75 | 100 | 5 |
| temperature | | | | | | | | |
| Coolant delta | °C | | | | | 0 | 10 | 1 |
| Oil cooler in | °C | | | | | 120 | 140 | 5 |
| temperature | | | | | | | | |
| Heating oil | °C | | | | | 120 | 165 | 5 |
| temperature | | | | | | | | |
| - Exhaust | °C | | | | | 450 | 500 | 10 |
| temperature | | | | | | | | |
| Crankcase | kPa | | | | | 0.0 | 1.5 | 0.1 |
| pressure | | | | | | | | |
| Coolant pressure | kPa | | | | | 60 | 95 | 5 |

^A The threshold for operational validity is 0.00.

^B Only to be used in the calculation of Quality Index and Average and does not affect how process is graphed.

^C Quality Index Scales are to range from -0.3 to 1.0 with increments of 0.1. The axis for test time is 0 to 360 h in 30-h increments. X-axis length should be at least 8.0 in. Y-axis length should be at least 5.5 in.

∰ D 6681 – 01

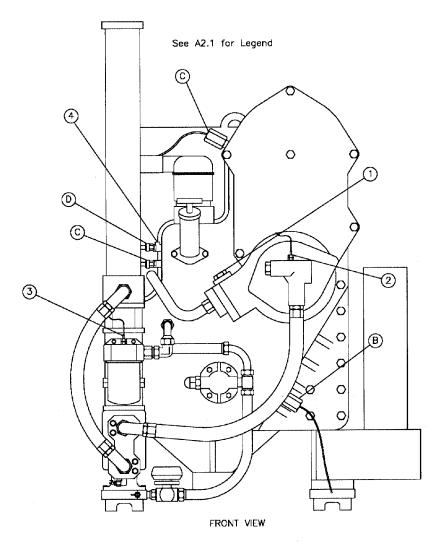


FIG. A2.1 Instrument Locations—Engine Front View

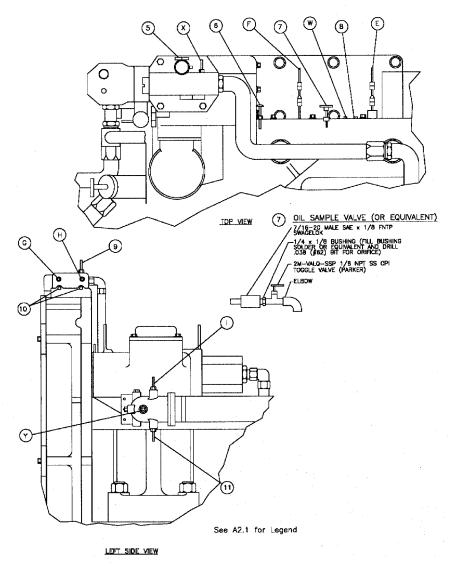
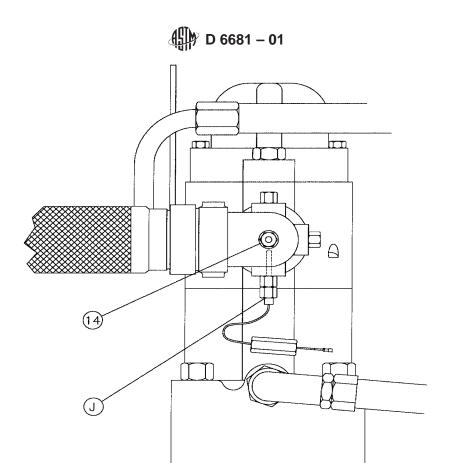
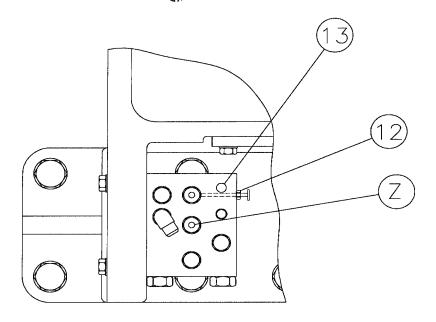


FIG. A2.2 Instrument Locations—Top and Left Engine Views



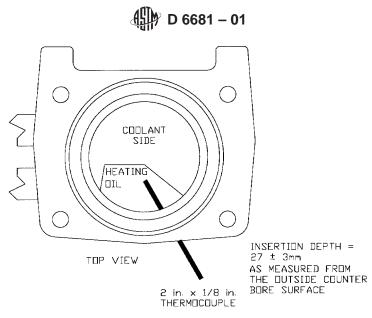
RIGHT SIDE VIEW
See A2.1 for Legend

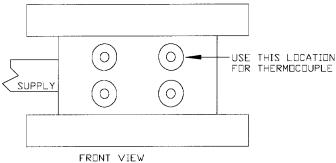
FIG. A2.3 Instrument Locations—Right Engine View



TOP VIEW
See A2.1 for Legend

FIG. A2.4 Instrument Locations—Top Engine View





Note—Turn oil filter block drain valve 180° so that it is facing out and easier to use.

FIG. A2.5 Engine Heating Oil Thermocouple Location

A3. COOLING SYSTEM ARRANGEMENT

- A3.1 Install a sight glass as shown using the following components listed in Table A3.1.
- A3.1.1 Reuse one of the straight 37° flare swivel hose fittings on the existing hose for the tower side of assembly. The 90° fitting in the cylinder head is also still used. Installation angle will be slightly different.
- A3.2 Cleaning Procedure for the Engine Coolant System—Clean the coolant system when visual inspections show the presence of any oil, grease, mineral deposits, or rust. The engine cooling system arrangement is shown in Fig. A3.1.
- A3.2.1 To remove oil and grease from the cooling system:
- A3.2.1.1 Operate the engine until oil and water operating temperatures are attained; shutdown the engine and drain the cooling system.
- A3.2.1.2 Fill the cooling system with a solution of 454 g of trisodium phosphate (Na₃PO₄) to 38 L of water; operate the engine for 5 min to ensure complete mixing of the solution with any material remaining from the previous fill.
- A3.2.1.3 Shutdown the engine and drain and flush the engine with fresh water and drain the water from the system.

TABLE A3.1 Coolant Sight Glass Components

| Item | Quantity | Part No. | Source | Description | Location |
|------|----------|-----------------------|-------------------|--|-----------------------------------|
| 1 | 1 | 2061-20-20S | Aeroquip | 45° SAE O-ring port to 37° flare | inlet to top of coolant tower |
| 2 | 1 | 190265-20S | Aeroquip | 45° Elbow – SAE O-ring to 37° flore swivel | head outlet |
| 3 | 2 | 412-16-20S | Aeroquip | Male pipe re-usable fitting | inlet and outlet of sight glass |
| 4 | 1 | 4288 1 in. NPT Female | Gits ^A | style OL flow gage (sight glass) | locate in middle of hose assembly |
| 5 | 1 | FC350-20 | Aeroquip | hose ~ 51/2 in. | head side of assembly |
| 6 | 1 | FC350-20 | Aeroquip | hose ~ 6½ in. | tower side of assembly |

^A Gits Manufacturing Co.

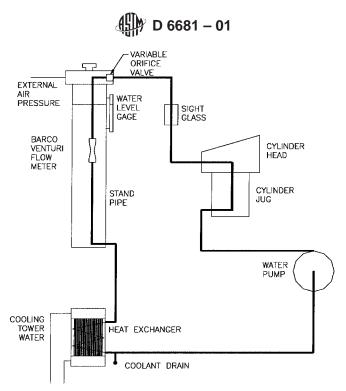
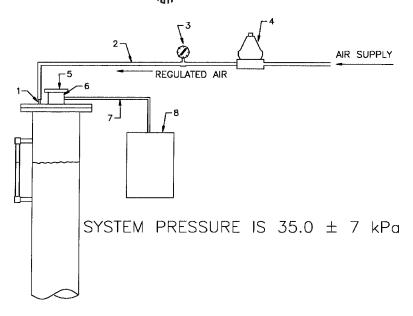


FIG. A3.1 Engine Cooling System Arrangement

- A3.2.2 To remove mineral deposits from the cooling system:
- A3.2.2.1 Operate the engine until oil and water operating temperatures are attained; shutdown the engine and drain the cooling system.
- A3.2.2.2 Fill the cooling system with a solution of 454 g of commercial sodium bisulfate (NaHSO₄) to 19 L of water; then run the engine at operating temperatures for 30 min.
- A3.2.2.3 Shutdown the engine, drain and flush the engine with fresh water and drain the water from the system.
- A3.2.2.4 Fill the cooling system with a solution of 454 g of trisodium phosphate (Na₃PO₄) to 38 L of water; operate the

- engine for 5 min to ensure complete mixing of the solution with any material remaining from the previous flush.
- A3.2.2.5 Shutdown the engine and drain the engine, flush with clear water and drain after flushing.
- A3.2.2.6 Disassemble the engine and prepare for the next test.
- A3.2.3 If the cooling system is contaminated by oil and mineral deposits, remove the oil from the system, then remove the mineral deposits. Alternatively, the cylinder head coolant passages may be cleaned after the head is removed.
- A3.2.4 The coolant pressurization system is shown in Fig. A3.2 and the cooling tower water circuit is shown in Fig. A3.3.

∰ D 6681 – 01



Note-Legend:

- 1. 1/4 in. NPT-to-No.4AN (male connector)
- 2. No. 4 hose
- 3. Pressure gage 0-15 psig
- 4. Pressure regulator (self bleeding)
- 5. Radiator cap 15-16 psig
- 6. Radiator filler neck
- 7. Overflow tube (optional)
- 8. Overflow tank (optional)

FIG. A3.2 Coolant Pressurization System

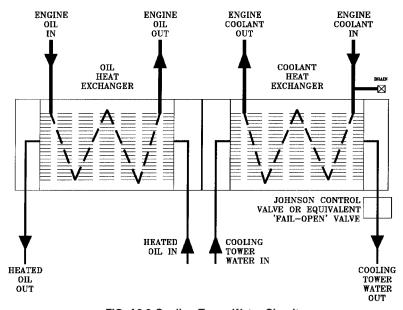
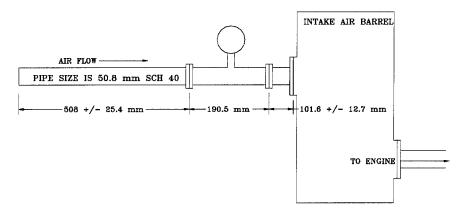


FIG. A3.3 Cooling Tower Water Circuit

A4. INTAKE AIR MASS FLOW SENSOR INSTALLATION

A4.1 The intake air sensor installation is shown in Fig. A4.1.



Note-Meter: Model 780 in-line mass flow meter by Sierra Instruments;

Accuracy: ±2 %;

Part No.: 780-F6-CG-(other options).

FIG. A4.1 Intake Air Sensor Installation

A5. FUEL SYSTEM DESIGN AND REQUIRED COMPONENTS

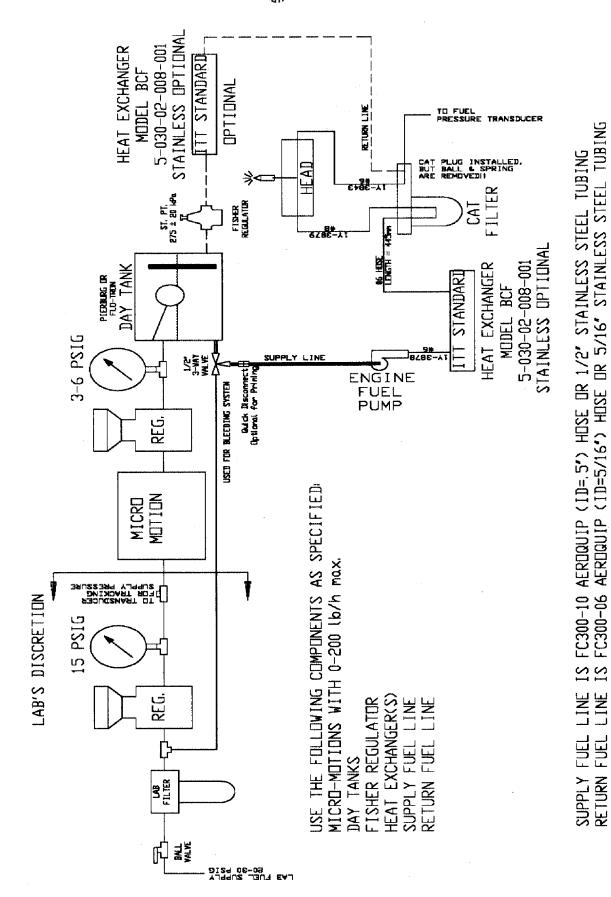


FIG. A5.1 Fuel System Design and Required Components

∰ D 6681 – 01

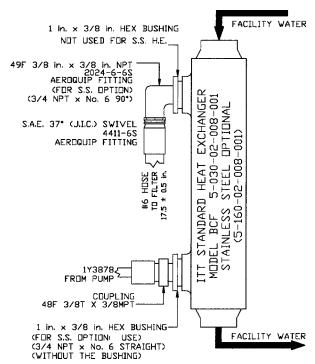


FIG. A5.2 Fuel Heat Exchanger Plumbing Connections

TABLE A5.1 Fisher Regulator Information

| Type | Pressure | Inlet, | Spring | Trim | Allowable Inlet |
|------|----------|--------|--------|----------|-----------------|
| 98 | Units | max | Range | Material | Pressure, max |
| H-17 | PSIG | 75 | 22-75 | SST | 250 |

A6. OIL SYSTEM

- A6.1 *Verification of Oil Scale Pump Flows*—Verify the oil scale pump flow rates with EF-411 at $26.5 \pm 5.5^{\circ}$ C as the test fluid using the following procedure. The following equipment is needed.
 - A6.1.1 One stopwatch.
 - A6.1.2 One to 2 gal of EF411 oil at 26.5 ± 5.5 °C.
 - A6.1.3 One temporary reservoir pan.
 - A6.1.4 One temporary discharge pan.
 - A6.2 Procedure for Flow from Oil Pan to Oil Scale:
- A6.2.1 Disconnect the line from the oil pan and place in temporary reservoir pan.
- A6.2.2 Disconnect the line from the oil scale and place in the temporary discharge pan.
- A6.2.3 The height of the pump relative to the reservoir and discharge pans shall be within 3 ft to reduce any head pressure differences, which may affect the flow rates.
- A6.2.4 Prime the system (both hoses and pump), then shutdown.
 - A6.2.5 Empty the discharge pan and record the weight of it.

- A6.2.6 Turn the system on and start the stop watch at the same time.
 - A6.2.7 Let the system run for 4 min and then stop it.
- A6.2.8 Weigh the oil in the discharge pan, subtracting the empty weight.
 - A6.2.9 Determine the flow rate.
 - A6.3 Procedure for Flow from the Oil Scale to the Oil Pan:
- A6.3.1 Repeat the above procedure by disconnecting the line from the oil scale and placing it in the temporary reservoir pan and disconnecting the line at the oil pan and placing it in the temporary discharge pan.
 - A6.3.2 The following materials are needed.
- A6.3.2.1 *Steel Tubing*, ½ in. OD, ¾ in. ID, approximately 1 in. long.
- A6.3.2.2 Adapter Fitting, ½ in. NPT to desired connection type (Fig. A6.4 shows an Aeroquip No. 2000-4-4B for a #4, 45° flare).
 - A6.3.2.3 Silver Solder.
 - A6.3.3 Procedure:

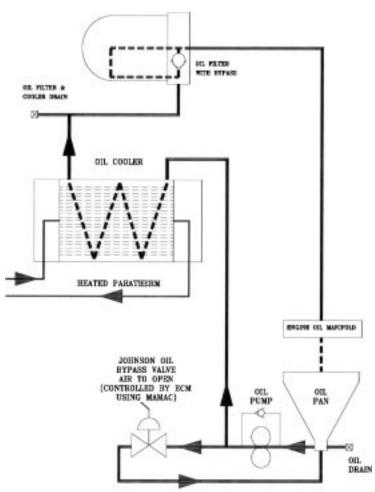


FIG. A6.1 Oil System

A6.3.3.1 Drill adapter fitting on pipe thread end to ½ in. nominal diameter, ½ in. min depth.

A6.3.3.2 Insert tube into fitting until bottomed out in the $\frac{1}{4}$ in. hole.

A6.3.3.3 Silver solder the tube-to-fitting joint.

A6.3.3.4 Remove oil pan from engine and install the fitting in location specified.

A6.3.3.5 Mark the tube location to achieve 5 \pm 1 mm protrusion into the oil pan.

A6.3.3.6 Remove the fitting and cut to length.

A6.3.3.7 Re-install fitting in pan, check protrusion, and re-install oil pan on engine.

A6.4 Oil Consumption Linear Regression Method—If there is good reason to assume that a variable *Y* is dependent upon another variable *X* and that the relationship is linear, the best-fit line describing this relationship can be plotted using the following equations. Also see Figs. A6.5 and A6.6.

$$m = \frac{\sum x_i y_i - \frac{\sum x_i \sum y_i}{n}}{\sum x_i^2 - \frac{(\sum x_i)^2}{n}}$$
(A6.1)

$$b = \left[\frac{\sum y_i}{n} - m \frac{\sum x_i}{n}\right] \tag{A6.2}$$

$$r^{2} = \frac{\left[\sum x_{i}y_{i} - \frac{\sum x_{i} \sum y_{i}}{n}\right]^{2}}{\left[\sum (x_{i})^{2} - \frac{(\sum x_{i})^{2}}{n}\right]\left[\sum (y_{i})^{2} - \frac{(\sum y_{i})^{2}}{n}\right]}$$
(A6.3)

where:

 y_i = oil weights taken at time x,

 x_i = times at which oil weight observation x are made,

m = slope of best-fit line = oil consumption,

b = y intercept, and

 r^2 = goodness of fit (1 if perfect, 0 if not fit at all).

A6.5 Oil Sampling Procedure:

A6.5.1 Record oil scale reading at test hour four _____ g. This is the *Full Mark*.

A6.5.2 Record the *oil weight* from the 24th hourly reading _____ g.

A6.5.3 Remove 250 mL purge sample from sample valve on the oil manifold.

$$\frac{g}{purge + container} - \frac{g}{container} = \frac{g}{purge}$$

A6.5.4 For test hours 24, 96, 240, 288 and 360, remove a 90 mL sample from the sample valve on the oil manifold.

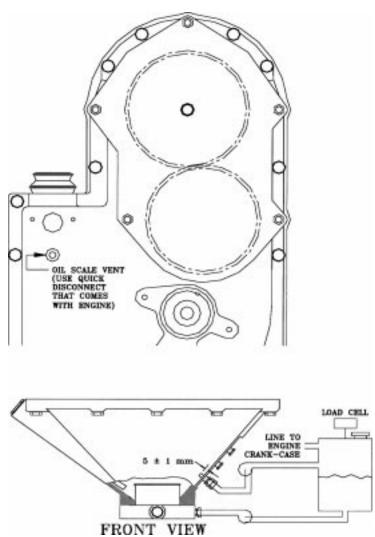


FIG. A6.2 Oil Scale Measurement System

$$\frac{g}{sample + container} - \frac{g}{container} = \frac{g}{sample}$$

A6.5.4.1 Add 370 \pm 10 g of *NEW test oil* to the oil weigh tank.

$$\frac{1}{new\ oil + container} - \frac{g}{container} = \frac{g}{new\ oil}$$

A6.5.5 For *test hours 48, 72, 120, 144, 168, 192, 216, 264, 312 and 336,* remove a *30 mL sample* from the sample valve on the oil manifold.

$$\frac{g}{sample + container} - \frac{g}{container} = \frac{g}{sample}$$

A6.5.5.1 Add 317 \pm 10 g of *NEW test oil* to the oil weigh tank.

$$\frac{1}{new\ oil + container} - \frac{g}{container} = \frac{g}{new\ oil}$$

A6.5.6 Add back enough purge sample to return the oil weigh tank to its Full Mark using the following formula:

purged to be returned =
$$FM - A$$
 (A6.4)

where:

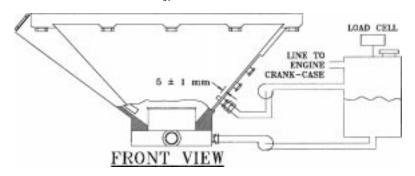
$$A = \frac{1}{\text{#2; 24th Hourly Reading; (Scale Weight)}} - \frac{1}{\text{#3; Purge Weight}} - \frac{1}{\text{#4; Sample Weight; (if taken)}} + \frac{1}{\text{#5; New Oil Weight}}$$

A6.5.7 Record the weight of *unused* purge sample by using scale.

$$\frac{g}{\textit{unused purge} + \textit{container}} - \frac{g}{\textit{container}} = \frac{g}{\textit{unused purge left over}}$$

 $\mbox{Note }A6.1\mbox{---}\mbox{If you are short in returning to the full mark, use fresh oil to make up the difference.}$

∰ D 6681 – 01



Note—(1) Suction Pump and Hose (or equivalent)

Type: Viking C-90 Pump Flow: 6 ± 1.5 g/h Speed: 285 r/min

Hose: 0.25 in. ID TFE-fluorocarbon steel braided 9 ft max length

Pulley: 4.95 in. OD

(2) Return Pump and Hose (or equivalent)

Type: Viking C-92 Pump Flow Differential: 3 ± 1 g/h

Speed: 163 r/min

Hose: 0.25 in. ID TFE-fluorocarbon steel braided 9 ft max length

Pulley: 8 in. OD

(3) Pump Motor (both pumps) (or equivalent)

Type: 56 Nema Grainger 6K949

Speed: 1140 r/min HP: 3/4

Pulley: 1.5 in. OD

(4) Vent Line: 0.25 in. ID hose

(5) Oil in Reservoir: 1000 g (approximately)

(6) Scale Precision: See Procedure

(7) Flexible Hose: (to and from fixed external sump support) (or equivalent): Aeroquip FC352-08

FIG. A6.3 Low Flow Oil Scale System

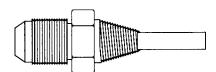


FIG. A6.4 Oil Pan Suction Fitting to Oil Scale

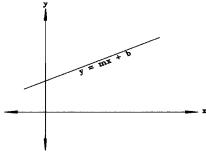


FIG. A6.5 Equation of a Straight Line

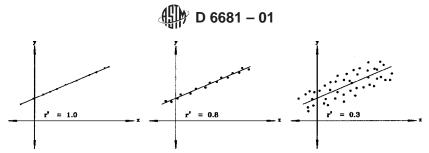
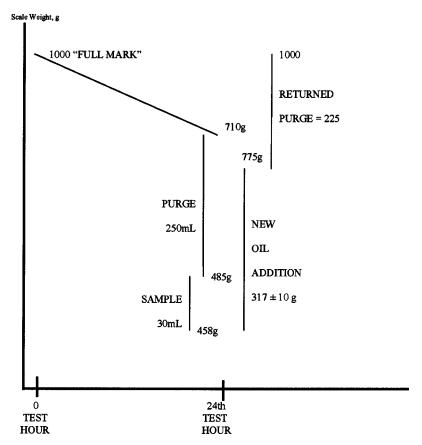
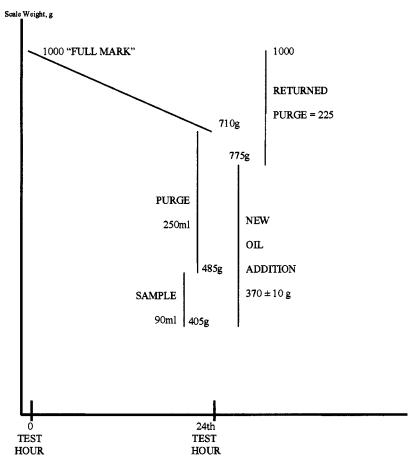


FIG. A6.6 Examples of the Goodness of Fit



Note—Taken at 48, 72, 120, 144, 168, 192, 216, 264, 312, 336 h. FIG. A6.7 Example of Oil Addition Procedure with 30 mL Sample



 $Note — Taken \ at \ NEW, \ 24, \ 96, \ 240, \ 288, \ 360 \ h.$ FIG. A6.8 Example of Oil Addition Procedure with 90mL Sample



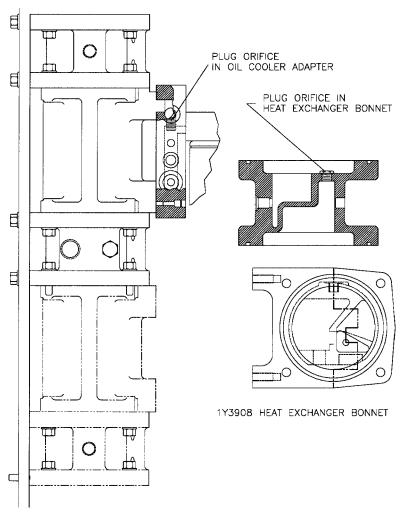


FIG. A6.9 Engine Oil Heating Hardware

A7. EXHAUST AND INTAKE BARREL PIPING

 $A7.1\,$ The exhaust and intake barrel piping are illustrated in Figs. A7.1 and A7.2.

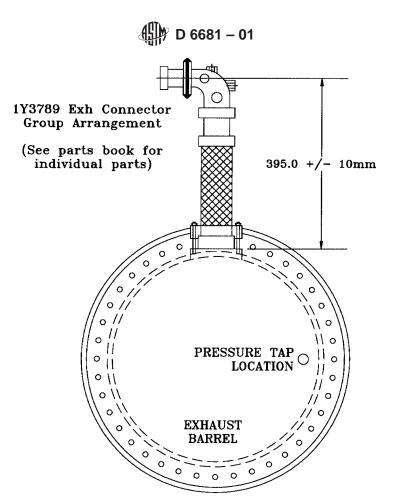
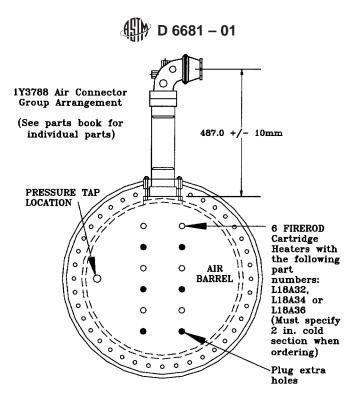


FIG. A7.1 1Y3978 Exhaust Barrel and Piping



Note 1—Dummy heater elements may be substituted for the FIREROD cartridge heaters, as long as they are the same dimension of 21 in. \times 5% in. diameter. The 21 in. is from end-to-end. Length tolerance is 3 in. and the diameter tolerance is $\frac{1}{64}$ in.

Note 2—FIREROD cartridge heaters may be purchased from Southwest Heater and Controls, 12052 Forestgate Dr., Dallas, TX 75243.

FIG. A7.2 1Y3976 Intake Air Barrel and Piping

A8. HUMIDITY PROBE INSTALLATION

A8.1 Figs. A8.1 and A8.2 illustrate the humidity probe installation locations.

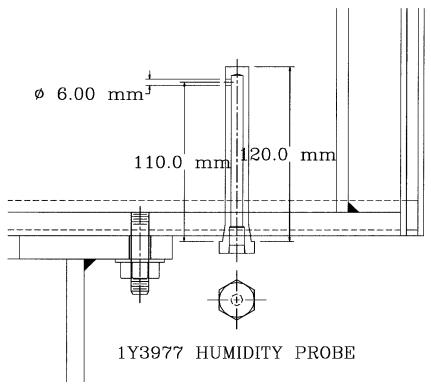


FIG. A8.1 Humidity Probe Installation Location

Bottom of Intake Air Barrel

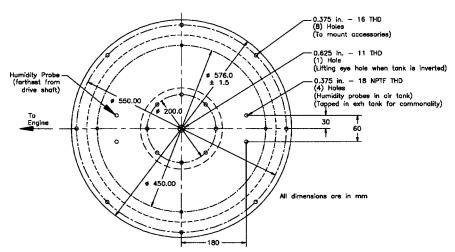


FIG. A8.2 Humidity Probe Installation Location—Barrel Bottom

A9. RETURN GOODS AUTHORIZATION

 $A9.1\;\; Fig.\, A9.1$ is a sample return goods authorization claim form.

| Return Goods Authorization Number: | |
|------------------------------------|---|
| Claim Date: | |
| Contact: | Caterpillar Inc Engine System Tech Dev. P.O. Box 610 Mossville, Il 61552 Phone: 309-636-5247 Fax: 309-675-1598 Attn: R.A. Riviere |
| Part Number / Quantity: | |
| Part Name / Hrs On Part: | |
| Date Part Purchased: | |
| Engine Serial Number: | |
| Test Lab | |
| | Name: |
| | Address: |
| | Contact Person's Name: |
| | Phone Number: |
| | Fax Number: |
| Name of Dealer That Sold Part: | |

INCLUDE DOCUMENTATION AND PHOTOS OF NONCONFORMING PART FIG. A9.1 Sample Return Goods Authorization Claim Form

A10. ENGINE ASSEMBLY INFORMATION

A10.1 1Y3700 Engine Mechanical Timing—Remove the camshaft gear to replace cylinder head components after test and re-time as follows (see Fig. A10.6):

A10.1.1 Rotate the engine to position the piston at TDC.

Note A10.1—The TDC mark on the flywheel will align with the timing pointer. The 6.28 mm diameter 1Y3919 timing pin will insert in the crank gear key-way slot through the timing hole in the front housing near the oil pump flange.

A10.1.2 Pin the camshaft with a second 6.28 mm diameter 1Y3919 timing pin.

A10.1.3 Mesh the camshaft gear with the adjustable idler gear and with the UP mark on the front face of the camshaft gear in the 12:00 o'clock position. Assemble the camshaft gear to the camshaft.

A10.1.4 Set lash between the adjustable idler gear and the camshaft gear and torque the six socket head bolts at the stub-shaft flange.

A10.1.5 Remove both 6.28 mm diameter timing pins.

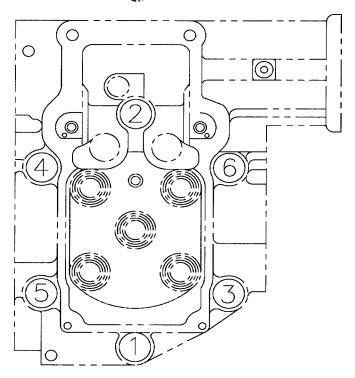
A10.2 1Y3700 Engine Mechanical Timing—General Information:

Note A10.2—This is not part of the normal engine timing procedure.

A10.2.1 This procedure is to be followed only on new engine assembly or in the event that a new timing disk, or crankshaft, or flywheel, or front housing is assembled on an old engine.

A10.2.2 With the crankshaft connecting rod journal at top dead center (TDC), the tooth valley V mark on the crankshaft gear is 35.38° clockwise from the vertical and the key-way is 68.48° clockwise from vertical. With the crankshaft gear fixed, assembly of the cluster idler gear on its stub-shaft causes the cluster idler gear to rotate 2.87° clockwise, so that its dash marked tooth is 145.73° counterclockwise from vertical. The V and dash marks line up valley-to-tooth.

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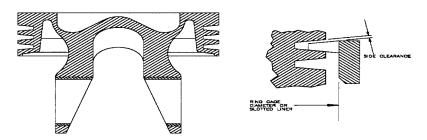


Note 1—(1) Lubricate stud threads and both washer faces with Mobil EF411 engine oil.

- (2) Tighten cylinder head nuts with hand torque wrench:
- (a) Tighten nuts 1 through 6 in numerical sequence to $100 \pm 15 \text{ N} \cdot \text{m}$.
- (b) Tighten nuts 1 through 6 in numerical sequence to 200 \pm 15 N·m.
- (c) Tighten nuts 1 through 6 in numerical sequence to $400 \pm 15 \text{ N} \cdot \text{m}$.

Note 2—Coat valve stems with Mobil EF411 engine oil immediately prior to installation.

FIG. A10.1 Cylinder Head Tightening Procedure



Note—Piston part nos: Skirt 1Y3659, Crown 1Y3400; Rings part nos: Top 1Y3802, Intermediate 1Y3803, Oil 1Y3804.

FIG. A10.2 Piston and Ring Specifications

A10.2.3 Assembly of the adjustable idler gear with its UP mark at the top orients the three kidney-shaped openings in the gear web to allow access to the socket head bolts that attach the adjustable idler gear stub-shaft to the front housing plate.

A10.2.4 Assembly of the camshaft gear with its V mark and UP mark at the top and with the camshaft pinned to the cylinder head, by design, results with the 0.50 in. bolts on-center of the 17 mm diameter clearance holes in the camshaft gear. Additive tolerances for all the involved parts can cause the bolts to be off-center in either direction. The purpose of the oversize holes is to ensure that the gears will mesh at all off-nominal, but in tolerance dimensions of the parts

A10.2.5 With the camshaft and the crankshaft pinned, the engine is necessarily at top dead center on the firing stroke. The

flywheel pointer is at 0° (TDC). The leading edge of a 3° timing notch on the camshaft gear is on the centerline of the cam sensor hole in the front housing. The leading edge of a 6° notch on the crankshaft timing disk is on the centerline of the crankshaft sensor hole in the front housing.

A10.2.6 With the flywheel pointer at 3° after top dead center, a 1Y3918 pin inserted in the crank timing sensor hole in the front housing shall also slide into a 6° wide notch of the crankshaft timing disk. This verifies that the leading edge of a notch on the timing disk is on the centerline of the crankshaft sensor which sets TDC for the electronic control module (ECM).



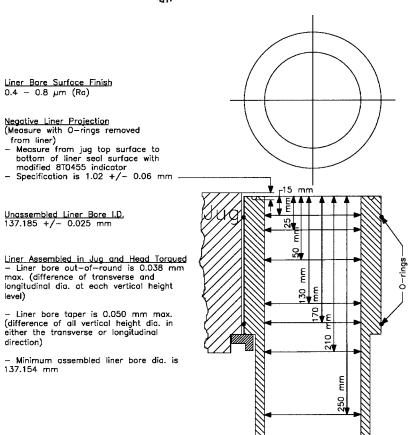
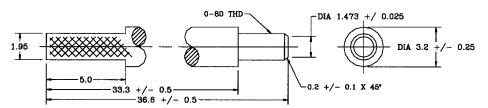


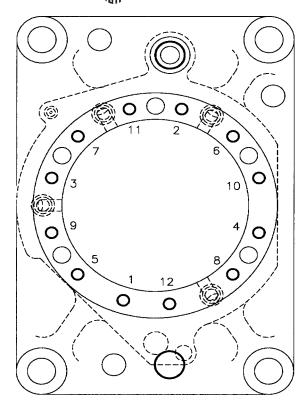
FIG. A10.3 Cylinder Liner Measurements and Specifications



Note 1—Grind the tip to 1.95 \pm 0.02 mm diameter for 5.0 \pm 0.5 mm long from spherical end. All dimensions are in mm.

Note 2—Indicator measures liner recession from the jug deck surface to the bottom of the liner combustion seal groove. The tip of the 8T0455 indicator rod requires modifications as indicated.

FIG. A10.4 Cylinder Liner Projection Measurement Indicator Modifications



Note 1—Center the support ring I.D. to the cylinder liner with four feeler gages of equal thickness, hand tighten the stud nuts, but remove feeler gages before tightening stud nuts.

Note 2—Tighten the stud nuts in numerical order as shown with a sequence level of 15, 55, and 105 \pm 10 N·m.

Note 3—The cylinder liner support ring torque sequence may be used after the cylinder head torque sequence as an alternate method if the liner bore distortion is out of test specifications.

FIG. A10.5 Cylinder Liner Support Ring Tightening Procedure



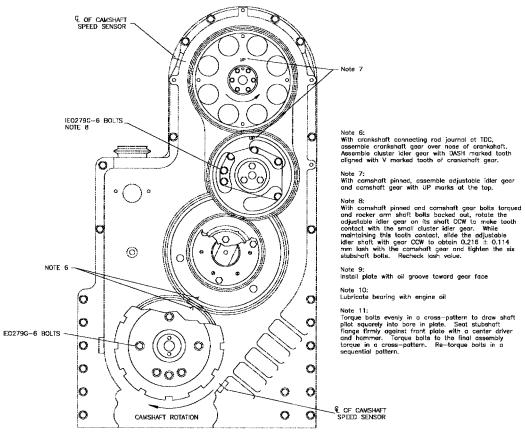
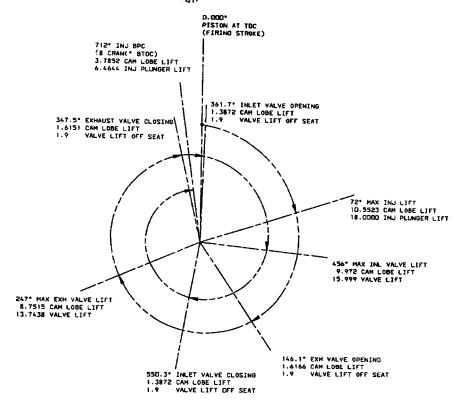


FIG. A10.6 1Y3700 Engine Timing





VALVE TIMING TOLERANCE ± 4°

Note—(a) Timing events in crankshaft degrees (reference only).

- (b) As viewed from front.
- (c) intake valve clearance set cold at 0.38.
- (d) intake valve clearance set cold at 0.76.
- (e) 1998 Scote engine.

FIG. A10.7 Timing Events in Crankshaft Degrees (for reference purpose only)

TABLE A10.1 Piston and Ring Specifications

| | Top Ring ^A | Intermediate Ring ^A | Oil Control Ring ^A |
|---|--------------------------|-----------------------------------|---|
| Width of groove in piston for piston ring (new) Thickness of piston ring (new) | | | $3.21 \pm 0.01 \text{ mm}$ $3.137 \pm 0.006 \text{ mm}$ |
| Side clearance between groove and piston ring (new) End gap clearance between end of ring (new) | 0.080 mm, min | 0.140214 mm | 0.057 - 0.089 mm |
| installed in 137.160 mm diameter gage | 0.585 - 0.737 mm | 1.004 - 1.156 mm | 0.382 - 0.636 mm |

^A This engine uses keystone style piston rings and grooves in the piston. The piston ring lands are also elliptically ground; therefore, measure ring side clearance as follows:

- (a) Assemble piston ring on the piston with UP side toward the top of the piston.
- (b) Install piston and ring in a 137.60 mm diameter ring gage or modified slotted liner (see Appendix X1).
- (c) Push piston and ring until ring to be measured is at the top of the gage. Keep the piston in the center of the gage.
- (d) Measure the side clearance with a feeler gage at both major (90° from the centerline of the pin bore) and minor diameters. Each measurement should be within specification shown.
- (e) Install the oil control ring with gap in the spring 180° away from the gap in the ring.

TABLE A10.2 Engine Assembly Measurements, mm

| Items to be checked | | Specifications | | Actual |
|--|-------------------|-----------------|-------------------|--------|
| | min | mean | max | |
| Crankshaft end play | 0.11 | 0.34 | 0.57 | |
| Camshaft end play | 0.175 | 0.25 | 0.325 | |
| Main bearing clearance (no.1) (front) | 0.089 | 0.138 | 0.187 | |
| Main bearing clearance (no.2) | 0.089 | 0.138 | 0.187 | |
| Main bearing clearance (no.3) | 0.089 | 0.138 | 0.187 | |
| Main bearing clearance (no.4) | 0.089 | 0.138 | 0.187 | |
| Nozzle tip projection | 1 | 1.3 | 1.6 | |
| Cam gear backlash | 0.102 | 0.216 | 0.33 | |
| Piston to head clearance | 1.55 | 1.62 | 1.69 | |
| ntake valve (1) Recess (closest to manifold) | 2.2 | 2.5 | 2.8 | |
| ntake valve (2) Recess | 2.2 | 2.5 | 2.8 | |
| Exhaust valve (1) Recess (closest to manifold) | 1.2 | 1.5 | 1.8 | |
| Exhaust valve (2) Recess | 1.2 | 1.5 | 1.8 | |
| nitial intake valve lash (cold) | | 0.38 | | |
| nitial exhaust valve lash (cold) | | 0.76 | | |
| nitial injector setting | | 78 ^A | | Α |
| After test intake valve lash (cold) | 0.3 | 0.38 | 0.46 | |
| After test exhaust valve lash (cold) | 0.68 | 0.76 | 0.84 | |
| After test injector setting | 77.8 ^A | 78 ^A | 78.2 ^A | Α |
| lywheel adapter runout (bore TIR) | | | 0.15 | |
| lywheel adapter runout (face TIR)(at R95) | | | 0.15 | |
| iming sensor location in front housing | 2° ATDC | 3° ATDC | 4° ATDC | |
| iner negative projection | 1.12 | 1.17 | 1.22 | |
| iner ID taper | | | 0.051 | |
| iner ID out of roundness | | | 0.038 | |
| iner ID smallest anywhere | | | 137.154 | |
| lign pointer with TDC mark on flywheel. | | | | |
| erify top of liner is below jug surface. | | | | |
| low cooling jet to verify aim. | | | | |
| njector and valve max lifts | | | | |
| njector plunger lift at 72° crank | 17.3 | 18.0 mm | 18.7 | |
| Exhaust valve lift at 247° crank | 13.0 | 13.7 mm | 14.4 | |
| ntake valve lift at 456° crank | 15.3 | 16.0 mm | 16.7 | |

^A Go/No-Go gage

A11. FLUSHING INSTRUCTIONS AND APPARATUS

A11.1 Table A11.1 is the flushing instruction sheet and Figs. A11.1-A11.3 illustrate the flushing apparatus.

TABLE A11.1 Flushing Instruction Sheet

| Step | Procedure | Flushing Fluid | Relief Valve ^A |
|------|--|-------------------------|--------------------------------|
| 1 | Drain used oil from sump, cooler, oil scale and remove oil filter Install 1Y3916 plug in front plate (in place of fuel cam/cylinder head) Install 1Y3979 cover on top of block Install 1Y3980 piston jet aim fixture on top of 1Y3979 cover Connect flush cart outlet to filter flush adapter 1Y3935 and 5 spray | | |
| | nozzles | | open |
| 2 | Connect flush cart pump inlet to solvent tank Install new oil filter on the oil flush cart | | opo.i |
| | Open engine sump drain. Then pump solvent into engine to flush | 7.6 L Stoddard solvent | |
| | used oil | no recirculation | closed |
| 3 | | Cleaning mixture of | |
| | Connect flush cart pump inlet to engine oil sump | 1.9 L Dispersant Engine | |
| | Close engine sump drain | Cleaner | closed 5 min. |
| | Circulate fluid with flush cart and oil scale pumps turned on | 5.7 L Stoddard Solvent | open 5 min. |
| 4 | Drain mixture from sump, cooler, oil scale, flush cart and filters | | open |
| 5 | | | open 5 min. |
| | Circulate fluid with flush cart and oil scale pumps turned on | 7.6 L Stoddard Solvent | closed 5 min. |
| 6 | Drain fluid from sump, cooler, oil scale, flush cart and filters | | open |
| 7 | Repeat steps 5 and 6 two times or as needed until solvent remains clean | | |
| 8 | | | open 5 min. |
| | Circulate EF-411 to flush Stoddard solvent | 5.6 L EF-411 | closed 5 min. |
| 9 | Drain oil from sump, cooler, oil scale, flush cart and filters | | open |
| 10 | Circulate EF-411 at 415 kPa manifold pressure and align piston jets | 5.6 L EF-411 | open 5 min. |
| 11 | Drain oil from sump, cooler and oil scale. Rebuild engine for test | | open |
| 12 | After engine is rebuilt, motor engine at a minimum of 200 r/min | 5.6 L EF-411 | Reconnect for normal operation |
| 13 | Drain oil from sump, cooler and oil scale | | open |

^A Supply 50 kPa air pressure to open the Johnson Controls oil relief valve.

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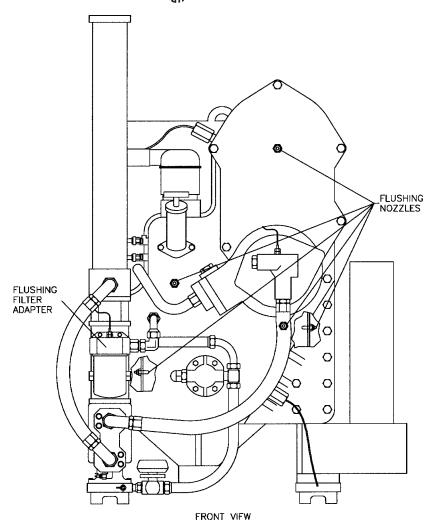


FIG. A11.1 Flushing Nozzle Locations

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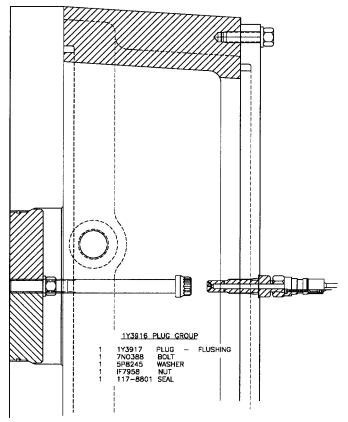


FIG. A11.2 Flushing Plug

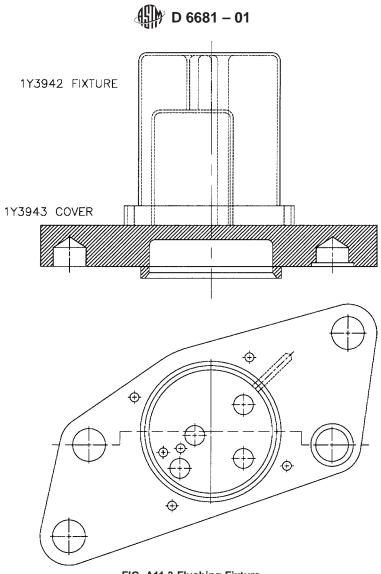


FIG. A11.3 Flushing Fixture

A12. WARM-UP, COOL-DOWN, AND TESTING CONDITIONS

A12.1 See Table A12.1.

TABLE A12.1 Warm-up, Cool-down, and Testing Conditions

| Parameter | Units | Tol | Test Specifications | | | | | |
|-------------------------|-------|--------|---------------------|---------|---------|---------|---------|--|
| | | | Step 1 | Step 2 | Step 3 | Step 4 | Step 5 | |
| | | | 5 min | 5 min | 5 min | 10 min | 60 min | |
| Speed | r/min | ±3 | 1000 | 1000 | 1400 | 1800 | 1800 | |
| Power | kW | | idle | 10 | 26 | 41 | ~55 | |
| Torque | N·m | (a) ±5 | | 100 | 176 | 219 | ~285 | |
| Fuel rate | g/min | (b) ±1 | | 48 | 95 | 148 | 185 | |
| Fuel timing | BTC | | 13 | 13 | 13 | 13 | 13 | |
| Humidity | g/kg | ±1.7 | | | | | 17.8 | |
| Temperatures °C | | | | | | | | |
| Fuel into head | | ±3 | ~31 | ~32 | ~33 | ~36 | 42 | |
| Coolant into jug | | | ~41 | ~51 | ~82 | ~86 | 86 | |
| Coolant from head | | ±3 | 42 | 52 | 83 | 90 | 90 | |
| Oil to cooler | | | | | | | ~128 | |
| Oil manifold | | ±3 | | | | | 130 | |
| External heating oil | | | 165 max | 165 max | 165 max | 165 max | 165 max | |
| Intake air manifold | | ±3 | | | 60 | 60 | 60 | |
| Exhaust manifold | | | ~120 | ~275 | ~340 | ~370 | ~480 | |
| Pressures kPa | | | | | | | | |
| Fuel from head | | ±20 | 275 | 275 | 275 | 275 | 275 | |
| Coolant into jug | | (c) | ~44 | ~44 | ~70 | ~81 | ~81 | |
| Oil manifold | | ±20 | 415 | 415 | 415 | 415 | 415 | |
| Intake air barrel (abs) | | ±1 | 120 | 120 | 157 | 225 | 272 | |
| Exhaust barrel (abs) | | ±1 | | 104 | 146 | 217 | 265 | |
| Crankcase | | | | | | ~.05 | ~.10 | |
| Flows | | | | | | | | |
| Coolant | L/min | ±2 | ~34 | ~34 | ~55 | 75 | 75 | |
| Blowby | L/min | | | | | ~35 | ~35 | |
| Air | kg/h | | | | | | ~315 | |

Note 1—(a) Engine controlled to torque specification for Steps 2, 3, 4 and 5 min of Step 5.

A13. PISTON AND LINER RATING MODIFICATIONS

A13.1 The 1P piston deposits are accessed using the Modified CRC Diesel Piston Rating Method described in CRC Manual No. 18. Three levels of carbon (heavy, medium, and light) are rated for grooves one and three. Only two levels of carbon (heavy and light) are rated for the second groove and all lands, and only one level of carbon (light) is rated for the cooling gallery and under-crown. The carbon deposit factors are 1.00 for heavy, 0.5 for medium, and 0.25 for light carbon. The varnish merit values range from 1.0 to 10 using the CRC Rust/Varnish Rating Scale where 10 is clean and 1.0 is maximum intensity. The merit varnish values are converted to demerit values resulting in deposit factors that range from 0 for clean to 9.0 for maximum intensity. The merit varnish values are converted to demerit values using Eq A13.1:

Demerit Varnish Zonal Rating = Area $\% \times (10 - Merit Rating)$ (A13.1)

A13.1.1 *Example*—15 % \times (10.0 – 8.5) = 0.15 \times 1.5 = 0.22 demerits using rounding guidelines presented in Practice E 29.

A13.1.2 Fig. A13.1 shows the deposit rating areas for the under-crown and cooling gallery of the piston crown.

A13.2 The rating location factors were chosen to yield separation between low and high calibration oils. All required rating equipment, such as the rating booth and particular lamp used, are described in CRC Manual No. 18.

A13.3 Use the following procedure for calculating this test method's piston deposit ratings:

A13.3.1 Rate the piston as is normally done according to the Modified CRC Diesel Piston Rating Method described in CRC Manual No. 18.

A13.3.2 For groove three, land three, land four, the cooling gallery and under-crown, replace the rater-assigned varnish merit values with the restricted factors listed in Table A13.1.

A13.3.3 Calculate a demerit value for each area.

A13.3.4 Round each demerit to the nearest 0.01 demerits according to Practice E 29.

A13.3.5 Add the demerits to get the individual unweighted demerit value for each piston location.

A13.3.6 Multiply the unweighted demerit value by its location factor to get the individual weighted demerit rating for each piston location.

⁽b) Engine controlled to fuel rate specification for last 55 min of Step 5.

⁽c) Air pressure at coolant tower controlled to 35 kPa.

Note 2—Ramp Up Conditions Between Warm-up Steps:

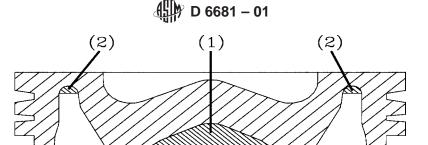
⁽a) Torque (Nm/min); at 5 min (beginning at Step 2)— 20 Nm/min.

⁽b) Speed (r/min); at 10 min (beginning at Step 3)— 100 r/min/min.

⁽c) Inlet air pressure (kPa); at 10 min (beginning at Step 3)—12 kPa/min.

⁽d) Exhaust air pressure (kPa); at 10 min (beginning at Step 3)— 12 kPa/min.

⁽e) Inlet air temperature (°C); at 10 min (at start of test)— 5°C/min.



Note—Area 1—Under-crown: All surfaces of the under-crown including transition radius, but not the vertical sides of the pin bore struts. Area 2—Cooling gallery: Only the upper radius area.

FIG. A13.1 Under-crown and Cooling Gallery Rating Areas

TABLE A13.1 Grouped Varnish Rating Factors

| Rater-Assigned Varnish Merit Value | Restricted Factor |
|------------------------------------|-------------------|
| 1.0–4.0 4.1–7.0 | 7.5 4.5 |
| 7.1–9.9 | 1.5 |

A13.3.7 Round each individual weighted demerit rating to the nearest 0.01 demerits.

A13.3.8 Add all individual weighted demerit ratings to get WDP

A13.3.9 Round WDP to the nearest 0.1 demerits.

A13.3.10 Top groove carbon (TGC) equals the total carbon demerits for groove one.

A13.3.11 Top land carbon (TLC) equals the total carbon demerits for land one.

A13.4 *Liner Rating Procedure*—Liner rating should follow the sequence outlined herein. If deposits above ring travel are to be evaluated this should be done immediately upon completion of the test or disassembly.

A13.4.1 Liner Preparation:

A13.4.1.1 *Marking*—Thrust and anti-thrust sides are marked T & AT along with appropriate test identification (run number, and so forth). See Fig. A13.2.

A13.4.1.2 *Cutting*—Liners are cut along the front and rear, leaving the thrust and anti-thrust halves.

A13.4.1.3 Surface Preparation—Caution should be observed in the handling of the liners due to the sharpness of the

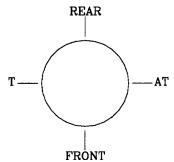


FIG. A13.2 Liner Thrust and Anti-Thrust Locations

cut edges. Wipe both halves of the liner using Stoddard solvent on a dampened soft rag followed by a clean soft dry rag.

A13.4.2 *Definition of Terms*—A clear plastic segmented overlay (see Fig. X1.6) is recommended as a useful rating aid in estimating the percentage of the area covered.

A13.4.2.1 *Bore Polishing*—Those areas of surface which are instantly recognizable as mirror finish regardless of random crosshatch honing marks.

A13.4.2.2 *Scuffing*—Localized adhesive wear distinguished by concentrated marks in the direction of motion, observed as a matte finish which is caused by a momentary welding and tearing of metal.

Note A13.1—Bore polishing and scuffing should be differentiated between and reported separately.

A13.4.2.3 *Scratching*—Random singular lines in the direction of motion generally a result of debris or installation of components. These need not be quantified, but should be noted in the appropriate remarks section.

A13.4.3 Liner Rating:

A13.4.3.1 *Rating Environment*—Rate liners in the CRC rating booth with the same light as specified to rate pistons or a two-bulb fluorescent desk lamp.

A13.4.3.2 *Bore Polishing*—The overlay is inserted in the liner half and the 10 to 15 % segments with 1 % indicators used as a guide in estimating the amount of polishing. Record the percent polish for each segment and then summarize those ten areas for each half. Tracing paper or equivalent may be used for a permanent record of the liner polishing.

A13.4.3.2.1 *Area Rated*—The area to be rated is generally defined as the area swept by the rings which is the distance from the top of the first ring at TDC to the bottom of the ring at BDC. On many occasions, it is required that the area above top ring travel be rated.

A13.4.3.3 *Liner Scuffing Rating*—Liner scuffing can be rated in a similar manner as bore polishing.

A13.4.3.4 Above Top Ring Travel Conditions—Area percentages may be determined in the liner by use of the 20-segmented template. Carbon deposits can be rated in two levels. Other conditions such as polishing, scratching/scuffing can be reported in area covered, if required.



A14. ADDITIONAL REPORT FORMS

A14.1 Figs. A14.1 and A14.2 are sample report forms.

LSRD4

| | rarp. | • | |
|--------------|-------|----------------|--|
| Product: | | Batch No.: | |
| | | TMC No.: | |
| Product No.: | | TMO No.: | |
| | | Tank No.: | |
| | | Analysis Date: | |
| | | Shipment Date: | |

| | I | | SPEC | IFICAT | IONS | | |
|---------------------------------|--------|-----------|-----------|--------|-----------|------------|------------|
| TEST | METHOD | UNITS | MIN | TARGET | MAX | RESULTS 'C | RESULTS 'F |
| Distillation - IBF | D-86 | ('C) 'F | (177) 350 | | (199) 390 | | |
| 10% | | ('C) 'F | (210) 410 | | (232) 450 | | |
| 50% | | ('C) 'F | (249) 480 | | (277) 530 | | |
| 90% | | ('C) 'F | (299) 570 | | (327) 620 | | |
| Distillation - EP | | ('C) 'F | (327) 620 | 1 | (360) 680 | | |
| Recovery | | vol% | | REPORT | | | |
| Residue | | vol% | | REPORT | | | |
| Loss | | vol% | | REPORT | | | |
| Gravity | D-4052 | 'APl | 32.0 | | 36.0 | | |
| Pour Point | D-97 | ('C) 'F | | | (-17) 0 | | |
| Cloud Point | D-2500 | ('C) 'F | | | (-12) 10 | | |
| Flash Point | D-93 | ('C) 'F | (54) 130 | | , , | | |
| Viscosity @ 40°C | D-445 | cSt | 2 | | 3.2 | | |
| Mercaptan Sulfur | D-3227 | wt% | | REPORT | | | |
| Sulfur | D-2622 | wt % | 0.030 | | 0.050 | | |
| Composition, Aromatics | D-1319 | vol% | 28.0 | | 35.0 | | |
| Composition, Olefins | D-1319 | vol% | | REPORT | | | |
| Composition, Saturates | D-1319 | vol% | | REPORT | | | |
| Basic sediment & water | D-2709 | vol% | | | 0.05 | | |
| Ramsbottom Carbon, 10 % residue | D-524 | w: % | | | 0.35 | | |
| Ash content | D-482 | wt % | | | 0.01 | | |
| Total Acid Number | D-664 | mg KOH/g | | REPORT | | | |
| Strong Acid Number | D-664 | mg KOH/g | | REPORT | | | |
| Accelerated Stability | D-2274 | mg/100 ml | | REPORT | | | |
| Copper Corrosion | D-130 | | | | 3 | | |
| Cetane Number | D-613 | | 42.0 | | 48.0 | | |
| Aliphatic paraffins | D-2425 | wt% | | REPORT | | | |
| Monocycloparaffins | D-2425 | wt % | | REPORT | | | |
| Dicycloparaffins | D-2425 | wt% | | REPORT | | | |
| Tricycloparaffins | D-2425 | wt % | | REPORT | | | |
| Alkylbenzenes | D-2425 | wt % | | REPORT | | | |
| Indanes/Tetralins | D-2425 | wt% | | REPORT | | | |
| Indenes | D-2425 | wt % | | REPORT | | | |
| Naphthalene | D-2425 | wt% | | REPORT | | | |
| Naphthalnenes | D-2425 | wt% | | REPORT | | | |
| Acenaphthenes | D-2425 | wt% | | REPORT | | | |
| Acenaphthylenes | D-2425 | wt% | | REPORT | | | |
| Tricyclic aromatices | D-2425 | wt % | | REPORT | | | |

| Approved by: | Analyst |
|--------------|-------------|
| | |

 $\label{eq:Note-Include} Note-Include a copy of Suppliers Fuel Sheet in the Test Report. \\ \textbf{FIG. A14.1 Fuel Batch Analysis Example}$

| Fax To: Company: Fax Number: | : | | | | | | Monitoring Charts And | g Center **** alysis *** | * | | | | |
|------------------------------------|-----------|-------------------|-----------------------|----------------|-------------|--------------------------------|---|-----------------------------|-------------------|------------|----------------------|----------------------|-----------|
| Start EOT date EOT time LTMS date | = = | | | |] | Lab Stand Run Reporte | | mm | | | CMII IND Analy | R = = vsis Com | piled: |
| LTMS time Parameter | = | Reported Value | | Trans Value | sforme | d | 1997021 Mean | S | Note: | When tw | r is the \ | <i>N</i> arning | |
| WDP TGC TLC AOC EOTOC | | | - | | | | • | | Keys: | and the lo | on alarn | 1 | on Limit. |
| | | | | EWM | | Stand A | nalysis | | | SHEWH | ART | | |
| | N | Z(i) | Severity Limit | Al | | Precision Limit | n Al | V(i) | Severity Limit | Al | | Precision Limit | Al |
| WDP TGC TLC AOC EOTOC | | | | | | | | | | | | | |
| | | | | EWM | | Laborat | tory Analy | sis | | SHEWH | ART | | |
| | N | Z(i) | Severity Limit | Al | | Precision Limit | n Al | Y(i) | Severity Limit | Al | | Precision Limit | Al |
| WDP TGC TLC AOC EOTOC | | | | | | | _ | | | | | | |
| | | WDP S | | | | tory Lev | vel Severity | Adjustments | TLC SA | | | | |
| STAND is Ca | alihrated | | AOC SA ≈ O_(Circle | | ed) | | | | ЕОТОС | SA = | | | |
| Calibration E | | | | _ | | | | | | | | | |
| A TMC Valid | • | - | | AC = A | - | | libration. | | | | | | |
| STAN | D PULI | LED FROM | A LTMS S | | | | | tance Criteria Reviewer | | | | | |

^A Based on review of call-in report of operational data and control chart analysis shown above.

FIG. A14.2 Example of Fax Copy of TMC Control Chart Analysis for Calibration Tests



A15. REPORT FORMS

A15.1 Figs. A15.1-A15.20 are example report forms.

VERSION 19980921

CONDUCTED FOR TSTSPON1 TSTSPON2

| | V = VALID |
|----------|--|
| LABVALID | I = INVALID |
| | N = RESULTS CAN NOT BE INTERPRETED AS |
| | REPRESENTATIVE OF OIL PERFORMANCE (NON- |
| | REFERENCE OIL) AND SHALL NOT BE USED IN |
| | DETERMINING AN AVERAGE TEST RESULT USING |
| [| MULTIPLE TEST CRITERIA |

| Test Number | | | | | |
|--------------------------------------|---------------|------------------|--|--|--|
| Test Stand: STAND | Engine Run No | o.: ENRUN | | | |
| EOT Time: EOTTIME | EOT Date: D7 | EOT Date: DTCOMP | | | |
| Oil Code ^A : OILCODE/CMIR | | | | | |
| Formulation/Stand Code: FORM | | | | | |
| Alternate Codes: ALTCODE1 | ALTCODE2 | ALTCODE3 | | | |

In my opinion this test OPVALID been conducted in accordance with the 1P TestMethod (D-XXXX) and the appropriate amendments through the information letter system. The remarks included in the report describe the anomalies associated with this test.

AOil Code (or CMIR if this is a reference oil test)

| SUBMITTED BY: | SUBLAB |
|---------------|--------------------|
| | Testing Laboratory |
| | SUBSIGIM |
| • | Signature |
| | SUBNAME |
| | Typed Name |
| | SUBTITLE |
| | Title |

FIG. A15.1 Final Report Cover Sheet

1P Form 1

TEST REPORT SUMMARY

| LAB: LAB | EOT DATE: DTCOMP | END TIME: EOTTIME | METHOD: METHOD | | | | | | | |
|--------------------------------|------------------|-------------------|----------------|--|--|--|--|--|--|--|
| STAND: STAND RUN NUMBER: ENRUN | | | | | | | | | | |
| FORMULATION/STAND CODE: FORM | | | | | | | | | | |
| OIL CODE/CMIR: OILCODE/CMIR | | | | | | | | | | |

| START DATE: DTSTRT | TOTAL TEST LE | NGTH: TESTLEN | TMC OIL TYPE. A IND |
|------------------------|---------------|-------------------|---------------------|
| LAB INTERNAL OIL CODE: | LABOCODE | ENGINE SERIAL NUM | MBER: ENGSN |

| i i | SPECTIVE DATE | WDP | TOC | TLC | OL CONSUMPTION On | TRANSPORMED OL CONSUMPTION | EOTOC gh | TRANSFORMED EGTOC |
|---|------------------|--------|--------|--------|-------------------------|----------------------------------|-------------|----------------------|
| UNADJUSTED LAB RATING | and the same | MD. | 10C | TLC | oc | OCT | ROPOC | 17007 |
| DENSITRY CORRECTION OF ANY) | DATACE | WOCF | 10004 | TLCCF | | OCTCF | 100-31 | RIOCICA |
| SUBTOTAL. | Challeton . | MOCCH | TOCCOR | TECCOR | 0.00 | OCTOR | 10000 | ETOCITOR |
| LAB SEVERITY ADJUSTMENT [®] OF ANY) | DATEKA | WZSA | TOXIX | TICH | | OCTEA | | 170C754 |
| TOTAL | 1400 | WORNS. | LOCART | TICPML | OCMA | OCTINE | BOTOCINE. | 17007/96 |
| | | | | | | | | |

| | EMICTIFE DATE | WDP | TGC | TLC | ONSUMPTION ON | TRANSFORMED OIL CONSUMPTION | EOTOC gh | TRANS-DRMED E000C |
|------------------------------|------------------|-----|------|-------|---------------|-----------------------------------|-------------|----------------------|
| TEST TAINIET MEAN! | EFFERTE | WIN | ROOM | TLOW | 77 71 7 | OCTM | 196-5 | SOTOCIM |
| TEST TARRET STD ^A | EPPDATE | MIR | POLY | 71.03 | | OCTE | 3/1950 | 8070078 |

| | MATERIALISM | WDP | TOC | TLC | | THE | |
|---------------------------------|-------------|--------|--------|-------|----------|--------------------|--|
| REFERENCE RATE-NOS ^A | MEAB | RSW(2) | RATION | RATIC | 10000000 | THE REAL PROPERTY. | |

| | TOP | INT.1 | OIL. | PISTON | PISTON SKIRT | LINER |
|------------------------------------|-----------------------------|--------------|--------------------|-------------------------|-----------------|----------|
| RING LOSS OF HIDE CLEARANGE (non.) | LSCTOP . | LSCINT | LSCOIL | | | 611111 |
| RINO END GAP INCREASE (WII) | MNGGTI | ADVGGIII | AINGFOI | | | |
| IS THE RING STUCK! | STUCKTOP | STUCKINI | STUCKOU | | | |
| SCUPPIED ABELA % | SCUFFTOP | SCUFFENI | SCUFFOIL | SCUPCHON | SCUPSKET | SCUFFLIN |
| AVERAGE WEAR STEP (run) | 3/858 L B | 111111111111 | THE REAL PROPERTY. | 1 | 03 V 100 V | AWEARST |
| % BORE POLISH | BOOK OF THE PERSON NAMED IN | | | Contraction of the last | | BOREFOL |

Notes: AReference oil tests or referee ratings requested by the test sponsor BNon-reference oil test only

FIG. A15.2 Test Report Summary

1P FORM 2 OPERATIONAL SUMMARY

| LAB: LA | AB | EOT DATE | : DTCOMP | | END TIME: | EOTTIME | METHOD: | METHOD | | |
|-------------|------------------------------|----------|-------------|-------|-----------|---------|---------|--------|--|--|
| STAND: | STAN | ID. | RUN NUMBER: | ENRUN | | | | | | |
| FORMULATI | FORMULATION/STAND CODE: FORM | | | | | | | | | |
| OILCODE (or | CMIR): | OILCOD | DE/CMIR | | | | | | | |

| Г | OPERATING | QUALITY | GUALITY INDEX | | PROCESS | ı | TO | TAL DATA PO | NTS |
|------------|----------------------|-----------|------------------|-------|---------|----------|-----------|-------------|---------------|
| 1 | PARAMETER | THRESHOLD | INDEX | UNITS | TARGET | AVERAGE | SAMPLES A | BQD P | OVER ON DER C |
| 1 | ENGINE SPEED | 0.00 | ORPM | r/min | 1800 | ARPM | NRPM | BRPM | ORPM |
| | FUEL FLOW | 0.00 | QFFL0 | g/min | 185 | AFFLO | NFFLO | BFFLO | OFFLO |
| | HUMIDITY | 0.00 | QHUMID | g/kg | 17.8 | AHUMID | NHUMID | BHUMID | OHUMID |
| | COOLANT FLOW | 0.00 | acolflo | L/min | 75 | ACOLFLO | NCOLFLO | BCOLFLO | OCOLFLO |
| æ | TEMPERATURE | | | | | | | | |
| Ē | COOLANT OUT | 0.00 | QCOLOUT | °C | 90 | ACOLOUT | NCOLOUT | BCOLOUT | OCOLOUT |
| PARAMETERS | OIL TO MANIFOLD | 0.00 | QOMANTM | ů | 130 | AOMANTMP | NOMANTMP | BOMANTMP | OOMANTMI |
| _ | INLET AIR | 0.00 | QINAIRT | °C | 60 | AINAIRT | NINAIRT | BINAIRT | OINAIRT |
| CONTROLLED | FUEL INTO HEAD | 0.00 | QFUELTMP | °C | 42 | AFUELTMP | NFUELTMP | BFUELTMP | OFUELTMP |
| NO | PRESSURES | | | | | | | | |
| ٥ | OIL TO MANIFOLD | 0.00 | QOMANPR | kPa | 415 | AOMANPR | NOMANPR | BOMANPR | OOMANPR |
| | INLET AIR (ABSOLUTE) | 0.00 | QINAIRP | kPa | 272 | AINAIRP | NINAIRP | BINAIRP | OINAIRP |
| | EXHAUST (ABSOLUTE) | 0.00 | QEBP | kPa | 265 | AEBP | NEBP | BEBP | OEBP |
| | FUEL FROM HEAD | 0.00 | OFUELPR | kPa | 275 | AFUELPR | NFUELPR | BFUELPR | OFUELPR |

| П | OPERATING | | PROCESS | | TO | TAL DATA PO | |
|----------------|--------------------------------------|-------|----------------|----------|----------------------|---------------|------------|
| | PARAMETER | UNITS | TYPICAL RANGE | AVERAGE | BAMPLES ^A | BOD® | OVERVAPERO |
| | INTAKE AIR FLOW(reference test only) | kg/h | 312-378 | AAIRFLO | | | |
| | POWER | kW | 53-57 | APWR | NPWR | BPWR | OPWR |
| | TORQUE | Nm | 248-301 | ATORQUE | NTORQUE | BTORQUE | OTORQUE |
| ERS | BLOWBY | L/min | 20-56 | ABLOBY | NBLOBY | BBLOBY | OBLOBY |
| PARAMETERS | TEMPERATURE | | | | | | |
| AR/ | COOLANT IN | •c | 86-88 | ACOLIN | NCOLIN | BCOLIN | OCOLIN |
| _ | COOLANT DELTA T | •c | 2-6 | ACOLDT | NCOLDT | BCOLDT | осоцт |
| 3 0 | OIL COOLER IN | °C | 128-131 | AOCOOLIN | NOCOOLIN | BOCOOLIN | OOCOOLIN |
| Ň | HEATING OIL | •c | 165 maximum | AHEATOIL | NHEATOIL | BHEATOIL | OHEATOIL |
| NON-CONTROLLED | EXHAUST | •c | 463-492 | AEXHTIMP | NEXHTMP | BEXHTMP | OEXHTMP |
| Z | PRESSURES | | | | | | |
| | CRANKCASE | kPa | 0.09-0.33 | ACCV | NCCV | BCCV | occv |
| | COOLANT TO JUG | kPa | 64-92 | ACOLPR | NCOLPR | BCOLPR | OCOLPR |

- A Total number of data points taken as determined from test length and procedural specified sampling rate
- B Number of Bad Quality Data points not used in the calculation of the statistical measures
- C Number of points clipped by over/under range limits of the statistical measures
- D Gathered from 1P Matrix Test data

FIG. A15.3 Operational Summary

1P

FORM 3 ASSEMBLY MEASUREMENTS AND PARTS RECORD

| LAB: LAB | LAB: LAB EOT DATE: DTCOMP | | | END TIME: | EOTTIME | METHOD: | METHOD | | | |
|-------------|------------------------------|-------------|-------|-----------|---------|---------|--------|--|--|--|
| STAND: STA | ND | RUN NUMBER: | ENRUN | | | | | | | |
| FORMULATION | FORMULATION/STAND CODE: FORM | | | | | | | | | |
| OILCODE: | OILCC | DE/CMIR | | | | | | | | |

| Additives y vigas (18) | MINERAL PROPERTY OF PRODUCTION |
|----------------------------------|--------------------------------|
| INJECTOR SETTING (GO / NO-GO) | INJSET |
| WAS TIMING INITIALIZED? (YES/NO) | TINIT |
| PISTON/HEAD CLEARANCE mm | PISTONCL |
| CAM GEAR BACKLASH mm | CAMLASH |
| DESIRED FUEL TIMING *BTC | FUELTIM |
| INTAKE VALVE OPEN "ATC | INVALOPN |
| INJECTOR PLUNGER LIFT mm @ 72° | PLUNLIFT |
| INTAKE VALVE LIFT mm @ 456° | INLIFT |
| EXHAUST VALVE LIFT mm @ 247° | EXLIFT |

| | PART NUMBER | R | SERIAL NUMBER | | DATE CODE | INSPECTION CODE |
|--------------------|-------------|---|---------------|---|-----------|-----------------|
| LINER | LINERPN | A | LINERSN | A | LINERDC B | |
| TOP RING | TOPPN | С | TOPSN | B | | |
| INTERMEDIATE RING | INTPN | С | INTSN | В | | |
| OIL RING | OILPN | С | OILSN | B | | |
| PISTON CROWN | CROWNPN | D | CROWNSN | D | CROWNDC F | CROWNIC G |
| PISTON SKIRT | SKIRTPN | н | SKIRTSN | 1 | | |
| FUEL INJECTOR | NOZZLEPN | J | NOZZLESN | K | | |
| ECM EPROM | ECMPN | | | | ECMDC | |
| PISTON COOLING JET | PTUBEPN | | PTUBESN | | | |

- A On liner O.D.

 B On liner O.D. (NNAN)
- B On paper envelope containing the ring
 F Number below "E" located on piston top
- H On bottom surface of skirt rim
 1 On bottom surface under pin bore

- C On box label
 D On top of piston
- G Number above "B" located on piston top
- J On top surface of plunger
- K On top surface of plunger -6 digits

FIG. A15.4 Assembly Measurements and Parts Record

FORM 4 PISTON RATING SUMMARY

| TE | ST IDENTIFICA | ATION | LAB: | LAB | EO | T DATE | :DTC | OMP | END | TIME: EO | TTIN | ИЕ | STANE | : STAI | VD | RUN | #; ENR | // ME | THOD: | METH | OD . |
|---------|---|----------------|------------|-------------|-------------------------------------|----------------|----------------|----------------|---------|---|------------|----------------|----------------|-------------|--------------------|-----------|-------------|-----------|--------------|---------------|-----------|
| FO | FORMULATION/STAND CODE: FORM OILCODE/CMIR: OILCODE/CMIR | | | | | | | | | | | | | | | | | | | | |
| | ST FUEL: TES | | | FUEL | BATCH | : FUEL | BTID | | DATE | ATE RATED: DTRATE RATER INITIALS: RINIT VERIFIED BY: VRINIT | | | | | | | · | | | | |
| | LAST STAND REI | ERENÇE ON | D/ | TE CO | MPLETI | ED: <i>LF</i> | DTCO | ИP | STAND | #: STAN | | | UN #: | LREN | | | OIL CO | | | | |
| | | | | WD | P | | TGC | | 1 | LC | OIL | CONSUM g/h | APTION | TRAN CON | SFOMED SUMPTION | OIL DN | | TOC /h | TI | ANSFO FOTO | RMED C |
| L | AST REF. THIS | STAN | D <i>U</i> | RWD | | LRTO | 3 <i>C</i> | | LRTLC | | LR | OC. | | LRO | CT | | LRE01 | ос | LR | ETOCT | |
| L | NDUSTRY AV | ERAGE | LI | RAWD | | LRA | TGC | | LRATL | С | ********** | | ************** | LRA | ост | | | | LR | AETOC | 7 |
| L | INDUSTRY | STD | LI | RSWD | | LRS | TGC | | LRSTL | C | | | | LRŞ | OCT_ | | | | LR. | SETOC | T |
| TO | OTAL PISTON RATINGS SUMMARY | | | | | | | | | , | | | | | | | | | | | |
| Ι, | | GROO | | · · · · · · | | LAND | • | | | | | GROO | VE | LAND | S | , | | | OOLING | | DER |
| | DEP. | NO | | |). 2 | NO | | NC |). 2 | DEP. | | | . 3 | |). 3 | _ | <u>0. 4</u> | | LERY | CRO | OWN |
| Ш | FACTOR | A,% | DEM. | A,% | DEM. | A,% | DEM. | A,% | DEM. | FACTO | R | A,% | DEM. | A,% | DEM. | A,% | DEM. | A,% | DEM. | A,% | DEM. |
| C | HC - 1.0 | G1HCA | G1HCD | G2HCA | В 2НСD | L1HCA | LIHCD | L2HCA | L2HCD | | | G3HCA | GЗHCD | 1.3HCA | L3HCD | LAHCA | L4HCD | | | | |
| R | MC - 0.5 | G1MCA | G1MCD | | | | | | | | | G3MCA | G3MCD | | | | | | | | |
| В | LC25 | GILCA | GILCD | G2LCA | GZLCD | LILGA | LILCO | LZLGA | LZLCD | | | G3LCA | G3LCD | L3LC4 | Tatco | LALCA | LALCD | OGLCA | OGLCD | UCLCA | UCLCD |
| 0 | | | | 1 | | | | | | | | | | | | | 7 | | | | |
| N | TOTAL | GIACTOI | G1DCTO | G2ACTO | твгостот | LIACTO | LIDCTOI | LZAÇTO | 1200707 | | | 3 <i>ACTOT</i> | 630CT0TE | 3ACTOT | L3DCTOTA | АСТОТ | L4DCTOT | SACTOT | рвостоп | CACTOT | рсостот |
| | | | G1V9D | | G2V9D | | | | | | | | | | | | | 1 | | | r |
| | 8 - 9 | GIVBA GIVBA | GIVED | G2V8A | G2V8D | LIV9A LIV8A | LIV9D LIV8D | L2V8A | L2V9D | | | | | | L3V75D | | | | | | |
| | 7 - 7.9 | GIV7A | G1V7D | G2V7A | G2V7D | LIVOA | LIVID | L2V0A | 12770 | 7.5 | | G3V75A | G3V750 | LSV/SA | LSV/SD | 140/54 | (47/50 | DGV75A | OGV75D | UCV/5A | UCV750 |
| ١., | 6 - 6.9 5 - 5.9 | GIV6A | G1V6D | GZV6A | G2V6D | LIVEA | LIVED | LZV6A | L2V6D | | \dashv | | | | - | <u> </u> | ╂ | | | <u> </u> | |
| Ă | 4 - 4.9 | GIV5A | GIV5D | G2V5A | G2V5D | LIV5A | LIVED | LZVSA | L2V50 | 4.5 | | G3V45A | G3V45D | 120454 | L3V45D | LAVASA | LAV45D | DOVASA | OGV45D | UCV454 | UCV45D |
| R | 3 - 3.9 | G1V4A | G1V4D | G2V4A | GZV4D | LIV4A | LTV4D | LZV4A | L2V4D | 4.5 | | | 55,455 | 20174 | | | | 00173 | | - | ******* |
| N | 2 - 2.9 | G1V3A | G1V3D | G2V3A | G2V3D | L1V3A | L1V3D | L2V3A | LZV3D | | | | | | | | <u> </u> | | | | |
| s | 1 - 1.9 | G1V2A | G1V2D | G2V2A | G2V20 | L1V2A | L1V2D | L2V2A | L2V2D | 1.5 | - | G3V15A | G3V15D | L3V15A | L3V150 | 4V15A | L4V15D | DGV15A | OGV15D | UCV15A | UCV150 |
| н | >0 - 0.9 | GIVIA | GIVID | G2V1A | G2V1D | LIVIA | LIVID | L2V1A | L2V1D | | | | | | | | | | | | 1 |
| | CLEAN 6 | VCLNA | 0 (| SACTATA | 0 | 1VCLNA | 0 | 2VCLNA | 0 | CLEAN | 1 | SVCLNA | 0 | 3VCLNA | 0 4 | IVCLNA | 0 | GVCLNA | 0 4 | CVCLNA | 0 |
| | | | | | | | | | | | | | | | | | | | | | |
| | TOTAL 61 | 4VTOT | G1DV704 | 2AVTOT | G20VTOT1 | IAVTOT | LIDVTOT | 2 <i>AVTOT</i> | LZDVTOT | | - | 3AVTOT | 33DVTOT E | SAVTOT | LSDVTOTE | 4AVTOT | L4DVTOT | GAVTOT | οσοντοτυ | CAVTOT | COVIOT |
| RA | TING | G1U | WD | G2U | <i>IWD</i> | L10 | JWD | L2U | IWD | | | G3U | WD . | L3U | WD | L4 | UWD | OGU | JWD | UC | IWD |
| LOC | ATION FACTOR | 2 | 2 | 3 | | 1 | | ; | 3 | | | 2 | 0 | | 0 | | 60 | 0 | .6 | | 1 |
| IN | RATING | G11 | ND | G2 | WD | L1\ | ND | L2 | WD | | | G3 | WD | L3 | WD | L4 | #WD | OG | WD | UC | WD |
| WDP TGC | | | | | TLC UNWEIGHTED DEP. T.L. FLAKED CAR | | | | CARBO | N % | | | | | | | | | | | |
| W | D | | | TGC | <u> </u> | | | | TLC | | | | UN | /D | | | | TLFC | | | |

FIG. A15.5 Piston Rating Summary

1P Form 4A PISTON RATING WORKSHEET^A

| LAB: LAB | EOT DATE: DTCOMP | END TIME: EOTTIME | METHOD: METHOD | | | | | | |
|-----------------------------|---------------------|-------------------|----------------|--|--|--|--|--|--|
| STAND: STAND | RUN NUMBER: ENRU | V | | | | | | | |
| FORMULATION/STAN | D CODE: <i>FORM</i> | | | | | | | | |
| OIL CODE/CMIR: OILCODE/CMIR | | | | | | | | | |

RATEWSIM

 A Refer to Appendix X1 for an example of a Piston Rating Worksheet. FIG. A15.6 Piston Rating Worksheet



1P

FORM 5 SUPPLEMENTAL PISTON DEPOSITS (GROOVE SIDES AND RINGS)

| LAB: | LAB | | EOT DATE | DTO | COMP | | | END TI | νίΕ: | EOTTIM | E ME | THOD: | METHOD |) | | | | |
|---------------|------------|---------|-------------------|-------------------|------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|---------------------|--|--|--|
| STAND: | STA | ND | RU | N NUMBE | R: | ENRUN | | | | | | | | | | | | |
| FORMULATION | i/STA | ND CO | DE: FORM | 1 | | | | | | | | | | | | | | |
| OILCODE/CMIR | : }: | | OILCODE/ | CMIR | | | | | | | | | | | | | | |
| | | | | CARBON | | | VARNISH | | | | | | | | | | | |
| DEPOSIT TYPE | | | нс | МС | LC | 8 - 9 | 7 - 7.9 | 6 - 6.9 | 5 - 5.9 | 4 - 4.9 | 3 - 3.9 | 2 - 2.9 | 1 - 1.9 | >0 - 0.9 | CLEAN | | | |
| | | | | | | | | | | | | | | | | | | |
| | 1 | | G1THCA | G1TMCA | GITLCA | G1T9A | G178A | G1T7A | G176A | G175A | GITAA | G1T3A | G1T2A | GITIA | GITCLNA | | | |
| | | В | G1BHCA | G1BMCA | G1BLCA | G189A | G1B8A | G187A | G186A | G185A | G184A | G183A | G1B2A | G1B1A | G1BCLNA | | | |
| GROOVE TOP | ********** | Т | G2THCA | GZTMCA | G2TLCA | G2T9A | G278A | G277A | G276A | G275A | G2T4A | G273A | G2T2A | G2T1A | G2TCLNA | | | |
| AND | 2 | В | G2BHCA | G2BMCA | G28LCA | G289A | G288A | G2B7A | G286A | G285A | G284A | G283A | 6282A | G281A | G2BCLNA | | | |
| воттом | | | | | | | | | | | | | | | | | | |
| | 3 | T B | G3THCA G3BHCA | G3TMCA G3BMCA | G3TLCA G3BLCA | G379A G389A | G3TBA G3B8A | G317A G387A | G3T6A G3B6A | G375A G385A | G374A G384A | G373A G383A | G3T2A G3B2A | G371A G381A | G3TÇLNA G3BCLNA | | | |
| | | | | | | | | | | | | l. | | 1 | | | | |
| | | Т | RITHCA | RITMCA | RITLCA | R1T9A | #1TBA | R177A | R176A | R175A | R1T4A | R1T3A | R1T2A | RITIA | RITCLNA | | | |
| | 1 | В | RIBHCA | R1BMCA | RIBLCA | R1R9A | R188A | R187A | R186A | R1B5A | A184A | R1B3A | R182A | RIBIA | R1BCLNA | | | |
| | ********* | BK | R1BKHCA | R1BKMCA | R1BKLCA | R1BK9A | R1BK8A | R1BK7A | R1BK6A | R1BK5A | R1BK4A | R1BK3A | R18K2A | R18K1A | R18KCLNA | | | |
| | | Т | RZTHCA | RZTMCA | RZTLCA | R2T9A | R2T8A | R2T7A | R2T6A | R2T5A | R2T4A | R2T3A | R2T2A | R2T1A | R2TCLNA | | | |
| TOP BOTTOM | 2 | В | R2BHCA | R28MCA | RZBLCA | RZBSA | R2B8A | #287A | R286A | R2B5A | R2B4A | R2B3A | R2B2A | R2B1A | R2BCLNA | | | |
| RINGS | | ВК | R2BKHCA | RZBKMCA | R2BKLCA | H2BK9A | R2BK8A | R2BK7A | R2BK6A | R2BK6A | R2BK4A | R2BK3A | R2BK2A | R2BK1A | R2BKCLNA | | | |
| | | | | | | | | | | | | | | | | | | |
| | _ | T | R3THCA | R3TMCA | R3TLCA | R3T9A | R3T8A | R3T7A | R3T6A | R3T5A | R3T4A | R3T3A | R3T2A | R3TIA | RSTCLNA | | | |
| | 3 | B BK | R3BHCA R3BKHCA | R3BMCA R3BKMCA | RBBLCA | R3B9A R3BK9A | R3B8A R3BK8A | R3B7A R3BK7A | R3B6A R3BK6A | R3B5A R3BK5A | R3B4A R3BK4A | R3B3A R3BK3A | R3B2A R3BK2A | R381A R3BK1A | R3BCLNA R3BKCLNA | | | |
| | | - DK | | | | | 1.55. | | | | | | 1 | | | | | |
| ADDITIONAL D | EPOS | IT & C | ONDITION | RATINGS | | | | | | | | | | | | | | |
| PISTON CROW | N | | CROWNAD | | | | | | | | | | | | | | | |
| PISTON SKIRT | | | SKIRTAD | | | | | | ., | | | | | | | | | |
| RINGS | | | RINGSAD | | | | | | | | | | | - | | | | |
| LINER | | | LINERAD | | | | | | | | | | | | | | | |

FIG. A15.7 Supplemental Piston Deposits (Groove Sides and Rings)



1P FORM 5A REFEREE RATING

| TEST IDENTIF | ICATION | | | | | | |
|--------------|-----------------|---------------|--------|-------------|---------|---------|--------|
| LAB: | LAB | EOT DATE: | DTCOMP | END TIME: | EOTTIME | METHOD: | METHOD |
| STAND: | STAND | RUN #: | ENRUN | | | | |
| FORMULATIO | N/STAND CODE: | FORM | | | | | |
| OILCODE/CM | R: | OILCODE/CMIR | | | | | |
| REFEREE RAT | ING INFORMATION | | | | | | |
| COMPANY | RRI AR | BATING NUMBER | RRNO | DATE BATED: | RRDATE | DATED: | RRINIT |

| то | TAL PISTON R | ATIN | 3S SUN | MARY | 1 | | | | | | | | | | | | | | | |
|--------|--------------|----------------|---|------------------------------|----------|-----------|----------|----------|----------|--------|---------|-----------|----------|---|----------|----------|---------|-----------------|---------|----------|
| ۱ _ | | | GRO | OVES | | | LAI | NDS | | | GRO | OVES | | LAI | NDS | | OIL C | OOLING | UN | DER |
| 1 1 | DEP. | N |). 1 | NO | D. 2 | NO |). 1 | N | 0. 2 | DEP. | N | 0. 3 | N | 0. 3 | N | 0. 4 | GAI | LERY | CR | OWN |
| نلـــا | ACTOR | Α,% | DEM. | A,% | DEM. | A,% | DEM. | A,% | DEM. | FACTOR | A,% | DEM. | A,% | DEM. | A,% | DEM. | A,% | DEM. | A,% | DEM. |
| d | HC-1.0 | N G1HCA | | | RRG2HCD | - | | | RRL2HCD | | RAG3HC/ | RRG3HCD | RRL 3HCA | AAL3HCD | RRLAHCA | RRL4HCD | | | | |
| ĬĂ | | RG1MCA | RRG1MCD | | | | | | | | RRG3MC/ | RRG3MCD | | | | | | | | |
| R | | RRG1LCA | ARG1LCD | RRG2LCA | RRGZLCD | RRLILCA | RRL1LCD | RRL2LCA | RRL2LCD | | RRG3LCA | ARG3LCD | RRL3LCA | RALSLCD | RRL4LCA | RRL4LCD | RROGLCA | RROGLCD | RRUCLCA | ARUCLCD |
| B | 20 /20 | | | | | | | | | | | | | | | | | | | |
| l Si | | | | GZACTO | RG2DCTOT | LIACTO | ALIDCTOT | L2ACTO | RL2DCTOT | | 63АСТО | RG3DC TOT | L3ACTO | *************************************** | L4ACTO | RL4DCTOT | обасто | POGDCTOT | UCACTO | RUCDCTO |
| | | | | | | | | | | | | | | | | | | | | |
| ╽┝ | 0.3 | 49G1V9A | | | | | RRL1V9D | | Ļ | | | | | | | | | | | Ī |
| ╽┝ | 7 - 7.5 | VAG I VALA | | RRG2V8A | | | | | RRL2V8D | 7.5 | RG3V75. | RAG3V75D | RRL3V75 | RRL3V75D | RAL4V75A | RRL4V750 | ROGV75 | RROGV75D | RUCV75/ | RRUCV75E |
| L | 0 - 0.9 | | RAG1V7D | | | | | | RRL2V7D | | | | | | | | ļ | | | |
| ╎╎ | 5 - 5.5 | VHG1VBA | 72.00 | | RRG2V6D | RRL1V6A | | | RRL2V6D | | | | | İ | | | | | | |
| 옶 | 4-4.3 | NG1V54 | | | | | | - | RRL2V5D | 4.5 | MG3V45 | RRG3V45D | RRL3V45/ | RRL3V450 | RRL4V45A | RRL4V45D | PROGV45 | AROGV450 | RUCV45 | RRUCV450 |
| N- | 3.3.0 | RG1V4A | RAG1V4D | | | ARL I V4A | | | RRL2V4D | | ļ | ļ | | ļ | | | | | | |
| ı _ | 2-2.5 | MG1V3A | | RAG2V3A | | ARL I V3A | | ARL 2V3A | | | | l | | | | | | | | |
| S | 1-1.3 | | | | | RRL 1V2A | RRL1V2D | ARL2V2A | | 1.5 | RG3V15 | RAG3V15D | RRL3V15A | RRL3V15D | RRL4V154 | RRL4V15D | ROGV15 | MROGV15D | RUCV15 | RRUCV150 |
| ╙ | 70-0.3 | IRG1V1A | | RRG2V1A | RRG2V1D | ARL1V1A | | ARL2V1A | | | | | | | | | | | | l |
| **** | CLEAN | MGTVCL | | IRG2VCL/ | 0 | RRL I VCL | | RRL2VCLA | 0 | | RG3VCL | 0 | RESVEL | , , | RRLAVCLA | | ROGVCL | | RUCVCL | 0 |
| | | | *************************************** | A PROTECTION OF THE PARTY OF | RG2DVTOT | | | | | | | RG3DVTOT | | | _ | | | | | |
| RA | TING | RRG | IUWD | RRG | 2UWD | RRL 1 | UWD | RRL | 2UWD | | RRG | 3UWD | RRL: | 3UWD | RRL4 | 1UWD | RRO | GUWD | RRU | CUWD |
| - | ATION FACTOR | | 2 | | 3 | | 1 | | 3 | | | 20 | | 20 | | 30 | |).5 | 711.0 | 1 |
| | | | | | | | • | | <u>-</u> | | | | | | | - | | | | |
| IND | RATING | RRG | 1WD | RRG | 2WD | RRL | 1WD | RRL | 2WD | | RRG | 3WD | RRL | 3WD | RRL | 4WD | RRC | GWD | RRU | ICWD |
| | WDP | | | | | TGC | | | | TLÇ | | U | NWEI | HTED (| DEP. | | T.L. FL | AKED (| ARBO | N % |
| R | RWD | | | RRT | GC | | | F | RRTLC | | | RRUV | VD | | | 1 | RRTLF | ; | | |

FIG. A15.8 Referee Rating

1P Form 6 Oil analysis

| TEST IDENTIFICA | TION | | | | | | |
|-----------------|-------------|--------------|-------------|---------|---------|--------|--|
| LAB: LAB | EOT DATE: | DTCOMP | END TIME: | EOTTIME | METHOD: | METHOD | |
| STAND: | STAND | RUN NUMBER: | ENRUN | | | | |
| FORMULATION/S | STAND CODE: | | FORM | | | | |
| OILCODE/CMIR: | | OILCODE/CMIR | | | | | |
| TEST FUEL: | TESTF | TUEL | FUEL BATCH: | FUE | LBTID | | |

| OIL ANALYSIS | NEW: | 24 | 48 | 72 | 96 | 120 | 144 | 168 | 192 | 216 | 240 | 264 | 288 | 312 | 336 | 360 |
|---------------------------------------|----------|----------|----------|----------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| VISC @ 100°C | V100HNEW | V100H024 | | | V100H096 | | | | | | V100H240 | | V100H288 | | | V100H360 |
| VISC @ 40°C | V40_HNEW | V40_H024 | | | V40_H096 | | | | | | V40_H240 | | V40_H288 | | | V40_H360 |
| TBN D4739 | TBN_HNEW | TBN_H024 | | | TBN_H096 | | | | | | TBN_H240 | | TBN_H288 | | | TBN_H360 |
| TAN D664 | TAN_HNEW | TAN_H024 | | | TAN_H096 | | | | | | TAN_H240 | | TAN_H288 | | | TAN_H360 |
| WEAR METALS Fe (ppm) | FEWMHNEW | FEWMH02 | | | FEWMH09 | | | | | | FEWMH24 | | FEWMH28 | | | FEWMH360 |
| Al (ppm) | ALWMHNEY | ALWMH02 | | | ALWMH09 | | | | | | ALWMH24 | | ALWMH28 | | | ALWMH36 |
| Si (ppm) | SIWMHNEW | SIWMH024 | | | SIWIMH096 | | | | | | SIWMH240 | | SIWMH280 | | | SIWMH360 |
| Cu (ppm) | CUWMHNEV | симмног | , | | CUWMH09 | , | | | | | CUWMH24 |) | CUWMH28 | | | Симмнзв |
| Cr (ppm) | CRWMHNEY | CRWMH02 | | | CRWMH09 | | | | | | CRWMH24 | , | CRWMH28 | , | | CRWMH36 |
| Pb (ppm) | PBWMHNEV | PBWMH02 | | | PBWMH09 | | | | | | PBWMH24 | | PBWMH28 | | | PBWMH38 |
| FUEL DILUTION % | | FDILH024 | | | | | | | | | FDILH240 | | | | | FDILH380 |
| BLOWBY (L/min) | | BLBYH024 | BLBYHO48 | BLBYH072 | BLBYH096 | BLBYH120 | BLBYH144 | BLBYH168 | BLBYH192 | BLBYH216 | BLBYH240 | BLBYH264 | BLBYH288 | BLBYH312 | BLBYH336 | BLBYH360 |
| Oil Consumption g/h for hrs ending | | OCOMHO24 | OCONHO48 | OCONHO72 | OCONHO96 | OCONH120 | OCONH144 | OCONH168 | OCONH192 | OCONH216 | OCONH240 | OCONH264 | OCONH288 | OCOMH312 | осомн336 | OCONH360 |
| Oil Consumption | | OCRRHO24 | OCRRHO48 | OCRRH072 | OCRRH096 | OCRRH120 | OCRRH144 | OCRRH168 | OCRAH192 | OCRRH216 | OCRRH240 | OCRRH264 | OCRRH288 | OCRRH312 | OCRRH336 | OCRRH360 |
| FUEL POSITION (mm) | | FPOSH024 | | | | | | | | | FPOSH240 | | | | | FPOSH360 |

FIG. A15.9 Oil Analysis



1P FORM 7

DOWNTIME SUMMARY

| LAB: | LAB EC | T DAT | E: DTCOMP | | END TIME: | EOTTIME | METHOD: | METHOD | |
|---------|----------|-------|-------------|-------|-----------|---------|---------|--------|---|
| STAND: | STAND | | RUN NUMBER: | ENRUN | | | | | |
| FORMULA | ATION/ST | AND C | ODE: : FORM | | | | | | _ |
| OILCODE | /CMIR: | OILCO | DDE/CMIR | | | | | | _ |

| Number of | Downtime | Occurrences | DWNOCR | |
|---------------|----------|-------------|---------|--------------------------|
| TEST HOURS | DATE | DOWNTIME | | REASONS |
| DOWNHOO1 | DDATHOO1 | DTIMHO01 | REAH001 | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| • | | | | 7.00 |
| | | | | |
| | | | | |
| | 1 | TOTLDOWN | TOTA | L DOWNTINE (126 HR. MAX) |

| Commente | | |
|-------------------------|--------|--|
| Number of Comment Lines | тотсом | |
| ОСОМН001 | | |
| | | |
| | | |
| | | |
| | | |
| | | |

FIG. A15.10 Downtime Summary

1P FORM 8 RING MEASUREMENTS

| LAB: LAB | EOT DATE: DTCOMP | END TIME: EOTTIME | METHOD: METHOD | | | | | | | |
|-----------------------------|------------------------------|-------------------|----------------|--|--|--|--|--|--|--|
| STAND: STAND | RUN NUMBER: ENRUM | V | | | | | | | | |
| FORMULATION/STANI | FORMULATION/STAND CODE: FORM | | | | | | | | | |
| OIL CODE/CMIR: OILCODE/CMIR | | | | | | | | | | |

ALL RING MEASUREMENTS ARE MADE USING METRIC FEELER GAGES

| RING GAPS (mm) | 1Y3802 TOP | 1Y3803 INTERMEDIATE | 1Y3804 OIL |
|----------------|----------------------------|-----------------------------|----------------|
| SPECIFICATIONS | $0.66 \pm 0.08 \text{mm}$ | $1.08 \pm 0.08 \mathrm{mm}$ | 0.51 ± 0.13 mm |
| PRE-TEST | RINGGTE | RINGFI1E | RINGGOE |
| POST-TEST | RINGFTO | RINGGI 10 | RINGGOO |
| INCREASE | RINGGTI | RINGGI 11 | RINGGOI |

| | NG SIDE CARANCE ^A | A | В | С | D | AVG. | MIN. | SPECIFICATION |
|-----|---------------------------------|-------------|----------|------------|------------|------------|------------|-----------------------------|
| | PRE-TEST | SIDETPE 1 | SIDETPE2 | SIDETPE3 | SIDETPE 4 | ASIDETPE | ISIDETPE | |
| TOP | POST-TEST | SIDETO1 | SIDETPO2 | SIDETPO3 | SIDETPO4 | ASIDETPO | ISIDETPO | $0.13 \pm 0.04 \mathrm{mm}$ |
| | LSC | LSCT1 | LSCT2 | LSCT3 | LSCT4 | LSCTOP | ILSCT | 0.10 = 0.0 |
| | PRE-TEST | SIDE 1 PE 1 | SIDE1PE2 | SIDE1PE3 | SIDE1PE4 | ASIDE I PE | ISIDE ! PE | |
| INT | POST-TEST | SIDE 1 PO 1 | SIDE1PO2 | SIDE I PO3 | SIDE 1 PO4 | ASIDE1PO | ISIDE1PO | $0.18 \pm 0.04 \mathrm{mm}$ |
| | LSC | LSCI1 | LSCI2 | LSC13 | LSCI4 | LSCINT1 | ILSCINT | 0110 - 010 1 11111 |
| | PRE-TEST | SIDEOPE 1 | SIDEOPE2 | SIDEOPE3 | SIDE OPE 4 | ASIDE OPE | ISIDEOPE | |
| OIL | POST-TEST | SIDEOPOI | SIDEOPO2 | SIDE OPO3 | SIDE OP 04 | ASIDEOP | ISIDEOPO | $0.07 \pm 0.02 \mathrm{mm}$ |
| | | | | | | 0 | | 0.07 = 0.0 2 kim |
| | LSC | LSCO1 | LSCO2 | LSCO3 | LSCO4 | LSCOIL | ILSCO | |

- ^A 1. Write STUCK in place of dimension when applicable.
 - 2. Write <0.03 mm for clearance when applicable.
 - 3. Write > before calculated decrease or average decrease values that incorporate a <0.03 mm in the calculation.
 - 4. LSC = Loss of Side Clearance.
 - 5. MIN: Oil ring minimum side clearance is measured 360° around piston.

FIG. A15.11 Ring Measurements



1P FORM 9 LINER MEASUREMENTS

| LAB: LAB | EOT DATE: DTCOMP END TIME: EOTTIME METHOD: METHOD | | | | | | | | |
|------------------|---|--|--|--|--|--|--|--|--|
| STAND: STAND | RUN NUMBER: ENRUN | | | | | | | | |
| FORMULATION/STA | AND CODE: FORM | | | | | | | | |
| OIL CODE/CMIR: O | OIL CODE/CMIR: O/LCODE/CM/R | | | | | | | | |

| DISTANCE FROM TOP | TRANSVERSE | LONGITUDINAL | AVERAGE |
|-------------------|------------|---------------|----------|
| 130 mm | BBLFINTI | BBLFINLI | BBLFINAI |
| 50 mm | BBLFINT2 | BBLFINL2 | BBLFINA2 |
| 25 mm | BBLFINT3 | BBLFINL3 | BBLFINA3 |
| | | TOTAL AVERAGE | BBLFIN |
| | | | |

| % LINER BO (ADD T/AT VALU | |
|------------------------------|---------|
| THRUST | BOREPT |
| ANTI-THRUST | BOREPAT |
| TOTAL | BOREPOL |

| | BEFORE TEST | - DIAMETER (DI | AL BORE GAGE |) | |
|-------------------|-------------|----------------|--------------|--------------------------------|--|
| BORE HEIGHT | LONGITU | DINAL TRA | ANSVERSE | OUT OF ROUND (0.038 mm max) | |
| 250 mm | BBLON | GI B | BTRANI | OOR1 | |
| 210 mm | BBLON | G2 B | BTRAN2 | OOR2 | |
| 170 mm | BBLON | G3 B | BTRAN3 | OOR3 | |
| 130 mm | BBLON | G4 B | BTRAN4 | OOR4 | |
| 50 mm | BBLON | G5 B | BTRAN5 | OOR5 | |
| 25 mm | BBLON | G6 B | BTRAN6 | OOR6 | |
| 15 mm | BBLON | G7 B | BTRAN7 | OOR7 | |
| TAPER (0.050 max |) TAPRLO | NG T | APRTRAN | | |
| | AFTER T | EST - (SURFACE | PROFILE) | | |
| 183 (253) | LONGIT | UDINAL | TR. | ANSVERSE | |
| minute la como S | FRONT | REAR | T | AT | |
| WEAR STEP @ 13 mm | AWEARLF | AWEARLR | AWEARTT | AWEARTAT | |

FIG. A15.12 Liner Measurements

FORM 10 CHARACTERISTICS OF THE DATA ACQUISITION SYSTEM

| LAB: LAB | EOT DA | TE; DTCOMP | END TIME: | EOTTIME | METHOD: | METHOD | | |
|----------------------------|---------|-------------------|-----------|---------|---------|--------|--|--|
| STAND: STA | ND | RUN NUMBER: ENRUM | " | | | | | |
| FORMULATION | I/STAND | CODE: FORM | | | | | | |
| OILCODE/CMIR: OILCODE/CMIR | | | | | | | | |

| PARAMETER | SENSING DEVICE | CALIBRATION | RECORD DEVICE | OBSERVATION FREQUENCY | RECORD FREQUENCY | LOG FREQUENCY | SYSTEM RESPONSE |
|----------------------|-------------------|-------------|------------------|--------------------------|---------------------|------------------|--------------------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
| OPERATION COMPATIONS | | | | | | | |
| ENGINE SPEED (R\min) | RPMSENS | RPMCALF | RPMRECO | RPMOBSF | RPMRECF | RPMLOGF | RPMSYSR |
| ENGINE POWER (kW) | PWRSENS | PWRCALF | PWRRECD | PWROBSF | PWRRECF | PWRLOGF | PWRSYSR |
| FUEL FLOW (g/min) | FFLOSENS | FFLOCALF | FFLORECD | PFL00BSF | FFLORECF | FFLOLOGF | FFLOSYSR |
| HUMIDITY (g/kg) | HUMSENS | HUMCALF | HUMREÇD | HUMOBŞF | HUMRECF | HUMLOGF | HUMSYSR |
| TEMPTRATURES IND | | | | | | | |
| COOLANT OUT | COTSENS | COTCALF | COTRECD | COTOBSF | COTRECF | COTLOGF | COTSYSR |
| COOLANT IN | CONSENS | CONCALF | CONRECD | CONOBSF | CONRECF | COMLOGF | CONSYSA |
| OIL TO MANIFOLD | OBRGSENS | OBRGCALF | OBRGRECO | OBRGOBSF | OBRIGRECF | OBRGLOGF | OBRGSYSR |
| OIL COOLER IN | OCOLSENS | OCOLGALF | OCOLRECO | OCOLOBS# | OCOLRECF | OCOLLOGF . | OCOLSYSA |
| INLET AIR | AIRTSENS | AIRTCALF | AIRTRECD | AIRTOBSF | AIRTRECF | AIRTLOGF | AMTSYSR |
| EXHAUST | EXTSENS | EXTCALF | EXTRECD | <i>EXTORSF</i> | EXTRECF | EXTLOGF . | EXTSYSR |
| FUEL TO HEAD | FUELSENS | FUELCALF | FUELRECO | FUELOBSF | FUELRECF | FUELLOGF | FUELSYSR |
| PRESSURES (SPS) | | | | | | | |
| OIL TO MANIFOLD | OBRPSENS | OBRPGALF | OBRPRECD | OBRPOBSF | OBRPRECF | OBRPLOGF | OBRPSYSR |
| INLET AIR | AIRPSENS | AIRPCALF | AIRPRECD | AIRPOBSF | AIRPRECF | AIRPLOGF | AIRPSYSR |
| EXHAUST | EXPSENS | EXPCALF | EXPRECD | EXPOBSF | EXPRECF | EXPLOGF | EXPSYSR |
| FUEL FROM HEAD | FFILSENS | FFILGALF | FFILRECD | FFILOBSF | FFILRECF | FFILLOGF | FFILSYSR |
| CRANKCASE | CCVSENS | CCVCALF | CCVRECD | CCVOBSF | CCVRECF | CCVLOGF | CCVSYSA |
| FLOWS (Limin) | | | | | | | |
| BLOWBY | BLBYSENS | BLBYCALF | BLBYRECD | BLBYOBSF | BLBYRECF | BLBYLOGF | BLBYSYSR |
| COOLANT FLOW | CFLWSENS | CFLWCALF | CFLWRECD | CFLWOBSF | CFLWRECF | CFLWLOGF | CFLWSYSR |

LEGEND:

- I COMPUTER, USING MARUAL DATA ENTRY
 (7) COMPUTER, USING MARUAL DATA ENTRY
 (7) COMPUTER, USING MARUAL DATA ENTRY
 (8) THE TYPE OF DEVICE WHERE DATA IS RECORDED
 (1) HANDLOG SHET

 DL AUTOMATIC DATA LOGGER
 C.M. COMPUTER, USING MARUAL DATA ENTRY
 (7) COMPUTER, USING MARUAL DATA ENTRY
 (7) COMPUTER, USING MARUAL DATA ENTRY

- (5) DATA AREA OBSERVED BUT ONLY RECORDED IF OFF SPEC.

 (6) DATA ARE RECORDED BUT ARE NOT RETAINED AT EOT

 (7) DATA ARE IGGGED AS PREMAMENT RECORD, NOTE SPECIFY IF:

 SS. SNAPSHOT TAKEN AT SPECIFIED FREQUENCY

 AGX AVERAGE OF X DATA POINTS AT SPECIFIED FREQUENCY

 (8) TIME FOR THE OUTPUT TO REACH 63.2% OF FINAL VALUE FOR STEP CHANGE AT INPUT

FIG. A15.13 Characteristics of the Data Acquisition System

1**P** FORM 11 ENGINE OPERATIONAL DATA PLOTS^A

| LAB: LAB | EOT DATE: DTCOMP | END TIME: EOTTIME | METHOD: METHOD | | | | | | |
|--------------------------------|------------------------------|-------------------|----------------|--|--|--|--|--|--|
| STAND: STAND RUN NUMBER: ENRUN | | | | | | | | | |
| FORMULATION/STANI | FORMULATION/STAND CODE: FORM | | | | | | | | |
| OIL CODE/CMIR: OILCODE/CMIR | | | | | | | | | |

 $^{^{\}mathrm{A}}Refer$ to Table A2.6 for plotting axes ranges and increments.

FIG. A15.14 Engine Operational Data Plots



1P FORM 12 TORQUE AND EXHAUST TEMPERATURE HISTORY

| LAB: LAB | EOT DATE: DTCOMP | END TIME: EOTTIME | METHOD: METHOD | | | | | | |
|--------------------------------|------------------------------|-------------------|----------------|--|--|--|--|--|--|
| STAND: STAND RUN NUMBER: ENRUN | | | | | | | | | |
| FORMULATION/STAN | FORMULATION/STAND CODE: FORM | | | | | | | | |
| OIL CODE/CMIR: OILCODE/CMIR | | | | | | | | | |

Data From Last 10 Tests

OCPIM

72

96

| Test No. | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|-----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| Avg. Exh. | AEXHHO01 | AEXHH002 | AEXHH003 | AEXHH004 | AEXHHD05 | AEXHHD06 | AEXHHO07 | AEXHH008 | AEXHH009 | AEXHHD10 |
| Temp. °C | | | | | | | | | | |
| Avg. Eng. | ATORHO01 | ATORHO02 | ATORHO03 | ATORHO04 | ATORHO05 | ATORHO06 | ATORHO7 | ATORHO08 | ATORHO9 | ATORHO10 |
| Torque | | | | | | | | | | |
| N·m | | | | | | | | | | |

FIG. A15.15 Torque and Exhaust Temperature History

1P FORM 13 OIL CONSUMPTION PLOT

| | | | | | | JIL CUI | APOINL | HUN P | LOI | | | | | | |
|--------------------------------------|-------|-------|--|------------|----|---------|--------|--------|-----|---------|-----|--------|----------|---|-------|
| LAB: | LAE | ? | EOT DATE: | DTCOMP | | | | END TI | ME: | EOTTIME | MET | HOD: / | METHOD | _ | |
| STAND: | | STAN | D | RUN NUMBER | ₹: | ENRUN | | | | | | | | | |
| FORMU | LATIO | N/STA | ND CODE: ' | FORM | | | | | | | | | | | |
| OILCOD | E/CMI | R: | OILCOL | DE/CMIR | | | | | | | | | | | |
| Oil | | , | | | | | | | | | | | | | |
| Consumption g/h | | | | | | | | | | | | | | | |
| | 30 | | | | | | | - | | | | | 1 | | |
| | 28 | | | | | | | | | | | | ··· | | |
| Beginning of Test Oil Consumption | 26 | | | | | | | | | | | | | | |
| вотос | 24 | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | 22 | | | | | | | | | | | | | | |
| End of Test Oil Consumption | 20 | | | | | | | | | | | | | | |
| EOTOC | 18 | | <u> </u> | | | | | | | | | | ļ | | |
| | 16 | | | | | | | | | | | | | | . |
| Overall Oil Consumption | | | | | | | | | | | | | | | |
| oc | 14 | | | | | | | | | | | | | | |
| | 12 | | | | | | | | | | | | | | - |
| | 10 | | <u> </u> | | | | | | | | | | L | | |

FIG. A15.16 Oil Consumption Plot

192

216 240

264

288

312

336 360

144 168

HOURS



$\begin{array}{c} 1P \\ Form~14 \\ PISTON, RING~AND~LINER~PHOTOGRAPHS^A \end{array}$

| LAB: LAB | EOT DATE: DTCOMP | END TIME: EOTTIME | METHOD: METHOD | | | | | | |
|------------------------------|-------------------|-------------------|----------------|--|--|--|--|--|--|
| STAND: STAND | RUN NUMBER: ENRUN | | | | | | | | |
| FORMULATION/STAND CODE: FORM | | | | | | | | | |
| OIL CODE/CMIR: OILCODE | VCMIR | | | | | | | | |

PRLIM

^ARefer to Fig. X1.7 for an example of a Photo Layout.

FIG. A15.17 Piston, Ring, and Liner Photographs



1P FORM 15 SEVERITY ADJUSTMENT HISTORY

| | L | EO! DAIR | : DTCO | WP | | END TIME: | EOTTI | ME M | ETHOD: | METHO | O |
|----------|----------|----------|---|----------------|---------|------------|----------|----------|----------|--------------|----------|
| STAND | STAND |) | RUN NUM | BER: <i>El</i> | VRUN | | | | | | |
| FORMU | LATION/S | TAND CO | DE: FORM | , | | | | | | | |
| OILCOD | E/CMIR: | OILCOL | DE/CMIR | | | - | | | | | |
| USAGE | DATES | W | DP | TC | 3C | т | c | | ORMED | TRANSF EO | ORMED |
| START | TIME | Zi | S.A. | Zi | S.A. | Zi | S.A. | Zi | S.A. | Zi | S.A. |
| DTSTROO1 | DTTMR001 | WDZIRO01 | WDSAR001 | TGZIA001 | TGSAR00 | 1 TLZIRO01 | TLSAR001 | OCZIRO01 | OCSAR001 | ETZIRO01 | ETSAR001 |
| | | | | | | | | | | | |
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| | | | | | | 1 | | | | | |
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FIG. A15.18 Severity Adjustment History



1P Form 16 FUEL BATCH ANALYSIS^A

| LAB: LAB | EOT DATE: DTCOMP | END TIME: EOTTIME | METHOD: METHOD |
|---------------------------|-------------------|-------------------|----------------|
| STAND: STAND | RUN NUMBER: ENRUN | | |
| FORMULATION/STAND CODE: | FORM | | |
| OIL CODE/CMIR: OILCODE/CM | TR . | | |

FUELIM

ARefer to Annex A14 for an example of a Fuel Batch Analysis page. Include a copy of the supplier fuel sheet in the test report.

FIG. A15.19 Fuel Batch Analysis

1P Form 17 TMC CONTROL CHART ANALYSIS^A (Reference Oil Test Only)

| LAB: LAB | EOT DATE: DTCOMP | END TIME: EOTTIME | METHOD: METHOD |
|---------------------------|-------------------|-------------------|----------------|
| STAND: STAND | RUN NUMBER: ENRUN | | |
| FORMULATION/STAND CODE: | FORM | | |
| OIL CODE/CMIR: OILCODE/CM | IR | | |

CCHIM

^ARefer to Annex A14 for an example of a TMC Control Chart Analysis. Include a copy of the TMC Control Chart Analysis in the test report.

FIG. A15.20 TMC Control Chart Analysis

A16. DATA DICTIONARY

A16.1 Fig. A16.1 presents the data dictionary.

| Description | 1P VERSION 19980921 BETA | METHOD CONDICTED FOR FIRST LINE | | ALIDA | STAND | ENGINE KON FING OF TREST TIME (UH:NA) | COMPLETED DATE (YYYYMMDD) | OIL CODE | CMIR | FORMULATION/STAND CODE | OIL CODE | ALIERNATE OIL CODE 2 ALTERNATE OIL CODE 3 | T | SUBMITTED BY: TESTING LABORATORY | BY: | BY: | SUBMITTED BY: TITLE | LAB CODE CEARTING DAME (VEXYMAND) | TOTAL TEST LENGTH (HHH) | IMC OIL CODE | LABORATORY INTERNAL OIL CODE | ENGINE SERIAL NUMBER | WEIGHTED TOTAL DEMERITS UNADJUSTED LAB RATING (DEMERITS) | TOP GROOVE CARBON UNADJUSTED LAB RATING (DEMERITS) | TOP LAND CARBON (DEMERITS) | LAB RATING OLL CONSUMPTION (9/11) | UNADJUSTED LAB RATING TRANSFORMED OIL CONSUMPT (TRANS UNITS) | UNADJUSTED LAB RATING TRANSFORMED ECTOC (TRANS UNITS) | INDUSTRY CORRECTION DATE (YYYYMMDD) | CORRECTION | CORRECTION | INDUSTRI CORRECTION TOP LAND CARBON (DEMERTES) INDUSTRY CORPECTION TRANSPORMED OTT. CONSTRUCTO (TRANS INTES) | CORRECTION TRANSFORMED ECTOC (TRANS UN | | CORRECTED TOP GROOVE CARBON (DEMERITS) | | CORRECTED TRANSFORMED OIL CONSUMPTION (TRANS UNITS) | CORRECTED TRANSFORMED ECTOC (TRANS UNITS) | SEVERITY ADJUSTMENT | SEVERITY ADJUSTMENT | SEVERITY ADJUSTMENT | SEVERITY ADJUSTMENT | TAB SEVERITY ADJUSTMENT TRANSFORMED OIL CONSUM (TRANS UNITS) | TWEET COOK ITTE | |
|----------------------------|--------------------------|---------------------------------|----------|-----------|-------|--|---------------------------|----------|------|------------------------|----------|---|---------|----------------------------------|----------|---------|---------------------|-----------------------------------|-------------------------|--------------|------------------------------|----------------------|--|--|----------------------------|-----------------------------------|--|---|-------------------------------------|------------|----------------|--|--|-------|--|----------|---|---|---------------------|---------------------|---------------------|---------------------|--|----------------------------|--|
| Units/Format | XXXXMMDD | | | V, I OR N | | nn.nn | XXXXMMDD | | | | | | | | | | | CUMPANA | HHH | ******* | | | DEMERITS | DEMERITS | DEMERITS | g/n | TRANS UNITS | TRANS UNITS | YYYYMMDD | DEMERITS | DEMERITS | DEMEKITS TOANS INTE | TRANS UNITS | | DEMERITS | DEMERITS | TRANS UNITS | TRANS UNITS | YYYYMMDD | DEMERITS | DEMERITS | DEMERTIS | TRANS UNITS | FIG. A16.1 Data Dictionary | |
| Data Type | υ i | υt | ט ט | υ | U | י נ | ט ט | υ | υ | υ i | U | ט נ | ບ | υ | υ | υ | υ i | υι |) k | ຸບ | v | υ | z | Z | z | 2; | zz | : 2 | ບ | Z | Z | 2 2 | 2 2 | z | Z | z | z | z | ပ | Z i | z | Z ; | z | 2 | |
| Dec. Size | 0 | 00 | 0 | 0 | 0 (| - | 0 | 0 | 0 | 0 (| 0 | > | 0 | 0 | 0 | 0 | 0 | > c | o c | · c | 0 | 0 | Н | c 4 | (1) | ٦ ، | m - | 4 (* | 0 | ~ | (4) | 74 M | ייי רי | , | c 4 | 61 | m | ო | 0 | н (| (4 (| :4 (| en (| า | |
| Field Length | ω (| N S | 40 | 1 | დ• | 4 R | , ω | 38 | 9 | 38 | 10 | 10 | 0 | 40 | 70 | 40 | 40 | :4 0 | יי ס | n ve | 12 | 11 | 7 | 9 | 91 | a (| n o | , ve | - ω | 7 | 9 | e u | o vo | , | 9 | 9 | 9 | 9 | ထ၊ | ۲ ، | φ· | ، م | ر م | Þ | |
| Field Fi Name Le | z | METHOD | TSTSPONZ | LABVALID | STAND | ENKON | DICOMP | OILCODE | CMIR | FORM | ALTCODE1 | ALTCODE2 | OPVALID | SUBLAB | SUBSIGIM | SUBNAME | SUBTITLE | LAB | TECTLEN | TND | LABOCODE | ENGSN | WD | TGC | TIC | ပ္ မ် | OCT | FOCE | DATECE | WDCF | TGCCF | | RTOCTOR | WDCOR | TGCCOR | TLCCOR | OCICOR | ETOCTCOR | DATESA | WDSA | TGCSA | TICSA | OCTSA | #C10013 | |
| | | | | | | | | | | | | | | | | | | ۸. ۵ | | . ^ | . n. | O. | ٥. | O. | <u>α</u> . ι | o. i | 1. 1.0 | υQ | . 0. | ٥. | ο. | n. r | . n | . n. | ٥. | n, | ۵ | ۵. | ٥. | _ | | | ۱ ۵۰ | . | |
| Test Area | 1.5 | 1 <u>P</u> | 15 15 | 11 | 1P | 4 F | 115 | 11 | 1. | 15 | 1P | 1 F | 1 1 | 1B | 1 P | 1P | 1P | d t | 1 - | 4 - | 115 | 1P | 1P | 1P | 1.5 | d : | - | 10 | : :: | 1P | 1. 1. 1. | 7 5 | 1 1 | 1.1 | 1. | 1P | 1 P | 1P | 1P | 1.5 | 1.5 | Du (| 1.P | 7 | |
| Test Sequence Form Area | | 0 1P | | 0 1P | | 0 TF | | 0 1P | 0 1P | 0 1P | | 0 15 | | 0 1P | 0 1P | | 0 1P | 1 | 1 - | 1 | | 1 11 | 1 11 | 1 11 | T . | · | | | 17 | 1 11 | 1 | T F | 1 - | 11 | 11 11 | 1 11 | 1 11 | 1 1: | 1 11 | 1 | 1 | | A : | i - | |

| Description | FINAL WEIGHTED TOTAL DEMERITS (DEMERITS) | FINAL TOP GROOVE CARBON (DEMERITS) | TOP LAND CARBON | OIL CONSUMPTION (g/h) | | FINAL BOTOC (g/h) FINAL FRANSFORMED FOTOC (TRANS INITS) | | TEST TARGET MEAN WEIGHTED TOTAL DEMERITS (DEMERITS) | TARGET MEAN | TARGET MEAN TOP LAND CARBON (DEMERITS) | TARGET MEAN | TARGET | TARGET STD | TARGET STD | TARGET STD TOP LAND CARBON (DEMERITS) | TAKGET STD | NON DEBEDENCE DASS TIME DEBECTIVE DAME (VOYCHAUD) | TASS MINIT REFERRED BORNE | WEIGHTED TOTAL DEMEKTES TOP GROOVE CARBON (DEMER | T.TMT.T | PASS LIMIT OIL CONSUMPTION | PASS LIMIT EOTOC (q/h) | S LIMIT | LAB CODE | REFEREE RATING WEIGHTED TOTAL DEMERITS (DEMERITS) | REFEREE RATING TOP GROOVE CARBON (DEMERITS) | REFEREE RATING TOP LAND CARBON (DEMERITS) | TOP KING SIDE CLEARANCE LSC (mm) | INI. I KING SIDE CLEARANCE LISC (MM) | OLL KING SIDE CLEARANCE LSC (mm) | RMEDI | OIL RING END GAP INCREASE (mm) | | THE | IS THE OIL RING STUCK? YES OR NO!! | AREA TOP (%) | AREA | AREA OIL (%) | PISTON | FISION SAIKI | AKEA LINEK (%) | -7 | | EOT QUALITY INDEX ENGINE SPEED AVG ENGINE SPEED (r/min) | LES ENG | parv (continued) |
|---------------------------|--|------------------------------------|-----------------|-----------------------|--------|--|------------|---|-------------|--|-------------|---------|------------|------------|---------------------------------------|------------|---|---------------------------|--|----------|----------------------------|------------------------|----------|---------------|---|---|---|----------------------------------|--------------------------------------|----------------------------------|-------------|--------------------------------|----------|----------|------------------------------------|--------------|----------|--------------|----------|--------------|----------------|------------|---------|--|---------------------|--|
| Data Type Inits/Rormat | | N DEMERITS | | d/b | | N g/h N TRANS INITES | | | | N DEMERITS | TRANS | - | | | N DEMERITS | TRANS | TKANS UNIT | | N DEMEKITS | | | | | | | | | | | | | N rom | υ | υ | U | N N | - | | op o | # (| ж Z ; | nun N | *° Z ; | N r/min | | FIG. A16.1 Data Dictionary (continued) |
| Dec. |) 1 ←1 | c⊲ | СI | H | ന | ⊣ (~ |) C | · | l (4 | СI | m | m | - | ঝ | ca c | m c | nο |) , | ⊣ ¢ | 1 C | ્ ⊢ | | 0 | 0 | Ţ | c⁄l | C1 (| m (| ന | n c | n m | m | 0 | 0 | 0 | 0 | 0 | 0 | 0 (| o 1 |) (| , (v. | ⊣ (| a) ← | 40 | |
| Field Landth | 7 | 9 | 9 | വ | Q | n u | > 00 | 7 | . ن | 9 | 9 | 9 | 7 | 9 | (O) | ه ی | ه د | o r | - u | o u | o ru | വ | ω | c -1 | 7 | 9 | 6 | ا وا | ا و | ا ف | o vo | 9 | | | | | | | | | | ، ب | 91 | | ~ ഗ | |
| Field | н | TGCFNL | TICENT | OCENE | OCTENE | EOTOCENE | E FEDATE | WDM | TGCM | ILCM | OCIM | EOTOCTM | WDS | IGCS | TICS | OCTS | EOTOCIES | DICERE. | WDPL | 1477 | OCPL | ROTOCPL | CATEGORY | RRLAB | RRWD | RRIGC | RRTLC | LSCTOP | LSCINT | LSCOIL | RINGGIL | RINGGOI | STUCKTOP | STUCKINI | STUCKOIL | SCUFFIOR | SCOFFINI | SCUFFOIL | SCUFCRON | SCUFSKRI | SCUFFLIN | AWEARST | BOREPOL | QRPM | ARFM | ! ! ! |
| Test | 1P | 15 | 1.P | 1₽ | ΤÞ | T 50 | ц <u>г</u> | 1 - | 1 4 | 1.P | 15 | 1.P | 1P | 15 | T. | д≀ | 그 . | À - - | H - | 4 F | η <u>μ</u> | <u>.</u> | ıμ | ΪÞ | ΙЪ | ΗF | 15 | 15 | I.P. | 1. 1. 1. | <u>т</u> н | 급 | 1.5 | 1.5 | 1.P | ΉÞ | 15 | 1.P | IΡ | Η | A. | Д. | ∐. | 다. 다. | 4 A | 1 |
| £ | | Η | П | H | r-d | ⊢ - | ⊢ | - ; | - ⊢ | H | Н | ∺ | H | ÷⁴ | , · | ⊣ , | ⊣ + | ⊣ , | | - | | ٠. | ı | 1 | П | Η | | ; · | | <u> </u> | | + ,→ | ₩ | ;I | \vdash | - | ₽Ħ | - | Η. | 1 | e | ~ 1 | 1 | сıс | 4 CI | 1 |
| | 510 | 520 | 530 | 540 | 550 | 560 | 0 / C | 000 | 009 | 610 | 620 | 630 | 640 | 650 | 660 | 670 | 089 | 0 v 0 | 700 | 770 | 730 | 740 | 750 | 760 | 770 | 780 | 790 | 800 | 810 | 820 | 0000 | 850 | 860 | 870 | 880 | 068 | 006 | 910 | 026 | 930 | 940 | 950 | 096 | 970 |) () () () |) } |

FIG. A16.1 Data Dictionary (continued)

| | Description | BOD ENGINE SPEED TOTAL DATA FOINTS OVER FINDER BANCE BACTAE SPEED TOTAL DATA DOTATS | INDEX | AVG FUEL FLOW (g/min) | SAMPLES FUEL FLOW TOTAL DATA POINTS | BOD FUEL FLOW TOTAL DATA POINTS | | EOT QUALITY INDEX HUMIDITY | LES HUMIE | BOD HUMIDITY TOTAL DATA POINTS | OVER/UNDER RANGE HUMIDITY TOTAL DATA POINTS | EOT QUALITY INDEX COOLANT FLOW | AVG COOLANT FLOW (L/min) | SAMPLES COOLANT FLOW TOTAL DATA POINTS DOD COOLANT FLOW TOTAL DATA DOINTS | OVER/UNDER RANGE COOLANT FLOW TOTAL DATA POINTS | EOT QUALITY INDEX COOLANT OUT | AVG COOLANT OUT (ØC) | SAMPLES COOLANT OUT TOTAL DATA POINTS | BOD COOLANT OUT TOTAL DATA POINTS | OVER/UNDER RANGE COOLANT OUT TOTAL DATA POINTS | EOT QUALITY INDEX OIL TO MANIFOLD TEMPERATURE | | SAMPLES OLL TO MANIFOLD TEMPERATURE TOTAL DATA FOLNTS | BOUND OLD TO MAINTEOLD TEMPERATORE LOTAL DATA FOLINGS OVER TINDER RANGE OTT. TO MANTFOLD TEMP. TOTAL DATA POINTS | ROT OUALTY INDEX INDEX TARE TEMPERATURE | AVG INLET AIR TEMPERATURE (ØC) | SAMPLES INLET AIR TEMPERATURE TOTAL DATA POINTS | BOD INLET AIR TEMPERATURE TOTAL DATA POINTS | OVER/UNDER RANGE INLET AIR TEMPERATURE TOTAL DATA POINTS | | AVERAGE FUEL & INJECTION HOUSING TEMP (SC.) SAMDLES WHEL & INJECTION HOUSING WEMP TOTAL DATA DOINTS | G INJECTOR HOUSING TEMP | OVER/UNDER RANGE FUEL GINJECTOR HOUSING TEMP TOTAL DATA POINT | EOT QUALITY INDEX OIL TO MANIFOLD PRESSURE | | SAMPLES OIL TO MANIFOLD PRESSURE TOTAL DATA POINTS | BOD OIL TO MANIFOLD PRESSURE TOTAL DATA POINTS | OVER/UNDER RANGE OIL TO MANIFOLD PRESSURE TOTAL DATA POINTS | EOT QUALITY INDEX INLET AIR PRESSURE | | | OVER/UNDER RANGE INLET AIR PRESSURE TOTAL DATA POINTS | EOT QUALITY INDEX EXHAUST PRESSURE | AVG EXHAUST PRESSURE (KPa) | A16.1 Data Dictionary (continued) |
|-------|-------------------|--|-------|-----------------------|-------------------------------------|---------------------------------|------------|----------------------------|-----------|--------------------------------|---|--------------------------------|--------------------------|--|---|-------------------------------|-----------------------|---------------------------------------|-----------------------------------|--|---|----------|---|--|---|---------------------------------|---|---|--|---------------------|--|-------------------------|---|--|---------|--|--|---|--------------------------------------|---------|---------|---|------------------------------------|----------------------------|-----------------------------------|
| ta | Type Units/Format | Z 2 | 2 2 | N g/min | Z | z | z ; | N a / bar | | Z | Z | N | N L/min | Z | . 2 | Z | N ØC | N | Z | Z | Z | N N | 2 2 | 2 2 | : 2 | N E | | N | N | | 2 Z | : Z | × | N | N ktPa | Z | Z | z | | | z z | z | z | N kPa | FIG. A16.1 Data Dict |
| | Φ | - · | | | 0 | | 5 (| ., (π | 4 0 | 0 | 0 | m | | 00 | | | н | | | 0 | m | ~ (| . | o c | o en | ٠ - | 0 | 0 | 0 | m, | c | 0 | 0 | e | -1 | 0 | 0 | 0 (| v) - | - C | 0 | 0 | o m | Н | _ |
| Field | Length | ņ | ٠ ٦ | 7 | S | ıcı | າດ | ى ~ | o ro | £ | , ro | 7 | 7 | ហេវ | ט גט | 7 | S | S. | ιO | S. | | | | | | - 10 | 5 | D. | | | | | | 7 | ø | ស | ഗ | ១០ | ~ u | o nu | , ro |) LO | 7 | 9 | |
| Field | Name | BRPM | OFFLO | AFFLO | NFFLO | BFFTO | OFFIG | QHOMID | NHOMID | BHUMID | OHUMID | OCOLFTO | ACOLFLO | NCOLFTO PCOT ETO | OCOLFLO | OCOLOUT | ACOLOUT | NCOLOUT | BCOLOUT | OCOTOOL | QOMANTMP | AOMANTMP | NOMANTME | DOMANTME | OTNATRT | AINAIRI | NINAIRT | BINAIRT | OINAIRT | QFUELTMP | AFUELTMP | BFUELTME | OFUELTMP | QOMANPR | AOMANPR | NOMANPR | BOMANPR | OOMANPR | QINAIRP | NTNATRE | BINAIRP | OINAIRP | QEBP | AEBP | |
| Test | Area | 1 F | 15 | 11 | 1.P | 1P | 러 : | H E | 1 E | 115 | 115 | 1.5 | 119 | 1 1 1 1 1 | 1 E | 15 | 15 | 1.P | 15 | 1P | 1 P | 다. | IP u | - F | 1 [| H H | 1P | 1P | 1P | 115 | 1 F | 1 [| 1.P | 1P | JЪ | 1B | 1.P | Н Н | IP of | 4 F | 1E | 15 15 | 1P | 11 | |
| ı | Form | N C | 4 (4 | (4 | CΙ | CI (| বে (| 54 C | 1 (1 | N | 121 | СI | c ⊲ | ca c | ા લ | C) | СI | Сd | Ø | લ | CΙ | (व (| (4 c | 40 | 1 (| 1 (4 | N | N | C4 | c 4 c | 0 C | 1 C4 | ı | Ø | Ø | C4 | C4 | C1 (| 9 C | 4 (| 1 (1 | 1 (4 | 1 (4 | 7 | |
| ı | Sequence Form | 1010 | 1020 | 1030 | 1040 | 1050 | 1060 | 10/0 | 1090 | 1100 | 1110 | 1120 | 1130 | 1140 | 1160 | 1170 | 1180 | 1190 | 1200 | 1210 | 1220 | 1230 | 1240 | 1260 | 1270 | 1280 | 1290 | 1300 | 1310 | 1320 | 1330 | 1350 | 1360 | 1370 | 1380 | 1390 | 1400 | 1410 | 1420 | 1430 | 1450 | 1460 | 1470 | 1480 | |

| | Description | SAMELES EARAGOI FALSSORE LOIAL DAIR FOINTS DOD EXHALIST DEFECTIVE TOTAL DATA DOTNIES | BOD EARTHOST FARSSONE TOTAL DATA FOINTS OVER/UNDER RANGE EXHAUST PRESSURE TOTAL DATA POINTS | EOT QUALITY INDEX FUEL @ FILTER HOUSING PRESSURE | AVG FUEL @ FILTER HOUSING PRESSURE (KPa) | SAMPLES FUEL @ FILTER HOUSING PRESSURE TOTAL DATA POINTS BOD FURT, @ FILTER HOUSING PRESSURE TOTAL DATA POINTS | OVER/UNDER FUEL @ FILTER HOUSING PRESSURE TOTAL DATA POINTS | AVG INTAKE AIR FLOW (kg/h) | AVG ENGINE POWER (KM) | SAMPLES ENGINE POWER TOTAL DATA POINTS | BOD ENGINE FOWER TOTAL DATA FOINTS OVER /INDER RANGE ENGINE DOWER TOTAL DATA POINTS | AVG TORQUE (Nm) | | | | AVG BLOWBY (L/MLN) SAMPIES BLOWBY TOTAL DATA POINTS | BOD BLOWBY TOTAL DATA POINTS | OVER/UNDER RANGE BLOWBY TOTAL DATA POINTS | AVG COOLANT IN (ØC) | SAMPLES COOLANT IN TOTAL DATA POINTS | BOD COOLANT IN TOTAL DATA FOINTS OVER/INDER RANGE COOLANT IN TOTAL DATA POINTS | AVG COOLANT DELITA (ØC) | SAMPLES COOLANT DELTA TOTAL DATA POINTS | BQD COOLANT DELTA TOTAL DATA POINTS | OVER/UNDER RANGE COOLANT DELIA TOTAL DATA FOINTS | SAMPLES OIL COOLER IN TEMPERATURE TOTAL DATA POINTS | BOD OIL COOLER IN TEMPERATURE TOTAL DATA POINTS | OVER/UNDER RANGE OIL COOLER IN TEMPERATURE TOTAL DATA POINTS | AVG HEATING OIL TEMPERATURE (ØC) | SAMFLES HEALING OLD LEMFERALORE LOIAU DAIA FOLNES ROD HEATING OII, TEMPERATURE TOTAI, DATA POINTS | OVER/UNDER RANGE HEATING OIL TEMPERATURE TOTAL DATA POINTS | AVG EXHAUST TEMPERATURE (ØC) | SAMPLES EXHAUST TEMPERATURE TOTAL DATA POINTS | BOD EXHAUST TEMPERATURE TOTAL DATA POINTS | SOURT CONTROL FANGE EXHAUST TEMPERATURE TOTAL DATA FOINTS | AVG CRANKCASE VACUUM PRESSURE (REA) SAMPTES CRANKCASE VACUUM PRESSURE TOTAL DATA POINTS | BOD CRANKCASE VACUUM PRESSURE TOTAL DATA POINTS | OVER/UNDER RANGE CRANKCASE VACUUM PRESSURE TOTAL DATA POINTS | AVG COOLANT TO JUG (kPa) | SAMPLES COOLANT TO JUG TOTAL DATA POINTS | BOD COOLANT TO JUG TOTAL DATA POINTS | OVER/UNDER RANGE COOLANT TO JUG TOTAL DATA POINTS | onary (continued) |
|-------|---------------|---|---|--|--|---|---|----------------------------|-----------------------|--|---|-----------------|------------|---------|------------|--|------------------------------|---|----------------------|--------------------------------------|---|--------------------------|---|-------------------------------------|--|---|---|--|-----------------------------------|--|--|-------------------------------|---|---|---|--|---|--|--------------------------|--|--------------------------------------|---|--|
| | Units/Format | | | | kPa | | | kg/h | K | | | Nm | | | * /: | L/min | | | Dø. | | | Ď | | | ر | Š. | | | S S | | | Ď | | | | K Pa | | | kPa | | | | FIG. A16.1 Data Dictionary (continued) |
| Data | Type | Z 2 | zz | z | Z | Z 2 | z | Z | Z | Z | 2 2 | z | z | Z | z | Z | z | N | Z | z | Z 2 | z | Z | Z | 2 2 | 2 2 | z | z | z | 2 2 | z | Z | Z | Z; | Z ; | 2 2 | Z | Z | Z | Z | Z | Z | Ë |
| Dec. | Size | > | 0 | m | Н | 0 0 | 0 | H | Н | 0 | 0 0 | o ⊷ | 0 | 0 | o , | - C | 0 | 0 | ᆏ | 0 (| o c | · | 0 | 0 | 0 - | - 0 | 0 | 0 | (| - | 0 | - | 0 | 0 |) | N C | 0 | 0 | Н | 0 | 0 | 0 | |
| Field | Length | വ | ດມດ | 7 | 9 | വവ | υ c | 7 | 9 | rO. | v r | ۲ | S | ខា | s (| ១៤ | , ro | ß | വ | ഥ | n u | വ | ß | ß | | | | | _ | n 10 | | 9 | 2 | LO I | Ω. | ប្រ | വ | S | വ | S | r. | വ | |
| Field | | NEBP | BEBP ORBP | QFUELPR | AFUELPR | NEUELPR | OFUELPR | AAIRFLO | APWR | NPWR | BPWR | ATOROUE | NTORQUE | BTORQUE | OTORQUE | ABLOBY | BBLOBY | OBLOBY | ACOLIN | NCOLIN | BCOLIN | ACOLDI | NCOLDT | BCOLDT | OCOLDI ACCOL IN | NOCOOL IN | BOCOOLIN | OOCOOLIN | AHEATOIL | DHEATOIL | OHEATOIL | AEXHTMP | NEXHTMP | BEXHTMP | OEXHIMP | ACCV | BCCV | OCCV | ACOLPR | NCOLPR | BCOLPR | OCOLPR | |
| Test | Area | 4 5 | - - - - | 11 | 11 | 1P | 15 15 | 11 | 115 | 1 P | 1P | 1 E | 1 <u>P</u> | 115 | 1F | IP or | 115 | 115 | 115 | 1Þ | 1P | 1 # | 1P | 1P | H : | 1 t | 1 # | 1P | 1 <u>P</u> | IP C | 15 15 | 1P | 115 | I. | E I | 4 t | 15 | 11 | 115 | 11 | 11 | 1P | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Sequence Form | 74 C | N C | 1 (1 | C 4 | 01 C | 1 (1 | N | C/I | (4 | (4 C | 4 (4 | N | ca : | (4) | (A) (c) | 1 (4 | N | N | C4 (| ca c | 1 (1 | C/1 | C/I | C4 C | 40 | 1 (4 | C-1 | C4 (| rd r | 1 (1 | c 4 | C/I | C4 (| K1 (| (4 C | 1 (4 | 1 (4) | (4 | Ø | N | C/I | |

70

| Description | INJECTOR SETTING (GO / NO-GO) | WAS TIMING INITIALIZED ? (YES / NO) | | LASH (| FUEL TIMING (Ø BTC) | INTAKE VALVE OPEN (Ø ATC) INTECTOD DIINGED LIET (mm) | INCECTOR FIRM (mm) | EXHAUST VALVE LIET (mm) | LINER PART NUMBER | LINER SERIAL NUMBER | LINER DATE CODE | | | INTERMEDIATE RING SET PART NUMBER | | | | PISTON CROWN SERIAL NUMBER | PISTON CROWN DATE CODE | CROWN | | PISTON SKIRT SERIAL NUMBER | FUEL NOZZIE FRAI NUMBER | ECH EPROM PART NUMBER | ECM EPROM DATE CODE | PISTON COOLING JET PART NUMBER | PISTON COOLING JET SERIAL NUMBER | TEST FUEL | | RATING DATE (IIIMMUD) | VERIFIED BY INITIALS | LAST STAND REFERENCE DATE COMPLETED (YYYYMADD) | STAND REFERENCE RUN | STAND | LASI SIAND REFERENCE TOTAL MELGRIED DEMENTES (DEMENTES) | STAND REFERENCE EOTOC (g/km-h) | STAND REFERENCE INDUSTRY AVG WDK | STAND REFERENCE INDUSTRY AVG TGC | LAST STAND REFERENCE INDUSTRY AVG TAC (DEMEKTIS) | | |
|---------------------------|-------------------------------|-------------------------------------|----------|---------|---------------------|--|--------------------|-------------------------|-------------------|---------------------|-----------------|------------|-------|-----------------------------------|---------------|-------|---------|----------------------------|------------------------|---------|---------|----------------------------|-------------------------|-----------------------|---------------------|--------------------------------|----------------------------------|-----------|----------|-----------------------|----------------------|--|---------------------|-------|---|-----------------|-----------------|-----------------|-----------------|--------------------------------|----------------------------------|----------------------------------|--|---------------------------------------|--|
| Data Twoe Units/Format | | | N mm | Hall | | N Ø ATC | TIMIL N | | | υ | U | υ | U | ບເ | ט נ |) t |) U | U | v | υ | υ | U (| υt | ט נ | υ | υ | υ | υ | O | CXXXXMMDD | ນ ບ | C YYYYMMDD | υ | | N DEMEKTIS | | _ | - | | | | | N DEMEKTI'S | FIG A16 1 Data Dictionary (continued) | |
| Dec. | 2 | 0 | က | ۲۷ | 0 | 0 1 | י רי | n m | 0 | 0 | 0 | 0 | 0 | 0 0 | > C | o c | 0 | 0 | 0 | 0 | 0 | 0 (| > C | 0 | 0 | 0 | 0 | 0 | 0 0 | > | 0 | 0 | 0 | 0 , | ⊣ (| 1 C | 1 ⊶ | ю | ო | - | ~ -1 | C4 C | 34 C | ו | |
| Field Length | | ო | 9 | 9 | m | m 4 | ט פ | 9 V2 | 12 | 12 | 12 | 12 | 13 | 25 | 7 - 1 |) C- | 1 2 | 12 | 12 | 12 | 12 | 12 | 7 - | 2 C | 12 | 12 | 12 | 10 | 10 | ∞ " | n m | ω | 4 | (O) | ه د | o vo | , ro | 9 | 9 | വ | 9 | v v | שפ | • | |
| Field I | E- | TINIT | PISTONCE | CAMLASH | FUELTIM | INVALOPN | TATTET | EXT.TFT | LINERPN | LINERSN | LINERDC | TOPPN | TOPSN | NTL | NETRIC | OTTEN | CROWNEN | CROWNSN | CROWNDC | CROWNIC | SKIRTPN | SKIRTSN | NOZZLEPN | RCMPN | ECMDC | PTUBEPN | PTUBESN | TESTFUEL | FUELBIID | DIKATE | VRINIT | LRDTCOMP | LRENRUN | LIND | LKWD | TRITIC | LROC | LROCT | LRETOCT | LREOTOC | LRAWD | LRAIGC | LRATIC | 100001 | |
| Test | 10 | 11 | 11 | 1P | 1 <u>P</u> | 1P | 4 F | 1 1 | 15 | 15 15 | 1B | 1 P | 1B | 15 | 4 5 | 11. | 15 | 15 | 1P | 1P | 1P | 1. 1. 1. 1. | - F | 1 F | 1.1 | 11 | 11 | 1P | 1P | 4 t | 15 | 1P | 11P | 1P | 4 t | 1 F | 15 15 | 1P | 1 <u>P</u> | 1P | 1 P | 15 | 1 P | 4 4 | |
| E C | #OF. | ო | m | m | ო | m r | n 0 | n r | , m | m | m | m | က | m (| יז מי | י ר | n m | m | m | ო | ო | m | יז רי | n m | m | m | ო | 4 | 4 | 4 < | . 4 | 4 | 4 | 4. | ₫ 4 | # 4 | 4 | 4 | 4 | 4 | 4 | ♥ • | 4. | r | |
| gonolipas | 1980 | 1990 | 2000 | 2010 | 2020 | 2030 | 0407 | 2060 | 2070 | 2080 | 2090 | 2100 | 2110 | 2120 | 2130 | 2150 | 2160 | 2170 | 2180 | 2190 | 2200 | 2210 | 0777 | 2240 | 2250 | 2260 | 2270 | 2280 | 2290 | 2300 | 2320 | 2330 | 2340 | 2350 | 2360 | 2380 | 2390 | 2400 | 2410 | 2420 | 2430 | 2440 | 2450 | 00 % | |

71

| Description Tast stath Reference Indistry AUG TRANS ROTOC (TRANS UNITS) | STAND REFERENCE INDUSTRY STD WDK (DEMERIT | LAST STAND REFERENCE INDUSTRY STD IGC (DEMERITS) | STAND REFERENCE INDUSTRY STD | LAST STAND REFERENCE INDUSTRY STD TRANS ECTOC (TRANS UNITS) GROOVE #1 HC-1.0 CARBON AREA PERCENT (% AREA) | GROOVE #1 HC-1.0 CARBON DEMERITS (DEMERITS) | GROOVE #2 HC-1.0 CARBON AREA PERCENT (% AREA) | | #1 HC-1.0 CARBON | LAND #1 HC-1.0 CARBON DEMERTIS (DEMERTIS) TAND #2 HC-1.0 CARBON AREA DERCENT (% AREA) | # | | GROOVE #3 HC-1.0 CARBON DEMERITS (DEMERITS) | LAND #3 HC-1.0 CARBON AREA FERCEN! (\$ AREA) | | #4 | GROOVE #1 MC-1.0 CARBON AREA PERCENT (% AREA) | | #3 MC-1.0 CARBON | GROOVE #3 MC-I.O CARBON DEMERITS (DEMERITS) | #1 LC-1.0 | GROOVE #2 LC-1.0 CARBON AREA PERCENT (% AREA) | GROOVE #2 LC-1.0 CARBON DEMERITS (DEMERITS) | | LAND #I IC-I.O CARBON DEMERITS (DEMERITS) | #2 LC-1.0 CARBON | | GROOVE #3 LC-1.0 CARBON DEMERITS (DEMERITS) | LAND #3 IC-1.0 CARBON AREA PERCENT (% AREA) | #4 IC-1 O CARBON | #4 | COLING | OIL COOLING GALLERY LC25 CARBON DEMERITS (DEMERITS) | | UNDER CROWN IC25 CARBON DEMERITS (DEMERITS) | GROOVE #1 CARBON DEMERITS (DEM | GROOVE #2 CARBON | | LAND #1 CARBON AREA PERC | TOTAL LAND #1 CAKBON DEWEKIIS (DEMEKIIS) TOTAL LAND #2 CARBON AREA PERCENT (% AREA) | nary (continued) |
|--|---|--|------------------------------|---|---|---|------------|------------------|--|------------|-------|---|--|-------|----------|---|-------|------------------|---|-----------|---|---|-------|---|------------------|-------|---|---|------------------------|-------|--------|---|-------|---|--------------------------------|------------------|------------|--------------------------|---|--|
| Data Type Units/Format | DEMERI | N DEMERITS N DEMERITS | TRANS | N TRANS UNITS N % AREA | N DEMERITS | N % AREA | | N % AREA | N DEMERTIES N * ARRA | N DEMERITS | | | N & AKEA | - | | | E . | N & AREA | N DEMERTIES N * APEA | | N & AREA | 집 | | N DEMERITS | | | | N & AREA | N & APPA | | | | | N DEMERITS | • <u>F</u> | | N DEMERITS | | N & AREA | FIG. A16.1 Data Dictionary (continued) |
| Dec. Size |) | ा ० | ım | m C | c 4 | 0 | c 4 | 0 (| NG |) (c) | 0 | c a e | ⊃ ເ | ч С | ্ৰ | 0 | C-1 | 0 (| N C | ં | 0 | c1 | 0 (| ra ⊂ | ⊃ (1 | 0 | cı | 0 (| d € | · (4) | 0 | сı | 0 | () C | o (< | 0 | СI | 0 (| 40 | |
| Field Length | 9 0 | w w | 9 | O 4 | - 1 | 4 | 7 | 4 7° (| ~ 4 | 7 | 4 | ۲. | 3" [| ~ 4 | | 4 | 7 | 41 | ~ < | | 4 | 7 | 4 | | # [~ | 4 | 7 | 4.1 | ~ < | 7 | 4 | 7 | 4 | L « | , , | 4 | 7 | 4.1 | , 4 | |
| Field F Name I | LRSWD | LRSTGC | LRSOCT | LRSETOCT | GIHCD | GZHCA | GZHCD | LIHCA | LIMCD | LZHCD | G3HCA | G3HCD | LSHCA | L3HCD | L4HCD | GIMCA | GIMCD | G3MCA | GSMCD | GILCD | GZLCA | GELCD | LILCA | Lilco | LICO | GBLCA | GSICD | LSLCA | 1.41.02 | L4LCD | OGLCA | OCICD | UCICA | UCICD | GIDCTOT | GZACTOT | G2DCTOT | LIACTOT | LIDCTOL | |
| Test Area | 4 4 | 1P | 1 F | 1.P | 115 | 11 | 1P | 1. 1. 1. | д Д | 4 | 1P | 1.5 | ન ÷ | 4 F | 1. 1. | 1.P | 1₽ | <u>Д</u> | H H | I I | 1.P | 1.5 | 1P | di f | Д. Д. | 1 P | 1 P | 1P | 4 1 | i i | 1.P | 1. | | 다. 다. | 4 A | | 1P | 1.5 | 4 T. | |
| Form | 4 4 | 4 4 | 4 4 | 4 4 | 4 | 4 | 4 | 4. | 4 4 | 7 | 4 | 4. | 4. | 4 4 | 7 | 4 | 4 | 4. | 4 < | 7 | 4 | 4 | 4 | 4.4 | 4 4 | 4 | 4 | 4 | 7 5 | 4 4 | 4 | 4 | 4 | 4 - | r 4 | 4 | 4 | 4 | 7 7 | |
| Seguence | 2480 | 4 ቢ | 2510 | 2520 | 2540 | 2550 | 2560 | 2570 | 2580 | 2600 | 2610 | 2620 | 2630 2630 | 2650 | 2660 | 2670 | 2680 | 2690 | 2700 | 2720 | 2730 | 2740 | 2750 | 2760 | 2780 | 2790 | 2800 | 2810 | 0 7 8 7 0 3 8 8 9 0 | 2840 | 2850 | 2860 | 2870 | 2880 | 2900 | 2910 | 2920 | 2930 | 2940 2950 | |

72

| | Description | TOTAL LAND #2 CARBON DEMERITS (DEMERITS) | TOTAL GROOVE #3 CARBON AREA PERCENT (% AREA) | GROOVE #3 CARBON DEMERITS (I | LAND #3 | LAND #3 | TOTAL LAND #4 CARBON AREA PERCENT (* AREA) TOTAL TAND #4 CARBON DEMENTES (DEMENTES) | OTT. | | | TOTAL UNDER CROWN CARBON DEMERITS (DEMERITS) | #1 | | | GROOVE #2 8-9 VARNISH DEMERITS (DEMERITS) | | #2 8-9 VARNISH | #2 | | 7-7.9 VARNISH | | GROOVE #2 7-7.9 VARNISH DEMERITS (DEMERITS) | | # # | #2 | GROOVE #3 7.5 VARNISH AREA PERCENT (% AREA) | | LAND #3 /.3 VAKNISH AKEA FERCENI (* AKEA) IAND #3 7 5 VARNISH DEMORPTS (DEMERITS) | #4 7.5 | #4 7.5 VARNISH | GALLERY | _ | UNDER CROWN /.5 VARNISH AREA PERCENT (% AREA) | A.S VAKNISH | #1 6-6.9 VARNISH | #2 6-6.9 VARNISH | GROOVE #2 6-6.9 VARNISH DEMERITS (DEMERITS) | #1 6-6.9 VARNISH AREA PERC | #1 6- | #2 6-6.9 VARNISH AREA PERC | <u>.</u> و | #: | | GROOVE #2 3-3.9 VAKNISH AKEA PEKCENI (* AKEA) CDOOVE #2 5-5 9 VARNISH DEWERITS (DEMERITS) | 7 | y (continued) |
|-----------|----------------|--|--|------------------------------|---------|----------|---|---------|----------|---------|--|------------|----------|----------|---|----------------------|----------------|----------|----------|---------------|-------------|---|----------------|------------|-------|---|------------|--|------------|----------------|----------|----------|---|------------------------|------------------|------------------|---|----------------------------|-------|----------------------------|------------|----------|---------|--|-----------|--|
| roj | e Units/Format | DEMERITS | & AREA | | | DEMERITS | * AREA | S AREA | DEMERITS | 8 AREA | DEMERITS | I & AREA | DEMERITS | I & AREA | DEMERITS | F AKEA I DEMERITS | S AREA | DEMERITS | I & AREA | DEMERITS | I & AREA | DEMERITS | F AKEA | | | 1 & AREA | | A & AKEA I DEMEDITE | | | V & AREA | DEMERITS | N * AREA | N DEMEKLIS N 9 ADEM | N DEMERITS | V & AREA | N DEMERITS | N & AREA | | | | | | N & AKEA N DEMEDITE | N DEMENTS | FIG. A16.1 Data Dictionary (continued) |
| Dec. Data | Size Type | Z N | 0 | | 0 | Z . | 2 2 | 12 |) (N | 0 | 7 Z | Z | C) | Z | Z 2 | 2 2 | 10 | i Z | 0 | C1 | 0 | N C | 2 Z | : Z | . C1 | 0 | 2 ; | 2 Z | 10 | | 0 | Z (| | | | 10 | | 0 | | | | | (4) | | - i | FIG. |
| ield | ength | 7 | 4 | 7 | 4 | 7 | 4. | - 4 | 7 | 4 | 7 | 4 | 7 | 4 | | 4 1 | 4 | 7 | 4 | 7 | 4 11 | ٠, | 4 L | - 4 | 7 | 4 | ۲, | 4 1 | ~ 🔻 | | 4 | 7 | 4 1.14 | ~ < | * [- | · 47 | 7 | 4 | 7 | ♥ : | 7 | † | _ " | 41 [| • | |
| Field F | Name L | L2DCTOT | GSACTOT | G3DCTOT | L3ACTOT | L3DCTOT | LAACTOT | OGACTOT | OGDCTOT | UCACTOT | UCDCTOT | G1V9A | G1V9D | G2V9A | G2V9D | L1V9D | T.2V9A | L2V9D | G1V8A | G1V8D | G2V8A | G2V8D | L1V8A | L2V8A | L2V8D | G3V75A | G3V75D | L3V/5A | 1.4V75A | L4V75D | OGV75A | OGV75D | UCV/5A | 000/130 | GIVID | G2V7A | G2V7D | L1V7A | L1V7D | L2V7A | L2V7D | GIV6A | GIV6D | GZV6A | 70,75 | |
| Test | Area | 1P | 1P | 11 | 15 | 1.5 | 1P | 1 L | 14 | 1P | 1 P | 1 P | 1P | 1P | 15 | 4 5 | 11 1D | 14 | 1P | 1P | 1 <u>P</u> | 15 15 | 1 t | 1 <u>1</u> | 1P | 1.5 | 1P | 4 F | ц <u>С</u> | 1.P | 11 | 15 | T F | 1 F | 4 C | Н Н | 1P | 1. | 1P | 1.5 | 1.P | 1. | IP T | 4 t | 41 | |
| | Form | 4 | 4 | 4 | 4 | 4 | 4 < | * 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4.4 | ₹ 5 | 7 | 4 | 4 | 4 | বা ' | 4 | 7 7 | * 4 | 4 | 4 | 4 | 4 < | r 7 | 4 | Ą | 4 | 4 4 | 4 - | * 4 | 4 | 4 | 4 | 4 | 4 | 4. | 4 | 4. | # < | 4 | |
| | Sequence | 2960 | 2970 | 2980 | 2990 | 3000 | 3010 | 3020 | 3040 | 3050 | 3060 | 3070 | 3080 | 3090 | 3100 | 3110 | 3130 | 3140 | 3150 | 3160 | 3170 | 3180 | 3200 | 3210 | 3220 | 3230 | 3240 | 3250 | 3270 | 3280 | 3290 | 3300 | 3310 | 3320 | 3340 | 3350 | 3360 | 3370 | 3380 | 3390 | 3400 | 3410 | 3420 | 3430 | † † | |

| ciption #1 5-5.9 VARNISH AREA PERC | LAND #1 5-5.9 VARNISH DEMERITS (DEMERITS) | #2 5-5.9 | 4-4.9 | GROOVE #1 4-4.9 VARNISH DEMERITS (DEMERITS) | # 2 | LAND #1 4-4.9 VARNISH AREA PERCENT (% AREA) | #1 4-4.9 | LAND #2 4-4.9 VARNISH AREA PERCENT (% AREA) | LAND #2 4-4.9 VARNISH DEMEKTIS (DEMEKTIS) GROOVE #3 4.5 VARNISH AREA PERCENT (% AREA) | GROOVE #3 4.5 VARNISH DEMERITS (DEMERITS) | #3 4.5 VARNISH | LAND #3 4.5 VARNISH DEMERITS (DEMERITS) | 4.5 VARNISH | GALLERY | OIL COOLING GALLERY 4.5 VARNISH DEMERITS (DEMERITS) | 4.5 VARNISH | | #1 3-3.9 VARNISH | GROOVE #1 3-3.9 VARNISH DEMERITS (DEMERITS) | 4 ¢ ≠ # | į ψ | #1 | | ۲ ۳ | GROOVE #1 2-2 VARNISH AREA PERCENT (* AREA) GROOVE #1 2-2 9 VARNISH DEMERITS (DRMERITS) | # # | #2 | | | LAND #2 2-2.9 VARNISH AKEA PERCENT (* AKEA) TAND #2 2-2 G WADNISH DEWEDTTS (DEMEDITS) | GROOVE #1 1-1.9 VARNISH ARRA PERCENT (% ARRA) | | GROOVE #2 1-1.9 VARNISH AREA PERCENT (% AREA) | GROOVE #2 1-1.9 VARNISH DEMERITS (DEMERITS) | LAND #1 1-1.9 VARNISH AREA PERCENT (* AREA) | | | | GROOVE #3 1.5 VARNISH AREA PERCENI (* AREA) GROOVE #3 1.5 VARNISH DEMERITS (DEMERITS) | 1.5 VARNISH AR | (population) |
|---------------------------------------|---|--------------------|--------|---|----------|---|----------|---|--|---|----------------|---|--------------------|---------|---|-------------|------------|------------------|---|-------------|--------|------------|--------|--------------|--|--------|------------|--------|----------|--|---|----------|---|---|---|----------|---------------|----------|--|----------------|-------------------|
| | DEMERITS | * AKEA DEMERITS | % AREA | DEMERITS | DEMERITS | & AREA | DEMERITS | & AREA | DEMEKITS % AREA | DEMERITS | % AREA | DEMERITS | 5 ANEA DEMESTES | 8 AREA | DEMERITS | & AREA | DEMERITS | 8 AREA | DEMERITS | * AKEA | % AREA | DEMERITS | % AREA | DEMERITS | * AKEA | 8 AREA | DEMERITS | 8 AREA | DEMERITS | * AKEA | PERIENTS S AREA | DEMERITS | & AREA | DEMERITS | & AREA | DEMERITS | & AREA | DEMERITS | * AREA | & AREA | 1 Data Dictionary |
| Data Type N | z | zz | Z | Z | 2 2 | Z | Z | z | zz | Z | Z | Z; | 2 2 | z | Z | Z | z | z | z | 2 2 | : Z | z | z | Z; | 2 2 | 2 2 | Z | Z | z | 2 2 | 2 2 | z | z | Z | Z | z | z | z | Z 2 | Z | =IG A16 |
| Dec. Size | (1) |) (| 0 | (1 C |) (4 | 0 | (1 | 0 (| N C | c 4 | 0 | (4) | ⊃ (· | 10 | · (4 | 0 | C 4 | 0 | (1) |) c | 10 | C 4 | 0 | c 4 0 |) c | 10 | (4 | 0 | (1) | o r | 4 C | 6 (4 | 0 | থে | 0 1 | C) (| 0 (| (4 C | o 6 | 10 | _ |
| Field Length | 7 | 4 / | 4 | r • | r / | 4 | 7 | 4,1 | - 4 | 7 | 4 | ۲. | # F | - 4 | 7 | 4 | 7 | 4 | ۲. | 4 1 | - 4 | 7 | 4 | ۲. | 4 L | - 4 | 7 | 7 | ۲. | 4 , (| ~ 4 | , , | 4 | 7 | 47' ∣ | 7 | ⊲ †' [| | 4 C | . 4 | |
| Field Name LlV6A | L1V6D | L2V6D | GIV5A | G1V5D | G2V5D | L1V5A | LIV5D | L2V5A | L2V5D G3V45A | G3V45D | L3V45A | L3V45D | 14745A | OGV45A | OGV45D | UCV45A | UCV45D | G1V4A | G1V4D | G2V4A | LIV4A | L1V4D | L2V4A | L2V4D | GIV3A | G2V3A | G2V3D | L1V3A | LIV3D | LZV3A TOTTO | 12√3D ⊄1√2A | GIV2D | G2V2A | G2V2D | LIVZA | LIV2D | LZVZA | L2V2D | G3V15A | L3V15A | |
| Test Area 1P | 1P | 1 E | 1. | 1P | 15 15 | 1P | 1. | 1.P | IP G | 1.P | 11 | 1 <u>P</u> | 4 5 | 1 1 | 1.P | 1P | 1P | 1F | 1P | 1 t | 1P | 1.5 | 1. | 1. 1. | IP d | 1 F | 1 P | 1P | 1. 1. | I L | 1 F | 1 1 | 1.P | 1.P | 15 | 1.5 | 1P | 15 | 4 t | 1 <u>P</u> | |
| Form 4 | ₹ ₹ | 4 4 | 4 | 4. | . 4 | 4 | 4 | 4 | 4 4 | 4 44 | 4 | ♥・ | # < | r 4 | 4 | 47 | 4 | 4 | 4. | 4. 2 | r 4 | 4 | 4 | 4. | 4 < | 1 4 | 4 | 4 | 4 | 4. 4 | # ₹ | 7 | 4 | 4 | 4 | 4 | 7 - | 4 - | ক ব | 7 | |
| | 91 | 34/0 | 3490 | 3500 | 3520 | 3530 | 3540 | 3550 | 3560 | 3580 | 3590 | 3600 | 3610 | 3630 | 3640 | 3650 | 3660 | 3670 | 3680 | 3590 | 3710 | 3720 | 3730 | 3740 | 3750 | 3770 | 3780 | 3790 | 3800 | 3810 | 3830 | 3840 | 8 | 3860 | 3870 | 3880 | 3890 | 3900 | 3910 | 3930 | |

FIG. A16.1 Data Dictionary (continued)

| Description LAND #3 1.5 VARNISH DEMERITS (DEMERITS) LAND #4 1.5 VARNISH AREA PERCENT (% AREA) LIAND #4 1.5 VARNISH DEMERITS (DEMERITS) OIL COOLING GALLERY 1.5 VARNISH AREA PERCENT (% AREA) OIL COOLING GALLERY 1.5 VARNISH DEMERITS (DEMERITS) UNDER CROWN 1.5 VARNISH AREA PERCENT (% AREA) UNDER CROWN 1.5 VARNISH DEMERITS (DEMERITS) | GROOVE #1 0-0.9 VARNISH AREA PERCENI (# AREA) GROOVE #1 0-0.9 VARNISH AREA PERCENI (# AREA) GROOVE #2 0-0.9 VARNISH AREA PERCENT (# AREA) GROOVE #2 0-0.9 VARNISH AREA PERCENT (# AREA) LAND #1 0-0.9 VARNISH AREA PERCENT (# AREA) LAND #2 0-0.9 VARNISH AREA PERCENT (# AREA) LAND #2 0-0.9 VARNISH AREA PERCENT (# AREA) LAND #2 0-0.9 VARNISH AREA PERCENT (# AREA) GROOVE #1 CLEAN VARNISH AREA PERCENT (# AREA) GROOVE #1 CLEAN VARNISH AREA PERCENT (# AREA) LAND #1 CLEAN VARNISH AREA PERCENT (# AREA) GROOVE #2 CLEAN VARNISH AREA PERCENT (# AREA) LAND #3 CLEAN VARNISH AREA PERCENT (# AREA) GROOVE #3 CLEAN VARNISH AREA PERCENT (# AREA) GROOVE #3 CLEAN VARNISH AREA PERCENT (# AREA) LAND #3 CLEAN VARNISH AREA PERCENT (# AREA) LAND #4 CLEAN VARNISH AREA PERCENT (# AREA) | | |
|--|---|--|---|
| Data Type Units/Format N DEMERITS N % AREA N DEMERITS N % AREA N DEMERITS N % AREA N DEMERITS | N | | 746 |
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| Field Length 7 7 7 7 4 4 4 | みてみてみてみなみみみなみ | *************************************** | . L 4 L 4 L 4 L 7 L L L L L L L L L L L L |
| Field Name L3V15D L4V15A L4V15D OGV15A OGV15A UCV15A | G1V1A G1V1D G2V1A G2V1A L1V1A L1V1D L1V1A L2V1A G2VCINA L1VCINA L2VCINA L3VCINA | OCYCINA GLAVTOT GLOVTOT GLOVTOT GLOVTOT GRAVTOT LIAVT LIAVTOT LIAVT LIAVTOT LIAVTOT LIAVTOT LIAVTOT LIAVTOT LIAVTOT LIAVTOT LIAVTOT LI | LADATOT LADATOT LADATOT CADATOT OGAVTOT OCAVTOT UCAVTOT UCDVTOT GLUWD GLUWD GLUWD LLUWD LLUWD LLUWD LLUWD LAUWD |
| Test Area 1P 1P 1P 1P 1P 1P | | 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | |
| ⊡ | च च च च च च च च च च च च च च | ਾ ਦਾ | ਾ ਚਾ |
| Sequence 3940 3950 3960 3970 3980 3990 4000 | 4010 4020 4020 4040 4050 4070 4090 4110 4110 4130 4130 | 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 4420 4410 4330 4330 4330 4330 4330 4330 433 |

| : | Description | ~ | ONDER CROWN ONWEIGHIED DEMERTIS (DEMERTIS) GROOVE #1 WRIGHTED DEMERTIS (DEMERTIS) | #2 WEIGHTED DEMERITS | WEIGHTED DEMERITS | #1 WEIGHTED DEMERITS | LAND #2 WEIGHTED DEMERITS (DEMERITS) | #3 WEIGHIED DEMEKLIS #4 INMETCHTED DEMEKLIS | OIL COOLING GALLERY WEIGHTED DEMERITS (DEMERITS) | F-4 | UNWEIGHTED TOTAL DEMERITS (DEMERITS) | | FON RATING WORKSHEET PLO | TOP GROOVE #1 HEAVY CARBON (* AREA) | GROOVE #1 LIGHT CARBON (| GROOVE #1 | TOP GROOVE #1 DEPOSIT 7.9 - 7 (% AREA) | GROOVE #1 DEPOSIT 6.9 - 6 (% | GROOVE #1 DEPOSIT 5.9 - 5 (% | GROOVE #1 DEPOSIT 4.9 - 4 (8 | GROOVE #1 DEPOSIT 3.9 - 3 (% | TOP GROOVE #1 DEPOSIT 2.9 - 2 (% AREA) | GROOVE #1 DEPOSIT 1:9 - 1 (8 | GROOVE #1 DEPOSIT CLEAN (% | OM GROOVE #1 HEAVY CARBON (| #1 MEDIUM CARBON | #1 | BOTIOM GROOVE #1 DEPOSIT 9 - 8 (% AREA) | GROOVE #1 DEPOSIT 7.9 - 7 (% | GROOVE #1 DEPOSIT 6.9 - 6 (% | GROOVE #1 | DEFOSIT 4.9 1 4 (4 | GROOVE #1 DEPOSIT 2.9 - 2 (% | GROOVE #1 DEPOSIT 1.9 - 1 (8 | BOTTOM GROOVE #1 DEPOSIT 0.9 - 0 (% AREA) | BOTTOM GROOVE #1 DEPOSIT CLEAN (% AREA) | HEAVY CARBON (| GROOVE #2 MEDIUM CARBON (% | GROOVE #2 LIGHT CARBON (% A | GROOVE #2 DEPOSIT 9 - 8 (* | GROOVE #2 DEPOSIT /.9 - / (* | GROOVE #2 DEPOSIT 6.9 - 6 (% | GROOVE #2 DEPOSIT 5.9 - 5 (% | TOP GROOVE #2 DEFOSIT 4.9 - 4 (* AREA) | | (continued) |
|-------|--------------|----------|--|----------------------|-------------------|----------------------|--------------------------------------|--|--|----------|--------------------------------------|--------------|--------------------------|-------------------------------------|--------------------------|-----------|--|------------------------------|------------------------------|------------------------------|------------------------------|--|------------------------------|----------------------------|-----------------------------|------------------|--------|---|------------------------------|------------------------------|---------------|--------------------|------------------------------|------------------------------|---|---|----------------|----------------------------|-----------------------------|----------------------------|------------------------------|------------------------------|------------------------------|--|-----|--|
| | Units/Format | DEMERITS | DEMERITS | DEMERITS | DEMERITS | DEMERITS | DEMERITS | DEMERTIS | DEMERITS | DEMERITS | DEMERITS | α l P | 1 | * AREA | & AREA | 8 AREA | 8 AREA | 8 AREA | % AREA | 8 AREA | & AREA | & AREA | A AREA | 8 AREA | & AREA | 8 AREA | 8 AREA | 8 AREA | 8 AREA | 8 AREA | * AKEA | S AREA | & AREA | 8 AREA | & AREA | & AREA | 8 AREA | & AREA | & AREA | * AKEA | * AKEA | * AKEA | & AREA | * AKEA * AREA | | FIG. A16.1 Data Dictionary (continued) |
| Data | Type | z | z 2 | z | Z | Z | z | 2 2 | 2 2 | z | Z | Z | υ | 2 2 | : 2 | z | Z | z | Z | Z | z | z | 2 2 | z | Z | z | Z | Z | Z | z | 2 2 | 2 2 | 2 | z | Z | z | z | Z | z ; | Z ; | 2 ; | z ; | z | zz | : (| i. A16.1 |
| Dec. | Size | N (| પ લ | (4 | (1) | C4 | cı c | 4 C | 1 (1 | લ | Н | 0 | 0 (| o c | 0 | 0 | 0 | 0 | 0 | 0 | 0 (| 0 0 | o c | 0 | 0 | 0 | 0 | 0 | 0 | 0 | > 0 | > | 0 | 0 | 0 | 0 | 0 | 0 | 0 (| > (| > 0 | > (| 0 0 |) C | , i | ב ב |
| Field | Length | - t | , , | | 7 | 7 | ۲ ر | - 1 | | 7 | 7 | 7 | 70 | ਰਾ ਵ | 4 | 4 | 4 | 4 | 4 | ₹ | 4. | 4. | # 4 | 7 | 4 | 4 | 4 | 4 | 4 | 4. | 4 4 | # ~ | r 4 | 4 | 4 | 4 | 4 | 4 | 4. | 4. | ਰਾ ⋖ | 4, 4 | 4. | # 4 | • | |
| ਚ | | OGUND | 000¥D | G2WD | G3WD | L1WD | L2WD | I A BE | OGMD | UCWD | OWD. | TLFC | RATEWSIM | GITHCA | GITLCA | G1T9A | G1T8A | G1T7A | GlI6A | G1T5A | G1T4A | GIT3A | G1171A | GITCLINA | GIBHCA | GIBMCA | GIBLCA | G1B9A | G1B8A | G1B7A | GIB6A | GIB3A | G1B3A | G1B2A | G1B1A | GIBCLNA | G2THCA | GETMCA | GZTLCA | GZT9A | GZT8A | GZT/A | GZT6A | G2T4A | 1 | |
| Test | Area | ₫ ; | 1 F | 1 H | 11 | 1P | 1P | 4 F | 1.P | 1.P | 1.P | 1.P | 1P | T. | 1F | 1P | 1 P | 115 | 1.5 | 1P | 1 <u>P</u> | 1 P | <u>η</u> μ | 15 | 1.P | 1P | 1.P | 11 | 11 | 다 . | 1 t | 1 F | 15 | 11 | 11 | 1P | 15 | 15 | 급 ; | 그 : | 4 5 | 4 5 | IP t | Δ | ; | |
| | Form | 4. | 4 4 | 4 | 4 | 4 | 4. | , | . 4 | 4 | 4 | 4 | 4a | n u | n un | Ŋ | ß | ß | വ | ഗ | ıc) i | wп | ט וכ | വ | . ro | Ŋ | ß | S | S | ហ | លម | ים כי | വ | 5 | വ | S | 2 | വ | ις | ຄເ | ១ ៤ | ກເ | ດພ | വറ | , | |
| | Sequence | 4430 | 4440 | 4460 | 4470 | 4480 | 4490 | 4500 | 4520 | 4530 | 4540 | 4550 | 4560 | 45/0 | 4590 | 4600 | 4610 | 4620 | 4630 | 4640 | 4650 | 4660 | 4680 | 4690 | 4700 | 4710 | 4720 | 4730 | 4740 | 4750 | 4/60 | 4780 | 4790 | 4800 | 4810 | 4820 | 4830 | 4840 | 4850 | 4860 | 48/0 | 4880 | 4890 | | 1 | |

| | P 05 7 - | GROOVE #2 DEPOSIT 0.9 - 0 (8 | TOP GROOVE #2 DEPOSIT CLEAN (% AREA) | GROOVE #2 HEAVY CARBON (4 | BOTTOM GROOVE #2 MEDIUM CARBON (* AREA) | GROOVE #2 DEPOSIT 9 - 8 | GROOVE #2 DEPOSIT 7.9 - 7 (8 | GROOVE #2 DEPOSIT 6.9 - 6 (% | GROOVE #2 DEPOSIT 5.9 - 5 (% | GROOVE #2 DEPOSIT 4.9 - 4 (\$ | | DEPOSIT 2.9 - 2 (8 | GROOVE #2 DEPOSIT 0.9 - 0 (8 | | HEAVY CARBON (| GROOVE #3 MEDIUM CARBON | GROOVE #3 LIGHT CARBON (% A | GROOVE #3 DEPOSIT 9 - 8 (* | GROOVE #3 DEPOSIT /.9 - / (* | GROOVE #3 DEPOSIT 6.9 - 6 (| | GROOVE #3 DEPOSIT 3.9 - 3 (8 | GROOVE #3 DEPOSIT 2.9 - 2 (8 | GROOVE #3 | GROOVE #3 | 40 | GROOVE #3 HEAVY CARBON (| GROOVE #3 MEDIUM CARBON (4 | | DEFOSII 9 - 0 (| GROOVE #3 DEPOSIT 6.9 - 6 | GROOVE #3 DEPOSIT 5.9 - 5 (8 | DEPOSIT 4.9 - 4 (% | GROOVE #3 DEPOSIT 3.9 - 3 (% | GROOVE #3 DEPOSIT 2.9 - 2 (% | GROOVE #3 DEPOSIT 1.9 - 1 | #3 DEPOSIT 0.9 - 0 (| _ | RING | KING #1 MEDIUM CARBON | KING #1 LIGHT CARBON (* A | RING #1 DEPOSIT 9 | TOP KING #1 DEPOSIT 1.9 = / (* AKEA) | F NING #1 DEFOSIT 0:3 - 0 (8 | nued) |
|-----------------|-------------|------------------------------|--------------------------------------|---------------------------|---|-------------------------|------------------------------|------------------------------|------------------------------|-------------------------------|----------|--------------------|------------------------------|----------|----------------|-------------------------|-----------------------------|----------------------------|------------------------------|-----------------------------|-------------------|------------------------------|------------------------------|-----------|-----------|----------|--------------------------|----------------------------|----------|-----------------|---------------------------|------------------------------|--------------------|------------------------------|------------------------------|---------------------------|----------------------|----------|---------------|-----------------------|---------------------------|-------------------|--------------------------------------|------------------------------|--|
| e a G | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N % AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA N & ADEA | N S AREA | N & AREA | N & AREA | N & AREA | N & AREA | N % AREA | N & AREA | N & AREA | N & AKEA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AKEA | N & AKEA | N % AREA | N & AREA | N & AKEA | FIG. A16.1 Data Dictionary (continued) |
| Dec. Size | o 0 | 0 | 0 | 0 | 0 0 | > C | 0 | 0 | 0 | 0 | 0 (| 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 (| 0 0 | > C | o | 0 | 0 | 0 | 0 | 0 | 0 (| > | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 ' | > (| o (| o ' | 0 (| > C | > | FIG. A16 |
| Field Length | 4.4 | 4 4 | 4 | 4 | 4. | # ₹ | r 4 7 | 4 | 4 | 4 | 4 | 4, 4 | * 4 | 4 | 4 | 4 | 4 | 4 | ♥ . | ₹ . | ₹ ₹ | # ~ | * 4 | . 4 | 4 | 4 | 4 | 4 | ₹' | | † 4 | 7 | 4 | 4 | 4 | 4 | 4 | 4 | 4. | 4 | 4 | ₹'' | d. 4 | 7 ' | |
| Field Name | G2T3A | G2T2A | GZTCLNA | G2BHCA | G2BMCA | GOBLCA | GZBSA | G2B7A | G2B6A | G2B5A | G2B4A | G2B3A | G2B1A | GZBCLNA | GSTHCA | G3TMCA | G3TLCA | G3T9A | G3T8A | G3T7A | G3T6A | GOLDA | 63T4A | GST2A | G3T1A | GSTCLNA | G3BHCA | G3BMCA | G3BLCA | G3B9A | G3B3A | G3B6A | G3B5A | G3B4A | G3B3A | G3B2A | G3B1A | GBCLNA | RITHCA | RITMCA | RITICA | R1T9A | RITSA | KIT/A | |
| Test | 15 15 | 4 t | 1 P | 11 | 15 | 4 t | 1P | 11 | 11 | 1P | 1. | 15 15 15 | 4 t | 15 | 11 | 1P | 11 | 1B | 1P | 1B | 1P | 4 5 | 4 C | 115 | 15 | 1F | 1.P | 1P | 11 | 4 ; | 4 6 | 1 t | 15 15 | 1P | 1P | 1P | 1B | 1b | 1P | 1 <u>P</u> | 15 | 1. 1. | IP | ₫ | |
| Form | ıcı | വ | Ŋ | S. | ഗ | വ | o ro | 5 | S | S | ഗ | ம் | חנו | വ | 2 | ī, | ഹ | 2 | മ | 2 | ស | n u | טינ |) LC | , ro | S. | 2 | ß | S. | in o | വ | ט עכ | ഗ | 2 | S | വ | ις. | S | വ | ഗ | ည | ស | மட | ဂ | |
| Sequence | 4920 | 4930 | 4950 | 4960 | 4970 | 4980 | 5000 | 5010 | 5020 | 5030 | 5040 | 5050 | 5050 | 5080 | 5090 | 5100 | 5110 | 5120 | 5130 | 5140 | 5150 | 2160 | 51/0 | 5190 | 5200 | 5210 | 5220 | 5230 | 5240 | 5250 | 5260 | 5280 | 5290 | 5300 | 5310 | 5320 | 5330 | 5340 | 5350 | 5360 | 5370 | 5380 | 5390 | 5400 | |

| | ription | RING #1 DEPOSIT 5.9 - 5 (* | RING #1 DEPOSIT 4.9 - 4 (% | RING #1 DEPOSIT 3.9 - 3 (% | RING #1 DEPOSIT 2.9 - 2 (| RING #1 DEPOSIT 1.9 - 1 | #1 DEPOSIT | DEPOSIT CLEAN (% | RING #1 HEAVY CARBON (| BOTTOM RING #1 MEDIUM CARBON (% AREA) | ARBON (% A | 8) 8 - 6 | 7.9 - 7 (8 | BOTTOM RING #1 DEPOSIT 6.9 - 6 (% AREA) | #1 DEPOSIT 5.9 - 5 (8 | RING #1 DEPOSIT 4.9 - 4 (% | RING #1 DEPOSIT 3.9 - 3 (% | RING #1 DEPOSIT 2.9 - 2 (% | RING #1 DEPOSIT 1.9 - 1 (| #1 DEPOSIT 0.9 - (| # 9 | RING #1 HEAVY CARBON (| RING #1 MEDIUM CARBON (8 | RING #1 LIGHT CARBON (% A | RING #1 DEPOSIT 9 - 8 (% | RING #1 DEPOSIT 7.9 - 7 (% | RING #1 DEPOSIT 6.9 - 6 (% | RING #1 DEPOSIT 5.9 - 5 (* | RING #1 DEPOSIT 4.9 - 4 (* | RING #1 DEPOSIT 3.9 - 3 (* | KING #1 DEPOSIT 2.9 - 2 (* | BACK KING #1 DEPOSIT 1.9 - 1 (* AKEA) | DING #1 DEFOSII O.9 - O | RING #2 HEAVY CARBON (8 | RING #2 | TOP RING #2 LIGHT CARBON (% AREA) | DEPOSIT 9 - 8 (% AF | RING #2 DEPOSIT 7.9 - 7 (% | RING #2 DEPOSIT 6.9 - 6 (8 | RING #2 DEPOSIT 5.9 - 5 (% | #2 DEPOSIT 4.9 - 4 (% | RING #2 DEPOSIT 3.9 - 3 (% | RING #2 DEPOSIT 2.9 - 2 (% | RING #2 DEPOSIT 1.9 - 1 (8 | #2 DEPOSIT 0.9 - 0 (| DEPOSIT CLEAN (% | RING #2 HEAVY CARBON (| RING #2 MEDIUM CARBON (8 | BOTTOM RING #2 LIGHT CARBON (% AREA) | (par |
|-------|----------|----------------------------|----------------------------|----------------------------|---------------------------|-------------------------|------------|------------------|------------------------|---------------------------------------|------------|------------|------------|---|-----------------------|----------------------------|----------------------------|----------------------------|---------------------------|--------------------|----------|------------------------|--------------------------|---------------------------|--------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|---------------------------------------|-------------------------|-------------------------|----------|-----------------------------------|---------------------|----------------------------|----------------------------|----------------------------|-----------------------|----------------------------|----------------------------|----------------------------|----------------------|------------------|------------------------|--------------------------|--------------------------------------|--|
| | 5 0 | app | ф | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | dю | ф | dр | dip (| olo . | op i | opo | N & AREA | N & AREA | N & AKEA | N & AKEA | N & AKEA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | dp i | N & AREA | FIG. A16.1 Data Dictionary (continued) |
| | ക | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 ' | 0 | 0 (| 0 (|) | - (| o c | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | IG. A16.1 D |
| Field | Length | 4 | 4 | ∢ . | 47' | 4 | 4 | 4 | 4 | 4 | 4 | 작 | 4 | 4 | 4 | 4 | 7 | 4 | ₩ | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4. | 4. | ₹ • | # ₹ | r 4 | 4 | 4 | 4 | 4 | 4 | 4 | ₽' | 4 | 4 | 4 | ₽ | 4 | 4 | 4 | 4 | 正 |
| т | | RITGA | R1T5A | R1T4A | R1T3A | R1T2A | RITIA | RITCINA | RIBHCA | RIBMCA | RIBLCA | R1B9A | R1B8A | R1B7A | R1B6A | R1B5A | R1B4A | R1B3A | R1B2A | R1B1A | RIBCINA | RIBKHCA | RIBKMCA | RIBKLCA | R1BK9A | R1BK8A | R1BK7A | RIBK6A | RIBK5A | RIBK4A | KIBK3A | RIBKZA | RIBRIA | RETHCA | RZIMCA | RZTLCA | R2T9A | R2T8A | R2T7A | RZT6A | R2T5A | R2T4A | R2T3A | R2T2 A | RZT1A | RZTCLNA | R2BHCA | RZBMCA | RZBLCA | |
| Test | Area | 15 | 1 P | 1 <u>P</u> | 1 P | 11 | 1 P | 1 P | 15 15 | 11 | 1F | 1 P | 1 P | 1P | 1P | 1P | 1 P | 1B | 1P | 1P | 1P | 1P | 1P | 15 | 15 | 1 P | 1P | 15 | Н Н | Н Н | I.P | - - | 4 F | <u>1</u> | <u>Α</u> | 1P | 1.P | 1P | 1P | 15 | 1 P | 1P | 1.P | 1P | 1P | 1P | 1P | 1Б | 1P | |
| | Form | 'n | ഹ | 2 | ß | ស | വ | ស | S | വ | S | 5 | Ŋ | 5 | S | S | ĸ | വ | വ | S. | ß | ည | 2 | വ | ഗ | ເດ | ഗ | വ | ın ı | ស | ΩL | חת | വ | טירט | · ιΩ | ß | S | S | 2 | ß | 5 | S | വ | വ | S. | ည | Ŋ | ഗ | വ | |
| | Sequence | 5410 | 5420 | 5430 | 5440 | 5450 | 5460 | 5470 | 5480 | 5490 | 5500 | 5510 | 5520 | 5530 | 5540 | 5550 | 5560 | 5570 | 5580 | 5590 | 2600 | 5610 | 5620 | 5630 | 5640 | 5650 | 5660 | 2670 | 5680 | 5690 | 5700 | 5710 | 5720 | 5740 | 5750 | 5760 | 5770 | 5780 | 5790 | 5800 | 5810 | 5820 | 5830 | 5840 | 5850 | 5860 | 5870 | 5880 | 5890 | |

| Description | BOTTOM RING #2 DEPOSIT 9 - 8 (% AREA) | 7.9 - 7 (8 | RING #2 DEPOSIT 6.9 - 6 (8 | RING #2 DEPOSIT 5.9 - 5 (* | RING #2 DEPOSIT | | RING #2 DEPOSIT 1.9 - 1 (8 | RING #2 DEPOSIT 0.9 - 0 (8 | IAN | RING #2 HEAVY CARBON (% 1 | RING #2 MEDIUM CARBON (% | RING #2 LIGHT CARBON (% A | RING #2 | | RING #2 DEPOSIT 5.9 - 5 (8 | RING #2 | DEPOSIT 3.9 - 3 (% | RING #2 DEPOSIT $2.9 - 2$ (% | RING #2 DEPOSIT 1.9 - 1 (% | RING #2 DEPOSIT 0.9 - 0 (| RING #2 DEPOSIT CLEA | RING #3 | RING #3 MEDIUM CARBON | DEFOCIT 9 = 8 (4) | DING #3 DEFORTE 9 - C (s | RING #3 DEPOSIT 6.9 - 6 (8 | RING #3 DEPOSIT 5.9 - 5 (8 | RING #3 DEPOSIT 4.9 - 4 (8 | RING #3 DEPOSIT 3.9 - 3 (8 | RING #3 DEPOSIT 2.9 - 2 (% | RING #3 DEPOSIT | | FOM RING #3 HEAVY CARBON (| RING #3 MEDIUM CARBON | BOTTOM RING #3 LIGHT CARBON (% AREA) | #3 DEPOSIT 9 - 8 (% AF | RING #3 DEPOSIT 7.9 - 7 (% | RING #3 DEPOSIT 6.9 - 6 (% | RING #3 DEPOSIT 5.9 - 5 (% | RING #3 DEPOSIT 4.9 - 4 (* | RING #3 DEPOSIT 3.9 - 3 (% | RING #3 DEPOSIT 2.9 - 2 (% | RING #3 DEPOSIT | KING #3 DEPOSIT U.Y = U (* pinc #2 perocit Citeran /* Ap | BOTTOM KING #3 DEFOSIT CLEAN (8 | ed) |
|---------------------------|---------------------------------------|------------|----------------------------|----------------------------|-----------------|----------------------|----------------------------|----------------------------|------------|---------------------------|--------------------------|---------------------------|----------|------------|----------------------------|------------|--------------------|------------------------------|----------------------------|---------------------------|----------------------|----------|-----------------------|-------------------|--------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|-----------------|------------|----------------------------|-----------------------|--------------------------------------|------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|-----------------|--|---------------------------------|--|
| Data Time Inita/Formst | | ollo | N % AREA | N & AREA | N & AREA | N & AREA N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | αp | N & AREA | N & AREA | * P o | N * AKEA | p d | N & AREA N & AREA | o de | dю | N % AREA | N & AREA | N & AREA | N & AREA | N & AREA | ф | N & AREA | N & AREA | N % AREA | dю | N & AREA | N & AREA | dю | N & AREA | de d | olip o | N * AKEA | FIG. A16.1 Data Dictionary (continued) |
| Dec. D | | 0 | 0 | 0 | 0 | o c | o c | 0 | 0 | 0 | 0 | 0 | 0 | 5 (| - |) C | 0 | 0 | 0 | 0 | 0 | 0 (| o 0 | o 0 | 5 (| - | » o | 0 | 0 | 0 | 0 (| o c |) C | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 (| 5 (| 5 | FIG. A16.1 |
| Field | 4 | · 4 | 4 | 4 | 4 | 4, < | r 7 | * 4 | 4 | 4 | 4 | 4 | ₽' | 4. | * < | r v | 4 | 4 | 4 | 4 | 4 | 4 | 4. | 4. 4 | . 77 • | 4. 4 | r 7 | 4 | 4 | 4 | 4. | 4. < | r 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4.4 | 4 | |
| Field | 4 | R2B8A | R2B7A | R2B6A | R2B5A | RZB4A | RADSA POBOA | R2B1A | RZBCLNA | RZBKHCA | RZBKMCA | R2BKLCA | R2BK9A | RZBKBA | K CBK / A | ROBESA | R2BK4A | R2BK3A | R2BK2A | R2BK1A | RZBKCLNA | RSTHCA | RSTMCA | RSTICA | R3T9A | RSTEA | RST6A | R3T5A | R3T4A | RSTSA | R3T2A | RSTIA | RARHCA | R3BMCA | R3BLCA | R3B9A | R3B8A | R3B7A | R3B6A | R3B5A | R3B4A | R3B3A | R3B2A | R3B1A | R3BCLNA | |
| Test | 10 | 11 | 1.P | 1 P | 1P | 1. 1. | 1 1 | 1.P | 1 <u>P</u> | 1. | 1P | 1.P | 1P | д. Г | 4 t | 4 C | 1 4 | 11 | 1B | 1P | 11 | 1P | 15 | 15 | I.P | - T-E- | 1 F | 15 | 115 | 1P | 1 <u>P</u> | 4 5 | 10 | 1P | 1₽ | 1P | 11 | 1B | 1P | 11 | 1P | 11 | 1P | 1P | ΙÞ | |
| 1 | 11 C | വ | ı.C | വ | ß | ي س | ט ע | o ro | . R | ß | വ | r. | വ | மை | ពផ | ים כ | വ | 5 | S | S | S. | S | ı, | ហ | Ω, | រាជ | o ro | ഹ | S | S | ស | וטו | יא כ | , ru | . rv | ა | 5 | ស | S | S | 5 | S | 2 | ហ | വ | |
| | seduence 5900 | 5910 | 5920 | 5930 | 5940 | 5950 | 2960 | 5980 | 5990 | 0009 | 6010 | 6020 | 6030 | 6040 | 0509 | 6060 | 6080 | 0609 | 6100 | 6110 | 6120 | 6130 | 6140 | 6150 | 6160 | 6170 | 6190 | 6200 | 6210 | 6220 | 6230 | 6240 | 6260 | 6270 | 6280 | 6290 | 6300 | 6310 | 6320 | 6330 | 6340 | 6350 | 6360 | 6370 | 6380 | |

79

| | | #3 HEAVY CARBON (| | RING #3 LIGHT CARBON (% A | RING #3 DEPOSIT 9 - 8 (% | RING #3 DEPOSIT 7.9 - 7 (% | RING #3 DEPOSIT 6.9 - 6 (% | RING #3 DEPOSIT 5.9 - 5 (* | RING #3 DEPOSIT 4.9 - 4 (* | RING #3 DEPOSIT 3.9 - 3 (* | RING #3 DEPOSIT 2.9 - 2 (% | RING #3 DEPOSIT 1.9 - 1 | RING #3 DEPOSIT 0.9 - (| 턴 | DEPOSIT & CONDITION RATINGS NPISTON | DEPOSIT & CONDITION | DEPOSIT & | ADDITIONAL DEPOSIT & CONDITION MALINGS | RATING | RATING | RATING INITIALS | GROOVE #1 HC-1.0 CARBON AREA PERC | GROOVE #1 HC-1.0 CARBON | GROOVE | | LAND | LAND #1 HC-1.0 CARBON | | LAND #2 HC-1.0 CARBON DEMERITS (DEMER | GROOVE | REFEREE GROOVE #3 HC-1.0 CARBON DEMEKIIS (DEMEKIIS) | | | | GROOVE #1 MC-0.5 CARBON AREA PERCENT (| MC-0.5 CARBON | GROOVE #3 MC-0.5 CARBON | GROOVE #3 MC-0.5 CARBON | GROOVE #1 LC25 | GROOVE #1 LC25 | GROOVE | | LAND #1 LC25 CARBON | LAND #1 LC25 CARBON | LAND #2 | LAND #2 LC | REFEREE GROOVE #3 IC-, 25 CARBON AREA PERCENT (* AREA) DEFEREE CROOME #3 IC- 25 CARBON DEWERTER (DEWERTER) | | ary (continued) |
|---------|-------------------|-------------------|----------|---------------------------|--------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|-------------------------|-------------------------|----------|-------------------------------------|---------------------|------------|--|--------|------------|-----------------|-----------------------------------|-------------------------|---------|------------|------------|-----------------------|---------|---------------------------------------|----------|---|------------|------------|------------|--|---------------|-------------------------|-------------------------|----------------|----------------|---------|-------------|---------------------|---------------------|---------|------------|--|----------------------|-----------------|
| Data | Type Units/Format | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | N & AREA | dю | N & AREA | v | υ | ບ ເ | ن | | C YYYYMMDD | | _ | | • | - | | N DEMERITS | | N DEMERITS | N & AREA | N DEMERITS | N & AKEA | N DEMENTES | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | - | | - | | | | - | | N & AREA | | , T |
| Dec. Da | Size Ty | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 (| > | 0 | 0 | 0 | 0 | 64 | 0 | N | 0 | (1 | 0 | (1 | 0 (| N (| . . | 4 C | , c | 10 | C) | 0 | લ | 0 ' | (4) | 0 | (4) | 0 | ĸI | 0 | (4 | ، ٥ | 4 C | ָ . เมื |
| Field | Length | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | | 70 | 70 | 70 | 0/ | 10 | ω | m | 4 | 7 | 4 | 7 | 4 | 7 | 4 | 7 | 47 (| | ar t | ٠ | * [| 4 | 7 | 4 | 7 | 4 | 7 | 4 | 7 | 4 | 7 | 4 | 7 | 4.1 | ~ 4 | • |
| Field | Name | R3BKHCA | R3BKMCA | R3BKLCA | R3BK9A | R3BK8A | R3BK7A | R3BK6A | R3BK5A | R3BK4A | R3BK3A | R3BK2A | R3BK1A | R3BKCLNA | CROWNAD | SKIRTAD | LINERAD | KINGSAD | RRNO | RRDATE | RRINIT | RRG1HCA | RRG1HCD | RRG2HCA | RRG2HCD | RRITHCA | RRL1HCD | RRLZHCA | RRLZHCD | RRG3HCA | RRG3HCD | RKL3HCA | PPT AUCA | RPT.4HCD | RRGIMCA | RRG1MCD | RRG3MCA | RRG3MCD | RRGIICA | RRGILCD | RRGZICA | RRG2ICD | RRL1LCA | RRL1LCD | RRL2LCA | RRL2LCD | RRG3LCA | RRG3LCD RRT.3T.CA | |
| Test | Area | 1P | 1P | 11 | 1P | 1P | 1P | 1 P | 15 | 1P | 1B | 1 P | 1P | 11 | 1 P | 1P | 1 <u>P</u> | 1 F | 1B | 16 | 1.P | 1P | 1 P | 1P | 1 <u>P</u> | 1 <u>P</u> | 1 P | 1F | 1P | 15 | IΡ | 1 t | 4 5 | 1 1 | 15 | 1.P | 11 | 11 | 15 | 1 P | 1P | 1F | 15 | 1 P | 1P | 1 P | 1P | 4 t | ; |
| | Form | ß | 2 | ស | S | വ | വ | S | വ | ഗ | 'n | S | S) | 2 | S) | ß | r) | ŋ | 5а | 5a | 5a | 5а | 5a | 5a | 5a | Sа | Sа | Sa | 5a | 5a | 5a | д u | 10 u | טינ קית | S S | 5a | 5а | 5a | Sp | 5a | Sа | 5a | Sа | 5a | 5a | Бa | e g | n d | j |
| | Sequence Form | 6390 | 6400 | 6410 | 6420 | 6430 | 6440 | 6450 | 6460 | 6470 | 6480 | 6490 | 6500 | 6510 | 6520 | 6530 | 6540 | 0559 | 6560 | 6570 | 6580 | 6590 | 0099 | 6610 | 6620 | 6630 | 6640 | 6650 | 0999 | 6670 | 6680 | 0660 | 0/00 | 6720 | 6730 | 6740 | 6750 | 6760 | 6770 | 6780 | 6190 | 6800 | 6810 | 6820 | 6830 | 6840 | 6850 | 6860 | > |

FIG. A16.1 Data Dictionary (continued)

| | REFERRE LAND #3 LC25 CARBON DEMERITS (DEMERITS) | REFEREE RATING LAND #4 LC25 CARBON AREA % (% AREA) | REFEREE RATING LAND #4 LC25 CARBON DEMERITS (DEMERITS) | | REFFERE RATING OIL COOLING GALLERY IC 25 CARBON (DEMERITS) | REFEREE RATING UNDER CROWN IC25 CARBON (% AREA) | REFEREE TOTAL GROOVE #1 CARBON AREA PERCENT (% AREA) | | REFEREE TOTAL GROOVE #2 CARBON AREA PERCENT (% AREA) | TOTAL | TOTAL LAND #1 | TOTAL | TOIN | REFEREE TOTAL GROOVE #3 CARBON DEMERTIS (DEMERTIS) | TOTAL | | REFEREE TOTAL LAND #3 CARBON DEMERITS (DEMERITS) | REFEREE TOTAL LAND #3 CARBON AREA PERCENT (% AREA) | | REFEREE RATING TOTAL OIL COOLING GALLERY CARBON % (% AREA) | RATING TOTAL OIL COOLING GALLERY CARBON DEM. (| RATING TOTAL UNDER CROWN | REF. RATING TOTAL UNDER CROWN CARBON DEMERITS (DEMERITS) | NEFEREE GROOVE #1 8-9 VARNISH AREA PERCENT (* AREA) RREEDER GROOVE #1 8-9 VARNISH DEMERITS (DEMERITS) | GROOVE #2 | GROOVE #2 | 8-9 | 8-9 | | LAND #2 8- | GROOVE #1 | NEFERER GROOVE #1 /-/.9 VAKNISH DEMEKTIS (DEMEKTIS) DEEEDDE COONT #2 7-7 G VARNISH APEN DEDCEMT (\$ APEN) | GROOVE #2 | LAND #1 7- | 7-7.9 | REFEREE LAND #2 7-7.9 VARNISH AREA PERCENT (% AREA) | LAND #2 7- | GROOVE #3 7.5 VARNISH | | 7.5 VARNISH | LAND #3 7.5 VARNISH | LAND | LAND #4 7.5 VARNISH DEMERITS (DEMERITS) | REFEREE LAND OIL COOLING GALLERY 7.5 VARNISH AREA & (% AREA) REFEREE LAND OIL COOLING GALLERY 7.5 VARNISH (DEMERITS) | ued) |
|-------|---|--|--|------------|--|---|--|------------|--|------------|---------------|------------|-------------|--|------------|----------|--|--|------------|--|--|--------------------------|--|--|-----------|------------|----------|------------|----------|------------|-----------|---|------------|------------|------------|---|------------|-----------------------|------------|-------------|---------------------|------------|---|--|------------|
| Data | N DEMERITS | | N DEMERITS | N & AREA | N DEMERITS | N % AREA N DEMERTTS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AKEA | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AKEA N DEMERTE | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERTIS | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | - | ם . | N S AKEA | (F |
| Dec. | 21.20 | 0 | C4 | 0 | (4) | ، د | 10 | ۲۷ | 0 | (4 | 0 | (1) | - (| N 0 | (4 | 0 | (1) | 0 | (1 | 0 | ca · | 0 (| (4 C |) (| 1 0 | C4 | 0 | 71 | 0 | (4) | 0 (| 4 C | o (\ | 0 | (1 | 0 | 64 | 0 | (4 | 0 | 63 | 0 | (4) | > 64 | I |
| Field | nengen 7 | 4 | 7 | 4 | 7 | 4 1 | . 4 | 7 | 4 | 7 | ₹ | _ | 3" (| - 4 | 7 | 4 | 7 | 4 | 7 | 4 | _ | ∀ (| | 4. [- | - 4 | 7 | 4 | 7 | 4 | ۲. | 4 (| ~ < | | 4 | 7 | 4 | 7 | 4 | 7 | 4 | 7 | 4 | · · | * ~ | • |
| Field | RRL3LCD | RRL4LCA | RRL4LCD | RROGICA | RROGLCD | RRUCLCA | RG1ACTO1 | RGIDCTOT | RG2ACTOT | RG2DCTOT | RLIACTOT | RL1DCTOT | RECTOI | RG3ACTOT | RG3DCTOT | RL3ACTOT | RL3DCTOT | RL4ACTOT | RL4DCTOT | ROGACTOT | ROGDCTOT | RUCACTOT | RUCDCTOT | RRG1V9A | RRG2V9A | RRG2V9D | RRL1V9A | RRL1V9D | RRL2V9A | RRL2V9D | RRG1V8A | PPG2V8A | RRG2V8D | RRL1V8A | RRL1V8D | RRL2V8A | RRL2V8D | RRG3V75A | RRG3V75D | RRL3V75A | RRL3V75D | RRL4V75A | RRL4V75D | RROGV/5D | : |
| Test | AL CA | 11 | 1 P | 1 <u>P</u> | 115 | 1P | 1B | 1 P | 1 P | 1 P | 115 | 1P | 4 ; | 1 E | 15 15 | 11 | 1 P | 1P | 1P | 1P | 15 | 15 | 1 I I | 4 t | 1 1 | 11 | 11 | 11 | 1P | 11 11 | 4 ; | 4 5 | 1 = | 1P | 1P | 1B | 1 P | 1B | 1P | 1 P | 1 P | 1 P | 1. 1. | 4 4 | |
| | 5a | 5a | 5a | 5a | 5a | S B | o ro | 5.2 | 5a | 5a | Sa | 50 a | 10 L | 0 to | 5a | 5a | 5a | 5a | 5a | 5a | 5 a | g B | r g | U T. Mag |) (C | 5a | 5a | 5a | 5а | Sa 1 | о С | n n | 1 m | 5.8 | 5 a | 5a | 5a | Sa | 5a | 5а | 5a | 5 a | S a | മറ | , |
| | oe89 | 0689 | 0069 | 6910 | 6920 | 6930 | 6950 | 0969 | 6970 | 6980 | 0669 | 7000 | 010/ | 7030 | 7040 | 7050 | 7060 | 7070 | 7080 | 1090 | 7100 | 7110 | 7120 | 7140 | 7150 | 7160 | 7170 | 7180 | 7190 | 7200 | 7210 | 7230 | 7240 | 7250 | 7260 | 7270 | 7280 | 7290 | 7300 | 7310 | 7320 | 7330 | 7340 | 7360 | |

FIG. A16.1 Data Dictionary (continued)

| | Description | LAND UNDER CROWN | LAND UNDER CROWN 7.5 VARNISH | GROOVE #1 6-6.9 VARNISH | GROOVE #1 6-6.9 VARNISH | GROOVE #2 | KEFEKEL GROOVE #4 6-6.9 VARNISH DEMEKLI'S (DEMEKLI'S) DEBEDDE TAND #1 6-6 9 WADNISH ADEA DEDCENH /* ADEA) | TAND #1 6-6 0 | LAND #2 6-6.9 VARNISH | LAND #2 6-6.9 VARNISH | GROOVE #1 5-5. | GROOVE #1 | 5-5. | GROOVE #2 5-5. | LAND #1 5-5.9 VARNISH | LAND #1 5-5.9 | LAND #2 5-5.9 VARNISH AREA PERC | LAND #2 5-5.9 | GROOVE #1 4-4.9 VARNISH AREA PERC | GROOVE #1 4-4.9 VARNISH | GROOVE #2 4-4 | GROOVE #2 4-4. | LAND #1 | LAND #1 4-4.9 VARNISH DEMERITS (DEM | LAND #2 4-4.9 VARNISH | LAND #2 4-4.9 VARNISH | _ | GROOVE #3 4. | LAND #3 4.5 VARNISH | LAND #3 4.5 VARNISH | LAND #4 | LAND #4 4.5 VARNISH DEMERITS (DEMERITS) | REFEREE RATING OIL COOLING GALLERY 4.5 VARNISH (* AREA) | RATING UID COCLING SALLERI RATING UNDER CROWN 4.5 VARN | RATING UNDER CROWN 4.5 VARNISH | GROOVE #1 3-3.9 VARNISH AREA PE | #1 3-3.9 VARNISH | GROOVE #2 3-3. | REFEREE GROOVE #2 3-3.9 VARNISH DEMERITS (DEMERITS) | REFEREE LAND #1 3-3.9 VARNISH AREA PERCENT (% AREA) | REFEREE LAND #1 3-3.9 VARNISH DEMERITS (DEMERITS) | REFEREE LAND #2 3-3.9 VARNISH AREA PERCENT (% AREA) | LAND #2 3-3.9 VA | GROOVE #1 2-2.9 VARNISH | GROOVE #1 2-2.9 VARNISH DEMERITS (DEMERI | GROOVE #2 2-2.9 VARNISH | REFEREE GROOVE #2 2-2.9 VARNISH DEMERITS (DEMERITS) BEFEREE LAND #1 2-3 9 VARNISH AREA DEFORM (* AREA) | Continuod | |
|-------|-------------------|------------------|------------------------------|-------------------------|-------------------------|-----------|--|---------------|-----------------------|-----------------------|----------------|------------|------------|----------------|-----------------------|---------------|---------------------------------|---------------|-----------------------------------|-------------------------|---------------|----------------|-------------|-------------------------------------|-----------------------|-----------------------|----------|--------------|---------------------|---------------------|----------|---|---|---|--------------------------------|---------------------------------|------------------|----------------|---|---|---|---|------------------|-------------------------|--|-------------------------|---|------------------------|--|
| | Type Units/Format | - | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMEKTES | N DEWEDTER | N & AREA | N DEMERITS | N % AREA | N DEMERITS | N % AREA | N DEMERITS | N & AREA | ш | | | υp | Д | OΡ | _ | V 1- | _ | u, | _ | ~ | N DEMERITS | N & AREA | N DEMERITS | N & AREA | N DEMERITS | N * AKEA | N % AREA | N DEMERITS | N & AREA | N DEMERITS | N % AREA | N DEMERITS | N & AREA | N DEMERITS | N % AREA | H | N & AREA | 日 | | N DEMERITS N * AREA | N CANAGA DOLO DIOLO NO | TI A TO THE PERSON OF THE PERS |
| Dec. | Size | 0 | C) I | 0 (| :4 0 | 0 0 | √I C | oγ | 10 | (d | 0 | (·1 | 0 | СЛ | 0 | বে | 0 | C) | 0 | C 4 | 0 | N | 0 | C4 | 0 | લ | 0 | C4 | 0 | C-I (| 0 (| CI C |) (| 1 C | (4) | 0 | ¢4 | 0 | N | 0 | C1 | 0 | C-1 | 0 | લ | 0 (| чС | > | |
| Field | Length | | ۲ . | 4 1 | | 41.1 | _ < | * 1 | 4 | 7 | 4 | 7 | ₹ | 7 | 7 | 7 | 4 | 7 | 4 | 7 | 4 | 7 | 4 | 7 | 4 | 7 | | | A 4 | Q : | A 4 | 2 | 4 c | 4 · | 7 di | ر 4 | 7 (| 4 | 7 7 | 1 4 | 7 7 | 4 | 7 | 1 4 | 7 | 4 . | · 7 | , | |
| Field | Name | RRUCV75 | RRUCV75 | RRG1V7A | RRG1V/D | RRG2V/A | KKGZV/U | DDT.1177 | RRL2V7A | RRL2V7D | RRG1V6A | RRG1V6D | RRG2V6A | RRG2V6D | RRL1V6A | RRL1V6D | RRL2V6A | RRL2V6D | RRG1V5A | RRG1V5D | RRG2V5A | RRG2V5D | RRL1V5A | RRL1V5D | RRL2V5A | RRL2V5D | RRG3V45 | RRG3V45 | RRL3V45 | RRL3V45 | RRL4V45 | RRL4V45D | RKOGV45A | RRUCV45 | RRUCV45 | RRG1V4 | RRG1V4 | RRG2V4 | RRG2V4L | RRI1V4A | RRL1V4 | RRL2V4 | RRL2V4 | RRG1V3# | RRG1V3I | RRG2V37 | RRGZV3L RRT 1V32 | 1 | |
| Test | Area | 1 P | 1P | 1P | <u>,</u> | IP | 1 t | 4 F | 15 | 11 | 1P | 1P | 1 P | 1P | 11 | 15 | 15 | 1P | 1 P | 1 P | 1 P | 1 P | 1 P | 1 P | 1 <u>P</u> | 15 | 15 | 1P | 1P | 1P | 1P | 15 | 4 t | <u> 1</u> | 1P | 15 | 115 | 11 | 1P | 1P | 1P | 1P | 1P | 15 | 15 | 더 | 1 L | ; | |
| | Œ | 5a | 5a | g i | e r | g B | n n n | לו מ אור כ | S A | Sa | 5a | 5а | 5а | 5a | 5.0 | S. | വ | 52 | Sa | 5a | 5a | 5a | Sа | 5a | 5a | rg Cu | 5a | 5a | Sa | д 1 | ъ 2 | 5a | 10 to | מ מ | 5a | 5а | 5а | 5а | Sа | Sа | 5a | 5a | Sа | 5a | | n n | ש ת יש מי | 3 | |
| | Sequence | 7370 | 7380 | 7390 | 7400 | 7420 | 7430 | 0777 | 7450 | 7460 | 7470 | 7480 | 7490 | 7500 | 7510 | 7520 | 7530 | 7540 | 7550 | 7560 | 7570 | 7580 | 7590 | 7600 | 7610 | 7620 | 7630 | 7640 | 7650 | 7660 | 7670 | 7680 | 7200 | 7710 | 7720 | 7730 | 7740 | 7750 | 1760 | 7770 | 7780 | 7790 | 7800 | 7810 | 7820 | 7830 | 7850 |)) | |

FIG. A16.1 Data Dictionary (continued)

| | Description | REFEREE LAND #1 2-2.9 VARNISH DEMERITS (DEMERITS) | REFEREE LAND #2 2-2.9 VARNISH AREA PERCENT (% AREA) | GROOVE #1 1-1. | GROOVE #1 1-1.9 VARNISH | REFEREE GROOVE #2 1-1.9 VARNISH AREA PERCENT (% AREA) REFEREE GROOVE #2 1-1.9 VARNISH DEMERITS (DEMERITS) | | REFEREE LAND #1 1-1.9 VARNISH DEMERITS (DEMERITS) | LAND #2 1-1.9 VARNISH | GROOVE #3 1.5 VARNISH | | | | REFEREE LAND #4 1.5 VARNISH DEMERITS (DEMERITS) | RATING OIL COOLING GALLERY 1.5 VARNISH | RATING OIL COOLING GALLERY 1.5 | REFEREE RATING UNDER CROWN 1.5 VARNISH (* AREA) REFEREE RATING UNDER CROWN 1.5 VARNISH (DEMERITS) | GROOVE #1 0-0.9 VARNISH AREA PE | GROOVE | REFERE GROOVE #2 0-0.9 VARNISH AREA PERCENT (% AREA) REFERE GROOVE #2 0-0 9 VARNISH DEMERTS (DEMERTS) | LAND #1 0- | LAND #1 | | KEFEREE LAND #2 U-0.3 VAKNISH DEMEKIIS (DEMEKIIS) REFEREE GROOVE #1 CLEAN VARNISH DEMERITS (% AREA) | GROOVE #2 CLEAN VARNISH DEMERITS | LAND #1 CLEAN VARNISH DEMERITS (% | REFEREE GROOVE #3 CLEAN VARNISH DEMERITS (* AREA) | LAND #3 CLEAN VARNISH DEMERITS (% | REFEREE LAND #4 CLEAN VARNISH DEMERITS (% AREA) | | TOTAL GROOVE | TOTAL GROOVE #1 VARNISH | TOTAL GROOVE #2 | REFEREE TOTAL GROOVE #2 VARNISH DEMERITS (DEMERITS) | TOTAL GROOVE #3 VARNISH | TOTAL LAND #1 | TOTAL | TOTAL LAND #2 VARNISH AREA PERC | REFEREE TOTAL LAND #2 VARNISH DEMERITS (DEMERITS) REFEREE TOTAL LAND #3 VARNISH AREA PERCENT (* AREA) | |
|----------------|--------------|---|---|----------------|-------------------------|---|---------------|---|-----------------------|-----------------------|----------------|-------------------|--------------------|---|--|--------------------------------|--|---------------------------------|------------------|---|------------------|------------------|------------------|---|----------------------------------|-----------------------------------|---|-----------------------------------|---|----------------|----------------|-------------------------|---------------------|---|-------------------------|-----------------|---------------|---------------------------------|--|--|
| • | Units/Format | DEMERITS | & AREA | 8 AREA | DEMERITS | 8 AREA DEMERITS | & AREA | DEMERITS | DEMERITS | 8 AREA | DEMERITS | * AKEA | PEMEKITS 8 AREA | DEMERITS | & AREA | DEMERITS | S AKEA DEMERITS | & AREA | DEMERITS | 8 AREA Demente | AREA | DEMERITS | B AREA | B AREA | 8 AREA | & AREA | e AREA 8 AREA | 8 AREA | & AREA | * AREA | 8 AREA | DEMERITS | 8 AREA | DEMERITS 8 APPA | DEMERITS | 8 AREA | DEMERITS | & AREA | DEMERITS 8 AREA | FIG. A16.1 Data Dictionary (continued) |
| Data | Type | z | | | | | | | | | | | | _ | G, | — о | W L | dp | Ω | olo C |) olo | _ | OP 1 | -1 UP | | | | | | | | | • | i d | | | | | | |
| ď | | | Z | z z | Z | 2 2 | Z | 2 2 | 2 2 | z | Z | z | zz | z | z | z | # C | i de Z | Z | Z Z | ar : Z | Z | z | - G- | Z | Z | zz | Z | z | z 2 | Z | z | z | ⊠ a | 4 Z | Z | Z | Z | zz | <u> </u> |
| Dec | Size | | 000 | X X | 2 N | 0 0 | 0 | N 2 | 2 2 | 0 0 | N (| 2 2 | 7 O | 2 N | z Z | N 3 | * L | . Z | Z | Z 2 | 1 of 2 Z | Z | Z : | X X | N 0 | 0 0 | z z | 0 | z ż | 2 2 | 0 | 2 N | N O | (1) of | . Z | 0 | Z 2 | 0 0 | Z Z | FIG |
| | | 73 | 4 t | 2 0 4 N | 7 2 N | 4 0 N | 4 0 N | 2 C C C C C C C C C C C C C C C C C C C | | . 4 . 0 | 7 2 N | 7 T | 7 7 7 N | 7 2 N | 4 0 N | N 20 | 2 C | . Z. O | Z | Z 2 | · Z | Z | z | N N N | 4 0 N | 0 ° | 7 T | 4 0 N | 0 ° | 4 4 2 C | 4 0 N | 7 2 N | z | Z 2 | . Z | 4 0 N | 7 2 N | 0 0 0 N | . O | FIG |
| Field Field De | Length | 73 | RRLZV3A 4 0 N | RRG1V2A 4 0 N | RRG1V2D 7 2 N | RRG2V2A 4 0 N RRG2V2D 7 2 N | RRLIVZA 4 0 N | RRLIV2D 7 2 N | RRL2V2D 7 2 N | RRG3V15A 4 0 N | RRG3V15D 7 2 N | RRL3V15A 4 0 N | RKL4V15A 4 0 N | RRL4V15D 7 2 N | N 0 | W (| RECOVER 4 0 N T | . Z | 7 2 N | Z 2 | 10 | 7 2 N | 4 t | RRGIVCLA 4 0 N 9 | RRG2VCLA 4 0 N | RELIVELA 4 0 N | RRG3VCLA 4 0 N | RRL3VCLA 4 0 N | RRL4VCLA 4 0 N | RRIGUCIA 4 0 N | RG1AVTOT 4 0 N | 7 | . N | Z 2 | Z Z | 4 | 7 | 47 (| RLZDVTOT / 2 N RL3AVTOT 4 0 N | |
| Field | Name Length | 7 2 | 4 1 | | | 1P RRG2V2A 4 0 N 1P RRG2V2D 7 2 N | | 1P RRLIV2D 7 2 N | | | | IP RRLJVIDA 4 0 N | | | RROGV15A 4 0 N | RROGV15D 7 2 N | 2 C | RRGIVIA 4 0 N | RRG1V1D 7 2 N | 0 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° | RRIIVIA 4 0 N | RRLIVID 7 2 N | RRLZV1A 4 0 N | N N | | | 1P RRG3VCLA 4 0 N | | 1P RRL4VCLA 4 0 N | • | | RG1DVTOT 7 | RG2AVTOT 4 0 N | C1 C | RG3DVTOT 7 2 N | RL1AVTOT 4 | RL1DVTOT 7 | RL2AVTOT 4 | 1P RL3AVTOT / 2 N 1P RL3AVTOT 4 0 N | |
| Field Field | Name Length | 1P RRL1V3D 7 2 | RRL2V3A 4 | 115 | 1. | | 1P | | 4 6 | 1 11 | 119 | 4 F | | 11 | 1P RROGV15A 4 0 N | 1P RROGVI5D 7 2 N | RRUCVISD 7 2 N | 1P RRGIVIA 4 0 N | 1P RRGIVID 7 2 N | RRGZVIA 4 0 N | 1P RRIIVIA 4 0 N | 1P RRLIVID 7 2 N | 1P RRL2V1A 4 0 N | RRGIVCLA 4 0 N | 1.0 | 41 | | 11P | | יים ר | 11 11 | 1P RGIDVTOT 7 | a 1P RG2AVTOT 4 0 N | RG2DVTOT 7 2 N | 1P RG3DVTOT 7 2 N | a 1P RLIAVIOT 4 | 1P RLIDVIOT 7 | a 1P RL2AVTOT 4 | | |

83

| Dogovariation | REFEREE TOTAL LAND #3 VARNISH DEMERITS (DEWERITS) | | DEMERITS (DEMERITS) | RATING TOTAL OIL COOLING GALLERY | RATING TOTAL OIL COLLING | REF. RATING TOTAL UNDER CROWN VARNISH AREA PERCENT (* AREA) REF. RATING TOTAL UNDER CROWN VARNISH DEMERITS (DEMERITS) | REFEREE GROOVE #1 UNWEIGHTED DEMERITS (DEMERITS) | REFEREE GROOVE #2 UNWEIGHTED DEMERITS (DEMERITS) | REFEREE GROOVE #3 UNWEIGHTED DEMERITS (DEMERITS) | LAND #1 UNWEIGHTED DEMERITS | LAND #2 UNWEIGHTED DEMERITS | LAND #3 UNWEIGHTED DEMERITS | LAND #4 UNWEIGHTED | RATING OIL COOLING GALLERY UNWEIGHTED DI | RATING UNDER CROWN UNWEIGHTE | GROOVE #1 WEIGHTED DEMEKTIS | GROOVE #2 WEIGHTED DEMEKITS | GROOVE #3 WEIGHTED DEMERTIT | TAND #1 WEIGHTED DEMERITS | LAND #2 WEIGHTED DEMEKTES | LAND #3 WEIGHTED DEMERITS | REFERENCE LAND #4 WELGHIED DEMEKTIS (DEMEKTIS) | KALING | KEFEKEE KAIING UNDEK CKOWN WEIGHIED DEMEKIIS (DEMEKIES) REFEREER RATING INWELTCHTED TOTAI, DEMERITS (DEMERITS) | NEFERRED NATION OF T. WIAKED CAPRON (*) | VISC 6 100 oc AT XXX HOURS (CSt.) | 14 | 4739 AT XXX | TAN D664 AT XXX HOURS | FE - WEAR METALS AT XXX HOURS [<] (ppm) | - WEAR METALS AT XXX HOURS [<] | - WEAR METALS AT XXX HOURS [<] | - WEAR METALS AT XXX HOURS [<] | WEAR METALS AT XXX HOURS [<] | (mdd) | | | OIL CONSUMPTION @ ENGINE HOURS AT XXX HOURS (g/h) | OIL CONSUMPTION R SQUARED @ ENGINE HOURS AT XXX HOURS | FUEL POSITION AT XXX HOURS (mm) | | DATE | DOWNTIME TIME (HHH:MM) | DOWNTIME REASON | OTHER DOWNTIME COMMENTS XXX | NUMBER OF DOWNTIME OCCURENCES | DOWNTIME TIME TOTAL (HHH:MM) | onary (continued) |
|---------------------------|---|----------|---------------------|----------------------------------|--------------------------|--|--|--|--|-----------------------------|-----------------------------|-----------------------------|--------------------|--|------------------------------|-----------------------------|-----------------------------|-----------------------------|---------------------------|---------------------------|---------------------------|--|------------|---|---|-----------------------------------|----------|--------------|-----------------------|---|--------------------------------|--------------------------------|--------------------------------|------------------------------|---------|----------|----------|---|---|---------------------------------|----------|------------|------------------------|-----------------|-----------------------------|-------------------------------|------------------------------|--|
| Data mimo Huita/Bormot | | N & AREA | | | N DEMERITS | N % AREA N DEMERTES | N DEMERITS | N DEMERITS | N DEMERITS | N DEMERITS | N DEMERITS | | | N DEMERITS | | | | | ' | N DEMEKTI'S | | | | N DEMERTES | | | | | Z | A ppm | A ppm | | | A ppm | A ppm | | | N g/h | Z | N mm | C HHH:MM | C YYYYMWDD | C HHH:MM | υ | υ | | C HHH:MM | FIG. A16.1 Data Dictionary (continued) |
| Dec. | 315G | 0 | C/I | 0 (| :4 ¢ | ၁ က | ı | (4 | C) | € | СЛ | (4 | C 1 | 61 | (4) | ч (| N (| N (| rsi (| ч (| (4) | м с | ч c | ν - | + C | o 6 | ı c | । द ब | C4 | 0 | 0 | 0 | 0 | 0 | 0 | .⊣ | H | H | বে | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Field | 11) 11) | 4 | 7 | 47 ' ! | | 4 7 | | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | ~ 1 | - 1 | - 1 | ۱ - | ~ r | ۱ | - 1 | - 1 | ٠, ١ | , [| ٠, ١ | | 7 | 7 | 4 | 4 | 4 | 4 | 4 | 4 | ഹ | 9 | വ | S | 2 | 9 | ω | 9 | 9 | 70 | m ' | ø | |
| 75 | RL3DVTOT | RL4AVTOT | RL4DVTOT | ROGAVIOT | ROGDVTOT | RUCAVIOI | RRGIUWD | RRG2UWD | RRG3UWD | RRL1UWD | RRL2UWD | RRISUWD | RRL4UWD | RROGUND | RRUCUWD | KKGIWD | RRGZWD | RRG3WD | RRLIWD | KKLZWD | RRL3WD | KKL4WD | KKOGWD | RRUCMD | DETTEC | VIOUHXXX | V40 HXXX | TBN HXXX | TAN HXXX | FEWMHXXX | ALWMHXXX | SIWMHXXX | CUWMHXXX | CRWMHXXX | PBWHXXX | FDILHXXX | BLBYHXXX | OCONHXXX | OCRRHXXX | FPOSHXXX | DOWNHXXX | DDATHXXX | DTIMHXXX | DREAHXXX | OCOMHXXX | DWNOCR | TOTLDOWN | |
| Test | ALEA 1P | 1F | 1B | 1P | I.P | 4 t | 15 15 | 11 | 119 | 1P | 1P | 1B | 1P | 15 | 15 | 4 ; | I.P | I.P | <u>н</u> ; | <u>구</u> : | 15 15 | 4 ; | 4 £ | 4 E | 1 5 | 1 F | 15 | 1.P | 1 P | 1P | 1P | 1 P | 1 P | 1P | ТЪ | 15 | 119 | 1P | 1 P | 1P | 15 | 1P | 11 | 1.5 | 15 | 1.P | 1P | |
| | . FOT.III | 5a | 5a | 5a | ba | യ ന വ | S d | 5a | 5а | 5а | 5а | 5a | 5a | รูล | ις, ι | e C | g . | g, | ر ا م | g G | S B | ر رو | в . | n n | ט ע ס מ | 9 4 | 9 | 9 | Q | 9 | 9 | 9 | Q | 9 | 9 | 9 | 9 | ૭ | ဖ | 9 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | |
| , | seduence 8350 | 8360 | 8370 | 8380 | 8390 | 8400 | 8420 | 8430 | 8440 | 8450 | 8460 | 8470 | 8480 | 8490 | 8500 | OTCR | 8520 | 8530 | 8540 | 8220 | 8560 | 8570 | 8580 | 8590 | 9610 | 0798 | 8630 | 8640 | 8650 | 8660 | 8670 | 8680 | 8690 | 8100 | 8710 | 8720 | 8730 | 8740 | 8750 | 8760 | 8770 | 8780 | 8790 | 8800 | 8810 | 8820 | 8830 | |

FIG. A16.1 Data Dictionary (continued)

| | Description | L LINES C | TOP RING GAP PRE-TEST (mm) | TI NING GAF FAR-IEST PRE-TEST (III) | RING GAP POST-TEST | CATE #1 RING GZ | OIL RING GAP POST-TEST (mm) | RING SIDE CLEARANCE A [| PRETEST RING SIDE CLEARANCE B [STUCK, <, >] | PRETEST RING SIDE CLEARANCE C [STUCK, <, >] | PRETEST RING SIDE CLEARANCE D [STUCK, <, >] (m | MINIMUM DING SIDE CLEARANCE AVG [SICCK, <, >] (HHI) | TOT-1 | SIDE CLEARANCE TOP POST-TEST B [STUCK, <, >] | SIDE CLEARANCE TOP POST-TEST C [STUCK, <, >] | RING SIDE CLEARANCE TOP POST-TEST D [STUCK, <, >] (mm) | SIDE CLEARANCE TOP POST-TEST AVERAGE [| RING SIDE CLEARANCE POSTIES | SIDE CLEARANCE TOP LSC A [STUCK, <, >] | SIDE CLEARANCE TOP LSC B [STUCK, <, >] | SIDE CLEARANCE TOP LSC C STUCK, <, >] | SIDE CLEARANCE TOP LSC D (STUCK, <, >) (mm) | KING SIDE CLEARANCE TOP LSC MINIMUM [STUCK, <, >] (MM) MINIMUM DINC SIDE CIERDRANCE - INT. DEFINEST (SMICE <) / Jum.) | THE PRESENT | SIDE CLEARANCE INT. PRETEST B | CLEARANCE INT. PRETEST C | INT. PRETEST D | ARANCE INT. PRETEST D | JUM RING SIDE CLEARANCE-INT1-POSTTEST [STUCK, <, | SIDE CLEARANCE INT. POST-TEST A [STUCK, <, >] | NING SIDE CLEARANCE INT. POST-TEST B [STUCK, <, >] (MM) | SIDE CLEARANCE INI. FOST-IESI ([SIOCA, /, /] | SIDE CLEARANCE INT. POST-TEST AVG [STUCK, <, > | RING SIDE CLEARANCE INT. LSC A [STUCK, <, >] (mm) | SIDE CLEARANCE INT. LSC B [| SIDE CLEARANCE INT. LSC | SIDE CLEARANCE INT. LSC | SIDE CLEARANCE INT. LSC MINIMUM [STUCK, <, > | SIDE CLEARANCE OIL PRE-TEST A [STUCK, <, >] | SIDE CLEARANCE OIL PRE-TEST B [STUCK, <, >] | SIDE CLEARANCE OIL PRE-TEST C | SIDE CLEARANCE OIL PRE-TEST | E OIL PRE-TEST AVG [STUCK, <, >] (mm | MINIMUM RING SIDE CLEARANCE-OIL-PRETEST [STUCK, <, >] (mm) | SIDE CLEARANCE OIL FOST-IEST A | | A16.1 Data Dictionary (continued) |
|-------|-------------------|-----------|----------------------------|--|--------------------|-----------------|-----------------------------|-------------------------|---|---|--|---|--------|---|--|--|--|-----------------------------|--|--|--|---|--|-------------|-------------------------------|--------------------------|----------------|-----------------------|--|---|---|---|--|---|-----------------------------|-------------------------|-------------------------|--|---|---|-------------------------------|-----------------------------|--------------------------------------|--|--------------------------------|-------|-----------------------------------|
| | Type Units/Format | 13 | N N | | um Z | N mm | N man | A mm | A mm | A mm | A mm | A min | | THE THE | A mm | A mm | A mm | A mm | A mm | A mon | A rren | A mm | A mm | THE T | | A mm | A mm | A mm | A mm | A * | A mm | | A mm | A mm | A mm | A mm | A mm | A mm | A mm | A mm | | | W IIII | A mm | A mm | | FIG. A16.1 Data DICT |
| Dec. | Size | 0 | mm | n m | , m | m | m | ო | m | ო | ლ (| י רי | n ~ | n m | m | ო | m | ო | ო (| m (| m (| י רי | יז ני | n m | nm | m | m | m | m (| יי רי | יי רי | ე ო | m | က | ო | m | m | ന | m (| m (| m c | יי) רי | יני | יי ריי | o m | , | |
| Field | Length | m · | vo v | , , | · w | 9 | Q | 7 | , | 7 | 7 | - 4 | | | 7 | 1 7 | 7 7 | 9 | 7 | - 1 | - 1 | ~ [| ٠ ، | - I | | 3 7 | 1 7 | 7 | 9 1 | | - r | | | 7 | 7 | 7 | 7 | 7 | 7 | - 1 | · r | ~ r | | 9 - | - [- | | |
| Field | Name | TOTCOM | PINGGTE | RINGGOR | RINGGIO | RINGGI10 | RINGGOO | SIDETPE1 | SIDETPEZ | SIDETPE3 | SIDETPE4 | Ternerne | STREET | SIDETPO2 | SIDETPO3 | SIDETPO4 | ASIDETPO | ISIDETPO | LSCT1 | LSCT2 | LSCT3 | LSCT4 | TETOFIDE | STORIDEL | SIDEIPEZ | SIDE1PE3 | SIDE1PE4 | ASIDE1PE | ISIDE1PO | SIDELPOL | SIDELPO2 | SIDELECS | ASIDE1PO | LSC11 | LSC12 | LSC13 | LSCI4 | ILSCINT | SIDEOPE | SIDEOPEZ | SIDEOPES | SIDEOPE4 | ASIDEOPE | SIDEOPE | SIDEOPO2 | | |
| Test | Area | 15 | IP T | 1 F | 1. 1.P | 1P | 1P | 1 b | 1P | 1P | 1. 1. | 4 5 | 1 5 | 15 | 1 P | 1 P | 1P | 11 | 1 <u>P</u> | 4 : | 4 ; | 4 5 | 크 t | 1 F | 1 1 | 1.5 | 1P | 15 | 1F | 4 5 | 1 1 | 1 1 | 1B | 1 P | 1 P | 15 | 15 | I.P | 1 <u>P</u> | H . | 1 t | ן קין נ | 4 ; | 1 F | 4 1 | i | |
| | Form | 7 | oo oo | ο α | ω | 80 | 8 | 80 | 8 | ω | ω (| ο α | α | σ | 80 | ω | ω | ω | ω (| ထပ | ω (| o c | οα | οα | οω | œ | œ | ω . | ω (| 0 0 | οα | 0 00 | 8 | 80 | ω | ထ | ω | ω . | ω (| 00 (| 000 | 20 0 | oc | α | ο α | , | |
| | Sequence | 8840 | 8850 | 8870 | 8880 | 0688 | 8900 | 8910 | 8920 | 8930 | 8940 | 0000 | 0000 | 8980 | 8990 | 0006 | 9010 | 9020 | 9030 | 9040 | 9050 | 9060 | 9080 | 0606 | 9100 | 9110 | 9120 | 9130 | 9140 | 9150 | 9170 | 9180 | 9190 | 9200 | 9210 | 9220 | 9230 | 9240 | 9250 | 9260 | 9270 | 0000 | 0878 | 9300 | 9320 | 1 | |

| | DESCRIPTION DING SIDE CIRADANGE OIL DOCE-FERT C [SMICK < > >] (mm) | SIDE CLEARANCE | SIDE CLEARANCE OIL POST-TEST AVG [STUCK, <, >] | UM RING SIDE CLEARANCE-OIL-POSTTEST [ST | SIDE CLEARANCE OIL LSC A [STUCK, <, >] | RING SIDE CLEARANCE OIL LSC B [STUCK, <, >] (mm) RING SIDE CLEARANCE OIL LSC C [STUCK, <, >] (mm) | SIDE CLEARANCE OIL LSC D [STUCK, <, >] | SIDE CLEARANCE OIL LSC MINIMUM [STUC | BORE SURFACE FINISH | BORE SURFACE FINISH -LONGITUDINAL- | BORE SURFACE FINISH - AVERAGE - 130 | LINER BORE SURFACE FINISH - TRANSVERSE - 50 MM (MICFOMETE) | DONE SOMERCE FINISH DONGILOSINAD | BORE SURFACE FINISH - TRANSVERSE - 25 1 | BORE SURFACE FINISH -LONGITUDINAL- | LINER BORE SURFACE FINISH - AVERAGE - 25 MM (micrometre) | | | SORE POLISH | | TEST LINER BORE | TEST LINER | TEST LINER | TEST LINER BORE | TEST LINER BORE | BEFORE TEST LINER BORE MEA 1/0 MM HT-LONGITUDINAL (UU) | TEST LINER BORE | TEST LINER BORE | | LINER BORE | TEST LINER BORE | TEST LINER BORE MEA50 MM HT-TRANSVERSE (m | TEST LINER | BEFORE IEST LINER BOKE MEA:20 MM HI-LONGILOLINAL (MM) DEBODE TEST TIMPS DODE MEN35 MM HI-TENNITEDSE (TM) | TEST LINER BORE MEA25 MM HI-TRANSVERSE (| TEST LINER BORE | LINER BORE | TEST LINER BORE MEA15 MM | BEFORE TEST LINER BORE MEATAPER -LONGITUDINAL (mm) | | TEST LINER BORE WEAR | TEST LINER BORE WEAR | TEST LINER BORE WEAR STEPTRANSVERSE T (| AFTER TEST LINER BORE WEAR STEPTRANSVERSE AT (mm) | ENGINE SPEED SENSING DEVICE | ionary (continued) |
|-------|--|----------------|--|---|--|---|--|--------------------------------------|---------------------|------------------------------------|-------------------------------------|--|----------------------------------|---|------------------------------------|--|--------------|------------|-------------|---------|-----------------|------------|------------|-----------------|-----------------|--|-----------------|-----------------|---------|------------|-----------------|---|-------------|--|--|-----------------|------------|--------------------------|--|----------|----------------------|----------------------|---|---|-----------------------------|--|
| Data | Type Units/Format | | | A mm | A mm | | A mm | A mm | N micrometre | N micrometre | N micrometre | | | N micrometre | | | N micrometre | of Z | of Z | N mm | N mm | | | | | | N N | N III | N mm | N mm | N mm | א אומנו | | | | um Z | N mm | N mm | N mm | N mm | N mm | N mm | N mm | N C | : : : | FIG. A16.1 Data Dictionary (continued) |
| Dec. | Size | n m | m | ო | m | m r | n m | m | (7) | (1 | (1) | (4) C | 4 (| 4 C | 1 (4 | (1 | Ø | Н | н | m | ю | m | m | m i | m (| m c | n m | m | ю | ო | ო | ന | 7) (| יי ני | าศ | n | е | m | m | ю | ო | ო | m | mc | > | |
| Field | rengtn | , , | 7 | 9 | 7 | <u>ر</u> ر | , _ | 7 | 5 | 5 | ស | ın u | O 4 | ם עם | വ | ß | S | 9 | 9 | 80 | œ | 9 | ω | ω ' | 9 (| ω (| o w | ω | ω | 9 | ထ | ω ' | ، م | ю o | o vo | - α | 80 | ø | ω | 80 | 9 | 9 | 9 | 9 [| /1 | |
| 73 | Name L | SIDEOPO4 | ASIDEOPO | ISIDEOPO | LSC01 | LSC02 | LSCO4 | ILSCO | BBLFINT1 | BBLFINL1 | BBLFINA1 | BBLFINT2 | BBLF INLA | BELFINAS | BBLFINL3 | BBLFINA3 | BBLFIN | BOREPT | BOREPAT | BBLONG1 | BBTRAN1 | 00R1 | BBLONG2 | BBTRANZ | OOR2 | BBLONG3 | DOR3 | BBLONG4 | BBTRAN4 | 00R4 | BBLONG 5 | BBTRAN5 | OORS | BBLONGS | OORE | BBLONG7 | BBTRAN7 | OOR7 | TAPRIONG | TAPRTRAN | AWEARLE | AWEARLR | AWEARTT | AWEARTAT | RPMSENS | |
| Test | Area | 15 | 1 <u>P</u> | 1 P | 1P | 1 1 1 | 1P | 1P | 11 | 11 | 16 | 15 | | 4 t | 1 1 | 1P | 1P | 1 P | 1 P | 1P | 1P | 1P | 1 P | 15 | 15 | 1P | 4 F | 1.P | 1.5 | 11 | 1P | 15 | A : | H 5 | 4 6 | 15 | 11 | 1 P | 1P | 11 | 1P | 1 P | 1B | # F | 4 | |
| ı | Form | 0 00 | ω | 89 | 00 | ω α | 0 00 | ω | 6 | თ | თ | o 0 | א ע | nσ | , o | თ | D | თ | σ | თ | თ | σ | σ | σ. | o (| o (| ח ס | n 01 | თ | თ | σ | თ : | э (| י ע | nσ | 0 | ი | თ | თ | 0 | თ | 0 | o . | σ, | 70 | |
| | Sequence | 9340 | 9350 | 9360 | 9370 | 9380 | 9400 | 9410 | 9420 | 9430 | 9440 | 9450 | 9460 | 94/0 | 9490 | 9500 | 9510 | 9520 | 9530 | 9540 | 9550 | 9560 | 9570 | 9580 | 9590 | 9600 | 9610 | 9630 | 9640 | 9650 | 0996 | 9670 | 0896 | 9690 | 9710 | 9720 | 9730 | 9740 | 9750 | 9760 | 9770 | 9780 | 9790 | 9800 | 9810 | |

FIG. A16.1 Data Dictionary (continued)

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | • | ~ | | | | | |
|---------------------------|------------------------------------|---------|---------|---------|----------------------------|---------|---------|----------------------------|------------|------------|------------------------------|-------------|--|-------------|---------------|---------------|---|------------|------------|------------|---------------------------|------------|--|-----------------|--|-----------------|---------------------------------------|------------------|----------------|----------------|--|----------------|--|-------------|---|------------|---|-------------------------|---|------|
| Description | ENGINE SPEED CALIBRATION FREQUENCY | SPEED | SPEED | SPEED | ENGINE SPEED LOG FREQUENCY | POWER | POWER | ENGINE POWER RECORD DEVICE | POWER | POWER | ENGINE POWER SYSTEM RESPONSE | RATE | FUEL RATE CALIBRATION FREQUENCY FUEL RATE RECORD DEVICE | RATE | RATE | ENGINE | FUEL RATE SYSTEM RESPONSE HIMIDITY SENSING DEVICE | | | | HUMIDITY RECORD FREQUENCY | | COOLANT OUT TEMPERATURE SENSING DEVICE | OUT TEMPERATURE | COOLANT OUT TEMPERATURE ENGINE SPEED RECORD DEVICE COOLANT OUT TEMPERATURE OBSERVATION FREQUENCY | OUT TEMPERATURE | COOLANT OUT TEMPERATURE LOG FREQUENCY | IN TEMPERATURE S | IN TEMPERATURE | IN TEMPERATURE | COOLANT IN TEMPERATURE OBSERVATION FREQUENCY | IN TEMPERATURE | COOLANT IN TEMPERATURE SYSTEM RESPONSE | TEMPERATURE | AVERAGE EXHAUST TEMPERATURE FOR LAST 10 TESTS (SC. OTT. TO MANIFOLD TEMPERATURE CALIERATION FREQUENCY | | OIL TO MANIFOLD TEMPERATURE RECORD DEVICE | TO MANIFOLD TEMPERATURE | OIL TO MANIFOLD TEMPERATURE RECORD FREQUENCY OII, TO MANIFOLD TEMPERATURE LOG FREQUENCY | |
| Data Tvoe Units/Format | | υ | ບ | D 8 | ט ני | υ | U | o t |) U | ຸບ | ບ | U t | ט ט | υ | ບ | U | υt | ט ט | υ | υ | ບະ | υ | υ | O t | ט נ | υ | ບເ | ט ע | υ | טּ | ט ט | υ | υ | ر د ت |) Si | E N | i O | ָּט | υυ | 0.00 |
| Data | | J | Ŭ | • | - | , , | | | , , | | Ŭ | • | - | | _ | • | _ | | Ŭ | • | | | Ĭ | | | Ū | | | Ĭ | | | | • | • | | | | _ | | Č |
| Dec. Size | 0 | 0 | 0 | 0 (| 0 0 | 0 | 0 | - | 0 | 0 | ٥ | 0 0 | 0 | 0 | 0 | 0 | 00 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 , | + C | · - | 0 | 0 | - 0 | |
| Field Length | 13 | 16 | 12 | 27. | 7 8 | 17 | 13 | 9 : | ; C\ | . A1 | | | | | | 6 .1 . | | | | | | | | | _ | | | | _ | | S1 61 | . 61 | ۵ | ~ . | ρm | ی و | 16 | 12 | 77 | |
| E E | | | | | | | | | - | 12 | œ | 17 | 19 | 12 | 12 | 12 | 2 0 | 13 | 16 | 12 | 17 | 8 | 17 | 13 | 17 | 12 | 173 | 17 | 13 | 16 | 7 2 | 12 | w | 17 | 13 | • | | | | |
| Field | I.F | RPMRECD | RPMOBSF | RPMRECE | RPMSYSE | PWRSENS | PWRCALF | PWRRECD | | | | | FFLOCALF 13 | | | | FFLOSYSR 8 | | | | HUMRECE 12 | | | COTCALF 13 | | | COTLOGF 12 | | | | CONDESE 12 | | | OBRGSENS 1 | | | | OBRGOBSE | OBRGIOGE | |
| Test Field Area Name | PREMICALE | • | | | • | | | | PWRRECF | PWRLOGE | PWRSYSR | FFLOSENS | FFLORECD | FFLOOBSF | FFLORECF | FFLOLOGE | FFTOSYSR HIMSENS 1 | HUMCALF | HUMRECD | HUMOBSE | HUMRECF | HUMSYSR | COLSENS | COTCALF | COTOBSE | COTRECF | COTLOGE | CONSENS | CONCALF | CONRECD | CONRECF | CONLOGE | CONSYSR | OBRGSENS | OBRGCALF | ATORHXXX | OBRGRECD | | 1P OBRGLOGE | |
| u m | 1P RPMCALF | 0 1P | 1.5 | | 1 F | 0 1P | 11. | | 1P PWRRECF | 1P PWRLOGE | 1P PWRSYSR | 1P FFLOSENS | FFLORECD | 1P FFLOOBSF | 0 1P FFLORECF | 1P FFLOLOGF | FFTOSYSR HIMSENS 1 | 1P HUMCALF | 1P HUMRECD | 1P HUMOBSE | HUMRECF | 1P HUMSYSR | 1P COTSENS | COTCALF | 1P COTOBSE | 1P COTRECF | 1P COTLOGE | 1P CONSENS | 1P CONCALF | 1P CONRECD | 1P CONDESE | 1P CONLOGE | 1P CONSYSR | 1P OBRGSENS | 1P OBRGCALF | 1P ATORHXX | 1P OBRGRECD | 1.0 | | |

FIG. A16.1 Data Dictionary (continued)

| | Description | USAGE START DATES (YYYYMMDD) | OIL TO MANIFOLD TEMPERATURE SYSTEM RESPONSE | | OIL COOLER IN TEMPERATURE SENSING DEVICE | WEIGHTED TOTAL DEMERITS ZI | OIL COOLER IN TEMPERATURE CALIBRATION FREQUENCY WETCHTED TOTAL DEMERTTS SEVERITY ADDITISTMENT | OIL COOLER IN TEMPERATURE RECORD DEVICE | TOP GROOVE CARBON ZI | | TOP GROOVE CARBON S.A. | | | | TOP LAND CARBON S.A. | | INDET AIR TEMPERATURE SENSING DEVICE | OIL CONSUMPTION S.A. | INLET AIR TEMPERATURE CALIBRATION FREQUENCY | EOT OIL CONSUMPTION ZI | INLET AIR TEMPERATURE RECORD DEVICE | EOT OIL CONSUMPTION S.A. | | INLET AIR TEMPERATURE ENGINE SPEED RECORD FREQUENCY | INLET AIR TEMPERATURE LOG FREQUENCY | | TEMPERATURE | TEMPERATURE | EXHAUST TEMPERATURE RECORD DEVICE | TEMPERATORE | TEMPERATURE | TEMPERATURE | TEMPERA | HEAD TEMPERATURE | TO MANIFOLD PRESSURE | OIL TO MANIFOLD PRESSURE SYSTEM RESPONSE | INLET AIR PRESSURE SENSING DEVICE | (continued) |
|-------|-------------------|------------------------------|---|------------|--|----------------------------|---|---|----------------------|----------|------------------------|----------|----------|------------|----------------------|------------|--------------------------------------|----------------------|---|------------------------|-------------------------------------|--------------------------|----------|---|-------------------------------------|------------|-------------|-------------|-----------------------------------|-------------|-------------|-------------|----------|------------------|---------------------|---------------------|---------------------|---------------------|---------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|--|-----------------------------------|-----------------------------------|
| Data | Type Units/Format | C YYYYMMDD | ບ | C HHH:MM | υ | Z | UZ | : ບ | Z | υ | Z | ŭ | Z | υ | 2. |) 2 | : U | × | U | Z | v | Z | ບ | υ | υ | U | ပ | U | | , t | . . | າ ບ | υ | ပ | ပ | O I | U i | υ [,] | ი | บ | ບ | υ | ပ | υ | υ i | ပေး | ט | A16.1 Data Dictionary (continued) |
| | Size Ty | 0 | 0 | 0 | 0 | m · | o - | 10 | | 0 | 7 | 0 | Э | 0 | (1) | > ~ | . 0 | | 0 | e | 0 | 7 | 0 | 0 | 0 | 0 | 0 (| 0 0 | . | . | | . 0 | 0 | 0 | 0 | 0 ' | 0 (| 0 (| 0 | 0 | 0 | 0 | 0 | 0 | 0 1 | 0 0 | | FIG. A |
| | | ~ | 80 | ١٥. | | 7 | m v | | 7 | 61 | 9 | C:I | 7 | ~ 1 | 9 0 | | . ~ | . L | . | 7 | w | z, | rs. | N. | C) | 6 0 | 7 | m (| 9 5 | <i>4</i> 6 | ı (\ | . & | 7 | 13 | 16 | 12 | 17 | 77 | ω (| 17 | 13 | 16 | 12 | 12 | 12 | ω [| | |
| Field | Length | | | | - | | - | - | | F 12 | | - | | - | | | 17 | | F 13 | | - | | | | - | | | | | | | | | | | | | | | | | | | | | | | |
| Field | Name | DISTRKK | OBRGSYSR | DTTMRXXX | OCOLSENS | WDZIRXX | MUSARKK | OCOLRECD | TGZIRXXX | OCOLOBSE | TGSARXXX | OCOLRECE | TLZIRXXX | OCOLLOGE | TLSARKK | OCCUBICA | AIRTSENS | OCSARXX | AIRTCALF | ETZIRXXX | AIRTRECD | ETSARXX | AIRTOBSF | AIRTRECF | AIRTLOGE | AIRTSYSR | EXTSENS | EXTCALE | EXTRECT | EATOBSE | EXTINGE | EXTSYSE | FUELSENS | FUELCALF | FUELRECD | FUELOBSE | FUELRECE | FUELLOGE | FUELSYSR | OBRPSENS | OBRPCALF | OBRPRECD | OBRPOBSF | OBRPRECF | OBRPLOGE | OBRPSYSR | AIRPSENS | |
| Test | Area | 15 | 15 | 1 <u>P</u> | 15 | H. | 1P | 15 | 15 15 | 1P | 1 P | 1B | 11 | 1 P | 15 | 1 1 | 15 | 1B | 1P | 11 | 1P | 11 | 1P | 15 | 15 | 1 P | 1 <u>P</u> | 15 15 | 4 5 | 4 - | ή <u>C</u> | 1 # | 1P | 15 | 115 | <u>1</u> | 15 | 15 15 | 1B | IP. | 15 | IP. | 15 15 | 1P | 1P | 1P | Ä | |
| | Form | 15 | 10 | 15 | 10 | 12 | 10 | 10 | 15 | 10 | 15 | 10 | 12 | 10 | 15 |) r | 10 | 15 | 10 | 15 | 10 | 15 | 10 | 10 | 10 | 10 | 10 | 10 | 2 5 | 3 5 | 9 5 | 2 2 | 10 | 10 | 10 | 10 | 10 | 10 | 01 | 01 | 01 | 10 | 10 | 10 | 10 | 10 | 70 | |
| | Sequence | 10310 | 10320 | 10330 | 10340 | 10350 | 10360 | 10380 | 10390 | 10400 | 10410 | 10420 | 10430 | 10440 | 10450 | 10470 | 10480 | 10490 | 10500 | 10510 | 10520 | 10530 | 10540 | 10550 | 10560 | 10570 | 10580 | 10590 | 10600 | 10620 | 10630 | 10640 | 10650 | 10660 | 10670 | 10680 | 10690 | 10700 | 10710 | 10720 | 10730 | 10740 | 10750 | 10760 | 10770 | 10780 | 10/20 | |

| | iption | AIR PRESSURE | AIR PRESSURE | PRESSURE | INLET AIR PRESSORE RECORD FREQUENCY | A TR | T PF | EXHAUST PRESSURE CALIBRATION FREQUENCY | EXHAUST PRESSURE RECORD DEVICE | EXHAUST PRESSURE OBSERVATION FREQUENCY | PRESSURE | EXHAUST PRESSURE LOG FREQUENCY | IST PRESSURE SYSTEM | FROM HEAD PRESSURE | FROM HEAD PRESSURE | TROM HEAD PRESSURE | | FROM HEAD DRESSINE | FROM HEAD PRESSURE | KCASE SENSING DEVICE | | CRANKCASE RECORD DEVICE | CRANKCASE OBSERVATION FREQUENCY | CRANKCASE RECORD FREQUENCY | CRANKCASE LOG FREQUENCY | CRANKCASE SYSTEM RESPONSE | SENSING | | | | | | COOLANT FILM RESPONSE | | MO.TH | FT.OW | FLOW | FLOW | COOLANT FLOW SYSTEM RESPONSE | 0 - 48 OIL CONSUMPTION (g/h) | OIL CONSUMPTION PLOT IMAGE | PISTON RING AND LINER PHOTOGRAPHS PLOT IMAGE | FUEL BATCH ANALYSIS PLOT IMAGE | TMC CONTROL CHART ANALYSIS PLOT IMAGE | continued) |
|-------|-------------------|--------------|--------------|---------------|-------------------------------------|------------|------------|--|--------------------------------|--|----------|--------------------------------|---------------------|--------------------|--------------------|--------------------|-----------|--------------------|--------------------|----------------------|---------|-------------------------|---------------------------------|----------------------------|-------------------------|---------------------------|----------|----------|------------|------------|----------|---------------|-----------------------|----------|------------|-----------|----------|----------|------------------------------|------------------------------|----------------------------|--|--------------------------------|---------------------------------------|--|
| Data | Type Units/Format | O · | ບເ | ن ر | ז נ |) U | , O | ບ | υ | U | υ | บ | υ | บ | υt | ، ر | ن ر | ט ני | יט | U | υ | υ | U | U | U | υ | υ | υ | υ | บ | υ | U (| ט נ |) ເ | , U | ייני | ı U | υ | υ | N g/h | | υ | ບ | υ | FIG. A16.1 Data Dictionary (continued) |
| Dec. | Size | 0 | 0 0 | > 0 | > < | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | o c | , c | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | > 0 | o c |) C | , c | | 0 | 0 | 0 | Η. | 0 | 0 | 0 | 0 | FIG. A |
| Field | Length | 133 | 9 7 | 4 F | 4 C | 1 00 | 17 | 13 | 16 | 12 | 12 | 12 | ω | 17 | 13 | 9 5 | 4 C | 1 ~ | ω | 17 | 13 | 16 | 12 | 12 | 12 | 80 | 17 | 13 | 16 | 12 | 12 | 17 | 1,0 | · ~ | 9 | - 2 | 12 | 12 | œ | R) | 70 | 70 | 70 | 70 | |
| Field | Name | AIRPCALF | AIRPRECD | AIRFORSE | AIRFIGE | ATRESYSE | EXPSENS | EXPCALF | EXPRECD | EXPOBSE | EXPRECF | EXPLOGE | EXPSYSR | FFILSENS | FFILCALF | TOUR TREE | FETT.RECE | FFTTATOGE | FFILSYSR | CCVSENS | CCVCALF | CCVRECD | CCVOBSF | CCVRECF | CCVLOGF | CCVSYSR | BLBYSENS | BLBYCALF | BLBYRECD | BLBYOBSF | BLBYRECF | BLBYLOGE | CFLWSENS | T.TACAT. | CFLWRECD | CFT.WORSF | CFLWRECF | CFLWLOGF | CFLWSYSR | BOTOC | OCPIM | PRLIM | FUELIM | CCHIM | |
| Test | Area | 1.P | ΙΡ | 4 t | 11. | 15 | 1 <u>P</u> | 1P | 1P | 1P | 1P | 1b | 1 <u>P</u> | 15 | 115 | 4 F | 1 L | - 4 | 11 | 1P | 1P | 1.P | 1P | 15 | 1 <u>P</u> | 15 | 15 | 1P | 1 P | 1 <u>P</u> | 1. 1. | 4 t | 4 C | 1 - | 15 | 10 | 1P | 1P | 11 | 1 <u>P</u> | 11 | 1B | 1 P | 1 p | |
| | Form | 10 | 0 5 | 2 5 | 1 5 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 2 5 | 2 5 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 010 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 13 | 13 | 14 | 16 | 17 | |
| | Sequence | 10800 | 10810 | 10020 | 10840 | 10850 | 10860 | 10870 | 10880 | 10890 | 10900 | 10910 | 10920 | 10930 | 10940 | 10950 | 10920 | 10980 | 10990 | 11000 | 11010 | 11020 | 11030 | 11040 | 11050 | 11060 | 11070 | 11080 | 11090 | 11100 | 11110 | 11120 | 11140 | 11150 | 11160 | 11170 | 11180 | 11190 | 11200 | 11210 | 11220 | 11230 | 11240 | 11250 | |

89



APPENDIXES

(Nonmandatory Information)

X1. VARIOUS EXAMPLES FOR REFERENCE PURPOSES

X1.1 See Figs. X1.1-X1.8.

∰ D 6681 – 01

| ¢ | G | ROOV | 1 | | ROOV | 12 | 9 | ROOVE | 13 | COOL | ING GA | LERY | UNDE | R CRO | WN |
|---|--------|----------------|---------|-------|------------------|--------|--------------------------------------|----------------|-----------------|--|-----------|--|----------------|-------------|--------|
| A | A% | FCT | DEM | A% | FCT | DEM | A% | FCT | DEM | A% | FCT | DEM | A% | FCT | DEN |
| R | 5 | 1.00 | 5.00 | 3 | 1.00 | 500 | 3 | 1.00 | 5.00 | 1000000 | | De la Constitución de la Constit | 100000 | OR THE REAL | 2 5 5 |
| | 5 | 0.50 | 250 | DOM: | NUMBER OF STREET | Karan. | 5 | 0.50 | 250 | | | | land. | | |
| 0 | 5 | 0.25 | 1.25 | 5 | 0.25 | 1.25 | 3 | 0.25 | 1.25 | 3 | 0.25 | 125 | 3 | 0.25 | 1.25 |
| N | SUBT | | 875 | SUB1 | _ | 625 | SUBT | OTAL | 875 | SUBT | | 1.8 | SUBT | | 1.25 |
| | 000000 | REAL PROPERTY. | 1000000 | 1000 | Name of Street | | O STATE OF THE PARTY. | Name of Street | NAME OF TAXABLE | DESCRIPTION OF THE PARTY OF THE | | 100000 | Name of Street | | 100000 |
| v | 9 | 85 | 276 | 3 | 85 | 0.75 | 1// | 8.5 | 0.87 | 117 | 7.5 | 0.57 | 117 | 7.5 | 0.57 |
| A | 7 | 75 | 0.52 | 7 | 75 | 052 | 17 | 7.5 | 452 | 9 | 4.5 | 0.40 | 9 | 4.5 | 240 |
| R | 9 | 65 | 0.58 | 9 | 65 | 0.58 | 1 | 65 | 0.22 | 1 7 | 1.5 | 0.10 | 7 | 1.5 | 410 |
| N | 7 | 55 | 0.8 | 7 | 55 | 0.8 | 13 | 55 | 4.58 | | | | | | - |
| ï | 9 | 15 | 0.40 | 9 | 15 | 040 | 1 | 4.5 | 40 | 1 | | | 1 | | |
| | 7 | 35 | 0.24 | 7 | 15 | 0.24 | 3 | 15 | 4.22 | | | | 1 | | |
| н | 9 | 25 | 0.22 | 9 | 25 | 0.27 | 11 | 25 | 0.16 | | | | 1 | | |
| | 7 | 1.5 | 0.10 | 7 | 1.5 | 0.10 | 17 | 1.5 | 0.10 | | | | | | |
| | 0 | 05 | 0.04 | 1 | 05 | 0.04 | 1 | 25 | 204 | | | | | | |
| | SUBT | 20.0 | 124 | SUBT | | 1N | SUBT | | 106 | SUBT | OTAL | 102 | SUBT | DIATO | 1.00 |
| - | TOTAL | | 11.99 | TOTAL | | 2.49 | TOTAL | | 11.81 | TOTAL | Section 1 | 227 | TOTAL | - | 227 |
| | LOCF | | 2 | LOC F | | 3 | LOCF | | 20 | LOCF | | 0.50 | LOCF | | 1 |
| | | CI_ | 23.98 | WTD | VI. | 20 | WTD | 61 | 236.20 | WTD | <u> </u> | 1.14 | WTD | Ç1 | 227 |
| | WTD | _ | 25.36 | WID | _ | 25.17 | WID | _ | 200.20 | MAID | | A.re | MIC | _ | 221 |
| С | _ | LAND 1 | | _ | LAND | | | LAND : | _ | 1 | LAND 4 | | 1 | | |
| | - | | _ | - | | | _ | | DEM | 450 | FCT | - | 4 | | |
| ^ | A% | FCT | DEM | A% | FGT | DEM | A% | | 5.00 | A% | _ | 500 | 1 | | |
| R | 5 | 1.00 | 500 | 3 | 1.00 | 5.00 | - | 1.00 | 3.00 | - | 1.00 | 200 | | | |
| | - | | 1.00 | - | | 1.00 | - | | 7.00 | | | 7.0 | | | |
| 0 | 5 | 0.25 | 1.25 | 3 | 0.25 | 1.25 | Name and Address of the Owner, where | 0.25 | 125 | 3 | 0.25 | 1.25 | 4 | | |
| N | SUBT | OTAL | 625 | SUBT | OTAL | 625 | SUBT | OTAL | 6.25 | SUBT | OTAL | 6.25 | | | |
| | 0 | 0.0 | 4.8 | 1 6 | 44 | 0.85 | 11 // | 100 | 0.81 | 11 77 | | 2.22 | | | |
| ٧ | 9 | 85 | 2/6 | 9 | 8.5 | 0.75 | // | 8.5 | 0.82 | 1// | 8.5 | 0.87 | | | |
| ۸ | - | 15 | 0.52 | 4 | 7.5 | 0.52 | 1 | 7.5 | | 1 | 7.5 | 0.52 | WOP | | 74.8 |
| R | 9 | 6.5 | 0.58 | 9 | 6.5 | 0.58 | | 6.5 | 0.22 | J. | 55 | 0.22 | TGC | _ | 75 |
| N | / | 55 | - | / | 55 | 0.8 | 13 | 5.5 | _ | 13 | | 0.58 | TLC | _ | 25 |
| ! | 9 | 15 | 0.40 | 9 | 45 | 240 | 9 | 45 | 240 | 9 | 4.5 | 0.40 | 4 | | |
| 8 | / | 35 | 0.24 | 1 | 15 | 024 | 5 | 15 | 0.22 | 5 | J5 | 0.22 | 4 | | |
| н | 9 | 25 | 0.77 | 3 | 25 | 0.22 | 11 | 25 | 0.16 | 11 | 25 | 2.16 | 4 | | |
| | 1 | 1.5 | 2.10 | 1 | 1.5 | 0.10 | 1 | 1.5 | 0.10 | 1 | 15 | 0.10 | 1 | | |
| | 9 | 25 | 0.04 | 3 | 95 | 0.04 | J | 0.5 | 0.04 | 1 | 0.5 | 2.04 | 1 | | |
| | SUBT | _ | 124 | SUBT | | 124 | SUBT | - | 106 | SUBT | | 206 | 1 | | |
| | TOTAL | | 8.49 | TOTAL | | 2.49 | TOTAL | | 9,37 | TOTAL | | 9,37 | 1 | | |
| | LOCF | CT | 1 | LOC F | CT | 3 | LOCF | CT | 20 | LOC F | CT | 60 | 1 | | |
| | OTW | 911 | 2.49 | WTD | 7.2 | 28.47 | WTD | | 186.20 | WTD | | 558.60 | 1 | | |
| | | | | | | | | | | | - 6 | | - | | |
| | | N NO. | 1 | RIF | VG STL | ICK | | SCUFFS | ED ARE | A.% | | TLFC | | | |
| | TOP R | ING | | | | | | | | ~ | | | | | |
| | INT. R | NG | | | | | | | | | | | | | |
| | OIL RI | NG | | -22 | | | | | | | | | | | |
| | PISTO | N | | 55000 | | | 7 | | | 3. | | | | | |
| | | | | | | | | | | | | | | | |

FIG. X1.1 Rating Worksheet Example

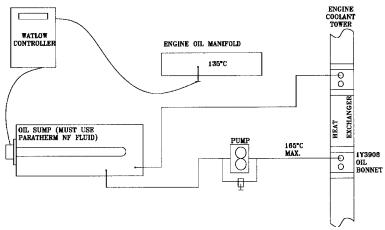
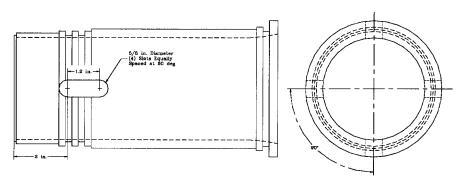


FIG. X1.2 Engine Oil Heating System





Note—Use a 1Y3555 liner from the 1K/1N test. The liner shall be free of I.D. distortion or surface distress. FIG. X1.3 Ring Side Clearance Measurement Fixture

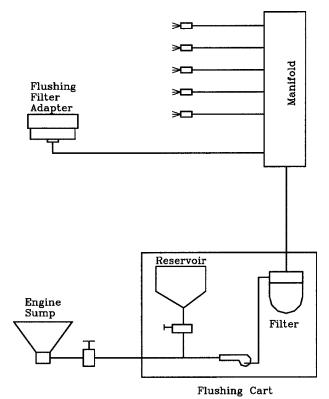


FIG. X1.4 Flushing Cart Flow Schematic

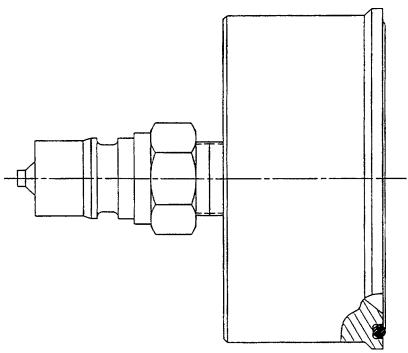
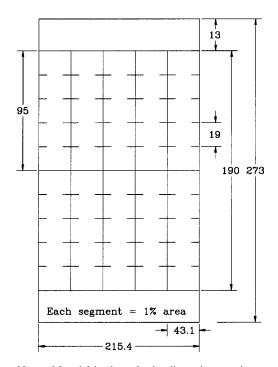


FIG. X1.5 Oil Filter Flushing Adapter Example



 $\label{eq:Note-Material} Note-Material is clear plastic; dimensions are in mm. \\ \textbf{FIG. X1.6 Bore Polish Grid}$

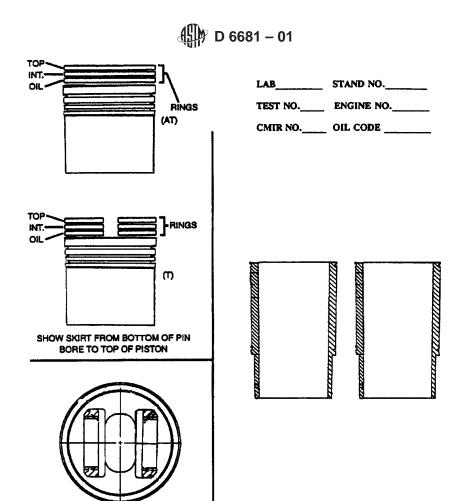


FIG. X1.7 Example of Piston, Rings and Liner Photograph Layout

PHOTO OF SECTION LINER

SHOW T & AT BORES

PHOTO OF PISTON UNDERCROWN

(Crown Only - No Skirt)

| | | 8. | | | SUMMAR | Y SHEET | | | | | |
|--------------------|----------------|---------------------|-----------------|--------------|---------|---------|----------|-----|-------------------------|--------------------|---------------------|
| | | | OIL CODE | NO | | | | _ | | | |
| | | | | | | | | | | | |
| 4 1 | DATE | | | ENGINE | | | | T | | | |
| TEST NO. | COMP | OIL CODE NO. | TEST LAB | STAND NO. | RUN NO. | WDP | TGC | TLC | 0 - 360 | BSOC g/h 0 - 48 | BSOC g/h 336-360 |
| TEST | DATA | | | | | | S. Frank | | The same of the same of | part of the | |
| 1ST 2 3 4 | | | | | | | | | | | |
| 2 | | | | | | | | | | | |
| 3 | | | | 1 | | | | | | | |
| 4 | | | | | | | | | | | |
| TES | TAVG | | | | | | | | | | 1 |
| 1ST | | | | | | | | _ | 1 | | |
| 3 | | | | | | _ | _ | _ | _ | | - |
| 3 | Marian Control | | | | 100 | | | | | | _ |
| OUTLIER | MIN. LEVEL | | | | | (1) | (2) | (4) | | | |
| 2 TEST A | VG. WITH OL | JTLIER REMOVED | | | | | - | - | | | |
| | | JTLIER REMOVED | | | | _ | - | - | | | |
| ACCEPTA | NCE LIMITS | | and the same in | | | | | | - | | |
| 1ST TEST | | | | | | - | - | - | + | | |
| 2 TEST P | | | | | | - | _ | + | + | | |
| 3 TEST P | ASS | | | | | _ | | | | | |
| NOTES: | | ST AVG + T AVG + | | | | | | | | | |
| | (4) TLHC 3 TE | | | | | | | | | | |

Note—If testing candidate lubricants in accordance with Specification D 4485, the results of multiple testing should be reported on this form.

FIG. X1.8 Example of Multiple Test Summary Sheet

X2. SAFETY

X2.1 The operating of engine tests can expose personnel and facilities to a number of safety hazards. It is recommended that only personnel who are thoroughly trained and experienced in engine testing should undertake the design, installation, and operation of engine test stands. Each laboratory conducting engine tests should have their test installation inspected and approved by their Safety Department. Personnel working on the engines should be provided with the proper tools, be alert to common sense safety practices and avoid contact with external moving or hot parts. When engines are operating at high speeds, heavy duty guards are required and personnel should be cautioned against working alongside the engine and coupling shaft. Barrier protection should be provided for personnel. All fuel, oil lines, and electrical wiring should be properly routed, guarded, and kept in good order. Scraped knuckles, minor burns, and cuts are common if proper safety precautions are not taken. Safety masks or glasses should always be worn by personnel working on the engines and no loose or flowing clothing should be worn near running engines. The external parts of the engine and the floor area around the engines should be kept clean and free of oil and fuel spills. In addition, working areas should be free of all tripping hazards. In case of injury, no matter how slight, first aid attention should be applied at once and the incident reported. Leaking fuel represents a fire hazard and exhaust gas fumes are noxious. Do not allow containers of oil or fuel to accumulate in the testing area. The test installation should be equipped with a fuel shut-off valve which is designed to automatically cut off the fuel supply to the engine when the engine is not running. A remote station for cutting off fuel from the test stand is recommended. Suitable interlocks should be provided so that the engine is automatically shut down when any of the following events occur: the engine dynamometer loses field current, engine over-speeds, low oil pressure, high water temperature, exhaust system fails, room ventilation fails, or the fire protection system is activated. Consider an excessive vibration pickup interlock if equipment operates unattended. Fixed fire protection equipment should be provided and dry chemical fire extinguishers should be available at the test stands.



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